## Traffic Impact Study Proposed Industrial Building 4540 W. Ann Lurie Place

 Chicago, Illinois

Prepared For:


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## Table of Contents

List of Figures and Tables, ii
I. Executive Summary ..... 1

1. Introduction ..... 3
2. Existing Conditions ..... 6
Site Location ..... 6
Existing Street System Characteristics ..... 6
Existing Traffic Volumes ..... 9
3. Traffic Characteristics of the Proposed Development ..... 14
Proposed Development Plan ..... 14
Directional Distribution ..... 14
Peak Hour Traffic Volumes ..... 14
4. Projected Traffic Conditions ..... 17
Development Traffic Assignment ..... 17
Ambient Traffic Growth ..... 17
Total Projected Traffic Volumes ..... 17
5. Traffic Analysis and Recommendations ..... 22
Traffic Analyses ..... 22
Discussion and Recommendations ..... 27
6. Conclusion ..... 30
Appendix

## List of Figures and Tables

## Figures

Figure 1 - Site Location ..... 4
Figure 2 - Aerial View of Site ..... 5
Figure 3 - Existing Street Characteristics ..... 7
Figure 4 - Existing Traffic Volumes ..... 11
Figure 5 - Existing Truck Traffic Volumes. ..... 12
Figure 6 - Existing Pedestrian/Bicycle Traffic Volumes ..... 13
Figure 7 - Estimated Directional Distribution. ..... 15
Figure 8 - Estimated Site-Generated Passenger Vehicle Traffic Volumes ..... 18
Figure 9 - Estimated Site-Generated Truck Traffic Volumes ..... 19
Figure 10 - Year 2028 No-Build Traffic Volumes ..... 20
Figure 11 - Year 2028 Total Projected Traffic Volumes ..... 21
Tables
Table 1 - Estimated Peak Hour and Daily Trip Generation ..... 16
Table 2 - Estimated Hourly Truck Trip Generation ..... 16
Table 3 - Capacity Analysis Results - Pulaski Road with Ann Lurie Place ..... 23
Table 4 - Capacity Analysis Results - Kildare Avenue with $47^{\text {th }}$ Street ..... 24
Table 5 - Capacity Analysis Results - Kildare Avenue with Ann Lurie Place. ..... 25
Table 6 - Capacity Analysis Results - Kildare Avenue with $45^{\text {th }}$ Street ..... 26

## I. Executive Summary

This report summarizes the results of a traffic impact study conducted by Kenig, Lindgren, O'Hara, Aboona, Inc. (KLOA, Inc.) for a proposed industrial building to be located at 4540 W . Ann Lurie Place in Chicago, Illinois. The objectives of the traffic study are as follows:

- Determine the existing vehicular, pedestrian, bicycle, and public transportation conditions in the study area to establish a base condition.
- Assess the impact that the proposed development will have on transportation conditions in the area.
- Determine any street, access, bicycle, and pedestrian modifications and/or improvements that will be necessary to effectively accommodate and mitigate future conditions.

Vehicle, pedestrian, and bicycle counts were conducted during the weekday morning and weekday evening peak periods at the intersections of Pulaski Road with Ann Lurie Place ( $42^{\text {nd }}$ Place) and Kildare Avenue with Ann Lurie Place, $45^{\text {th }}$ Street, and $47^{\text {th }}$ Street.

As proposed, the site will be developed with an approximately 147,500 square-foot industrial building. The development will provide 29 truck loading bays on the west side of the building Additionally, 102 parking spaces for employees will be provided on the north, east, and west sides of the building. Access to the site is proposed to be provided via two full movement access drives on Ann Lurie Place.

Based on the preceding analyses and recommendations, the following conclusions have been made:

- During the peak pick-up and drop-off periods of the Major Hector P. Garcia MD High School, Kildare Avenue is restricted to a one-way northbound street with queues on Kildare Avenue extending from the school pick-up and drop-off area to $47^{\text {th }}$ Street. Traffic aides are stationed at the intersections of Kildare Avenue with $45^{\text {th }}$ Street and $47^{\text {th }}$ Street to assist with the traffic flow and pedestrian activities.
- During the school peak periods, site traffic will not approach and depart the site via the Kildare Avenue and $47^{\text {th }}$ Street intersection.
- The signalized intersection of Pulaski Road with Ann Lurie Place has sufficient reserve capacity to accommodate site traffic and can accommodate all site-generated traffic during school peak periods.
- The signalized intersection of Kildare Avenue with $47^{\text {th }}$ Street has sufficient reserve capacity to accommodate site traffic. While this intersection will operate differently during school peak periods, this intersection will operate at a good LOS outside of school peak periods and site generated traffic will not turn at this intersection during the school peak periods.
- The unsignalized intersections along Kildare Avenue have sufficient reserve capacity to accommodate site-generated traffic and no traffic control improvements will be required as part of the development.
- The proposed access system will be adequate in accommodating the traffic estimated to be generated by the development.


## 1. Introduction

This report summarizes the methodologies, results, and findings of a traffic impact study conducted by Kenig, Lindgren, O'Hara, Aboona, Inc. (KLOA, Inc.) for a proposed industrial building to be located at 4540 W . Ann Lurie Place in Chicago, Illinois. The site, which currently contains a trailer storage lot, is located on the north side of Ann Lurie Place ( $42^{\text {nd }}$ Place) approximately 1,400 feet west of its intersection with Kildare Avenue. As proposed, the site will be developed with an approximately 147,500 square-foot industrial building. Access to the site is proposed to be provided via two full movement access drives off Ann Lurie Place.

The purpose of this study was to examine existing traffic conditions, assess the impact that the proposed development will have on traffic conditions in the area, and determine if any determine if any improvements to the transportation system are required to accommodate the proposed development. Figure 1 shows the location of the site in relation to the area street system. Figure 2 shows an aerial view of the site.

The sections of this report present the following:

## - Existing street conditions

- A description of the proposed development
- Directional distribution of the development traffic
- Vehicle trip generation for the development
- Future traffic conditions including access to the development
- Traffic analyses for the weekday morning and weekday evening peak hours
- Evaluation and recommendations with respect to adequacy of the site access, on-site circulation, and adjacent street system.

Traffic capacity analyses were conducted for the weekday morning and weekday evening peak hours for the following conditions:

1. Existing Conditions - Analyze the capacity of the existing roadway system using existing peak hour traffic volumes in the surrounding area.
2. Year 2028 No-Build Conditions - Analyzes the capacity of the existing roadway system using existing traffic volumes increased by an ambient area growth factor not attributable to any particular development.
3. Year 2028 Total Projected Conditions - Analyzes the capacity of the future roadway system assuming the projected traffic volumes that include the Year 2028 no-build traffic volumes and the traffic estimated to be generated by the proposed development.


## Site Location

Figure 1


## Aerial View of Site

Figure 2

## 2. Existing Conditions

Existing transportation conditions in the vicinity of the site were documented based on field visits conducted by KLOA, Inc. in order to obtain a database for projecting future conditions. The following provides a description of the geographical location of the site, physical characteristics of the area street system including lane usage and traffic control devices, and existing peak hour traffic volumes.

## Site Location

The site, which currently contains a trailer storage lot, is generally bounded by a Belt Railway of Chicago railroad to the north and west, BT Wholesale and Gold Eagle to the east, and Ann Lurie Place to the south. Land uses within the vicinity of the site are primarily industrial north of $43^{\text {rd }}$ Street and west of Keeler Avenue. Multiple commercial uses including Pulaski Promenade are located along Pulaski Road. The Major Hector P. Garcia M.D. High School is located in the northeast quadrant of the intersection of Kildare Avenue with Ann Lurie Place.

## Existing Street System Characteristics

The characteristics of the existing streets near the development are described below and illustrated in Figure 3.

Pulaski Road is a north-south principal arterial street that generally provides two lanes in each direction. Between Ann Lurie Street and $43^{\text {rd }}$ Street, Pulaski Road provides a northbound bus only lane. At its signalized intersection with Ann Lurie Place, Pulaski Road provides an exclusive leftturn lane, two through lanes, and a bus only lane on the northbound approach and a through lane and a shared through/right-turn lane on the southbound approach. All legs of this intersection provide high visibility crosswalks with pedestrian signals. Approximately one-half mile north of Ann Lurie Place, Pulaski Road has a single point urban interchange with Interstate 55. Pulaski Road is under the jurisdiction of the Illinois Department of Transportation (IDOT), carries an Annual Average Daily Traffic of 40,000 vehicles (IDOT 2021) and is designated as a Strategic Regional Arterial (SRA). Parking is prohibited on both sides of the street.
$47^{\text {th }}$ Street is an east-west major collector street. $47^{\text {th }}$ Street provides one lane in each direction; however, during the weekday peak periods, parking restrictions are enforced which adds an additional westbound lane. At its signalized intersection with Kildare Avenue, $47^{\text {th }}$ Street provides one eastbound lane and one westbound lane or two westbound lanes during the peak periods. It should be noted that a parking restriction approaching this intersection on the south side of the street provides adequate space for through and right-turning vehicles to bypass vehicles waiting to turn left. All legs of this intersection provide high visibility crosswalks with pedestrian signals. Within the vicinity of the site, $47^{\text {th }}$ Street is under the jurisdiction of the Chicago Department of Transportation (CDOT) and carries an AADT of 17,400 vehicles (IDOT 2021). Parking is generally permitted on the south side of the street at all times and on the north side of the street outside of the peak periods.


Ann Lurie Place (42 ${ }^{\text {nd }}$ Place) is an east-west local street that extends west from Pulaski Road and provides one lane in each direction. At its signalized intersection with Pulaski Road, Ann Lurie Place provides a shared left-turn/right-turn lane on the eastbound approach. All legs of this intersection provide high visibility crosswalks with pedestrian signals. At its all-way stop signcontrolled intersection with Kildare Avenue, Ann Lurie Place provides one lane on both approaches. All legs of this intersection provide high visibility crosswalks. Ann Lurie Place is under the jurisdiction of CDOT. Parking is generally permitted on the north side of the street and is generally permitted on the south side of the street east of Kildare Avenue.

Kildare Avenue is a north-south, local street that generally provides one lane in each direction. At its signalized intersection with $47^{\text {th }}$ Street, the south leg of Kildare Avenue is offset approximately 40 feet to the east and is restricted to southbound only traffic. At this intersection, Kildare Avenue provides a shared left-turn/through/right-turn lane on the southbound approach. All legs of this intersection provide high visibility crosswalks with pedestrian signals. At its all-way stop signcontrolled intersections with Ann Lurie Place and $45^{\text {th }}$ Street, Kildare Avenue provides one lane on both approaches. All legs of these intersections provide high visibility crosswalks. Kildare Avenue is under the jurisdiction of CDOT. Non-truck parking is generally permitted on both sides of street north of $45^{\text {th }}$ Street and south of $47^{\text {th }}$ Street. Between $45^{\text {th }}$ Street and $47^{\text {th }}$ Street, private perpendicular parking is provided on the west side of the street and permit parking is provided on the east side of the street except for along the Major Hector P. Garcia M.D. High School frontage which is public parking outside of school hours (7:00 to 5:00 P.M. school days).
$45^{\text {th }}$ Street is an east-west local street that provides one lane in each direction. At its all-way stop sign-controlled intersection with Kildare Avenue, $45^{\text {th }}$ Street provides one lane on both approaches. All legs of this intersection provide high visibility crosswalk. This segment of $45^{\text {th }}$ Street terminates just west of Keeler Avenue and does not provide connection to Pulaski Road. $45^{\text {th }}$ Place is under the jurisdiction of CDOT. Parking is generally permitted on the north side of the street and is generally permitted on the south side of the street east of Kildare Avenue.

## Alternative Modes of Transportation

Accessibility to and from the area is enhanced by the various alternative modes of transportation serving the area as summarized below.

Public Transportation. The area is served by the Chicago Transit Authority via the following bus routes that have stops near the development:

Route 47 ( $47^{\text {th }}$ Street) provides service along $47^{\text {th }}$ Street from Cicero Avenue to Lake Park Avenue. Service is provided seven days a week from 4:00 A.M. to 12:40 A.M. This line provides connection to the CTA Orange, Red, and Green lines and Chicago Midway International Airport.

Route 53 (Pulaski) generally runs along Pulaski Road between Peterson Avenue and $31^{\text {st }}$ Street serving destinations including the Irving Park Blue Line Station and Pulaski Blue Line Station. Service is provided seven days a week twenty-four hours a day between Irving Park Road and Harrison Street. Service between Peterson Avenue and $31^{\text {st }}$ Street is from approximately 4:00 A.M. to 1:00 A.M. seven days a week. This line provides connection to the CTA Blue (O'Hare and Forest Park), Pink, and Green lines.

Pedestrian Accommodations. Sidewalks and high-visibility crosswalks are generally provided on the majority of the streets within the study area.

## Major Hector P. Garcia M.D. High School Operations

The Major Hector P. Garcia M.D. High School is located in the northeast quadrant of the intersection of Kildare Avenue with $47^{\text {th }}$ Street. Pick-up and drop-off activity occurs on Kildare Avenue along the school frontage. Observations of school activity indicated the following:

- From approximately 7:20 A.M. to 8:05 A.M. and 2:05 P.M. to 2:45 P.M. a barricade is placed on the south leg of Kildare Avenue at its intersection with $45^{\text {th }}$ Street, restricting it to one-way northbound only traffic between $45^{\text {th }}$ Street and $47^{\text {th }}$ Street.
- From approximately 7:30 A.M. to 8:05 A.M and 2:15 P.M. to 2:45 P.M. traffic aides were stationed at the intersections of Kildare Avenue with $45^{\text {th }}$ Street and $47^{\text {th }}$ Street to direct both vehicular and pedestrian traffic.
- From approximately 7:20 A.M. to 8:00 A.M and 2:00 P.M to 2:45 P.M. queues from the pick-up and drop-off activity on Kildare Avenue extended to $47^{\text {th }}$ Street and vehicles were required to wait on $47^{\text {th }}$ Street. During this time, through vehicles on $47^{\text {th }}$ Street were able to continue to traverse the intersection. Westbound vehicles waiting to turn right queued in the outside westbound lane on $47^{\text {th }}$ Street allowing through vehicles to continue and sufficient space was available for eastbound through vehicles on $47^{\text {th }}$ Street to bypass eastbound vehicles waiting to turn left.

It should be noted that the intersection of Kildare Avenue with $47^{\text {th }}$ Street operates with a longer cycle length and different timings during the school peak periods. Outside of these peak pick-up and drop-off periods school operations had a limited impact on traffic operations in the area.

## Existing Traffic Volumes

In order to determine current traffic conditions in the vicinity of the site, KLOA, Inc. conducted peak period pedestrian, bike, and vehicle traffic counts using Miovision Scout Video Collection Units on Wednesday May 18, 2021 during the weekday morning (6:30 A.M. to 9:00 A.M.) and weekday evening (3:30 P.M. to 6:00 P.M.) peak periods at the following intersections:

- Pulaski Road with Ann Lurie Place
- Kildare Avenue with Ann Lurie Place
- Kildare Avenue with $45^{\text {th }}$ Street
- Kildare Avenue with $47^{\text {th }}$ Street

The results of the traffic counts indicated that the weekday morning peak hour of traffic occurs from 7:15 A.M. to 8:15 A.M. and the weekday evening peak hour of traffic occurs from 3:45 P.M. to 4:45 P.M. Copies of the traffic count summary sheets are included in the Appendix.

In order to ensure that the traffic counts reflect normal traffic conditions, they were compared with previous hourly counts conducted by IDOT on Pulaski Road in 2019. Overall, the comparison indicated that the traffic counts conducted in 2022 were higher than the historic traffic volumes and, as such, were not adjusted.

Figure 4 illustrates the existing peak hour vehicle traffic volumes, inclusive of heavy vehicles. Figure 5 illustrates the existing heavy vehicle peak hour traffic volumes. Figure 6 illustrates the existing pedestrian and bicycle volumes, showing direction of travel.




## 3. Traffic Characteristics of the Proposed Development

In order to properly evaluate future traffic conditions in the surrounding area, it was necessary to determine the traffic characteristics of the proposed development, including the directional distribution and volumes of traffic that it will generate.

## Proposed Development Plan

As proposed, the site will be developed with an approximately 147,500 square-foot light industrial development. The development will provide 29 truck loading bays on the west side of the building. Additionally, 102 parking spaces for employees will be provided on the north, east, and west sides of the building. Access to the development is proposed to be provided as follows:

- A full movement access drive on the north side of Ann Lurie Place located approximately 1,460 feet west of Kildare Avenue. This access drive will provide one inbound lane and one outbound lane with outbound movements under stop sign control. This access drive will serve the employee parking lots.
- A full movement access drive on the north side of Ann Lurie Place located approximately 1,720 feet west of Kildare Avenue. This access drive will provide one inbound lane and one outbound lane wide enough to accommodate truck turning movements. Outbound movements will be under stop sign control. This access drive will primarily serve the truck loading bays.

A copy of the preliminary site plan is included in the appendix.

## Directional Distribution

The directions from which employees and truck traffic will approach and depart the site were estimated based on existing travel patterns, the proposed access system, and travel routes to and from Interstate 55. It should be noted that truck traffic will be able to approach and depart the site via both Ann Lurie Place and Kildare Avenue. Figure 7 illustrates the directional distribution of traffic. Figure 7 also shows the distance, in feet, between the existing and proposed access intersections.

## Peak Hour Traffic Volumes

The number of peak hour trips estimated to be generated by the proposed development was based on trip generation rates published by the Institute of Transportation Engineers (ITE) in Trip Generation Manual, $11^{\text {th }}$ Edition. The "General Light Industrial" (Land-Use Code 110) was used for the development. Table 1 summarizes the trips projected to be generated by the development during the peak hours and on a daily basis. Table 2 summarized the truck trips projected to be generated by the development through the day.


Table 1
ESTIMATED PEAK HOUR AND DAILY TRIP GENERATION

| ITE Land Use | Type/Size |  | Veekd Morni ak H |  |  | week Even ak |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Code |  | In | Out | Total | In | Out | Total | In | Out |
| 110 | General Light Industrial ${ }^{1}$ ( 147,500 s.f.) | 92 | 12 | 104 | 7 | 46 | 53 | 303 | 303 |
|  | Truck Trips2 | 2 | 2 | 4 | 2 | 2 | 4 | 19 | 19 |
|  | Passenger Vehicle Trips ${ }^{3}$ | 90 | 10 | 100 | 5 | 44 | 49 | 284 | 284 |
| 1 - Based on the Institute of Transportation Engineers' (ITE) Trip Generation Manual, $11^{\text {th }}$ Edition <br> 2 - Daily rate based on ITE manual. Peak hours based on Table 2. <br> 3 - Equal to total trips less truck trips. |  |  |  |  |  |  |  |  |  |

Table 2
ESTIMATED HOURLY TRUCK TRIP GENERATION

|  | Light Industrial (ITE Land-Use Code 110) - 147,500 s.f. |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Hour | Weekday Morning |  |  |  | Weekday Evening |
|  | In | Out | Total | In | Out | Total |
| $12: 00$ | 0 | 0 | $\mathbf{0}$ | 2 | 2 | $\mathbf{4}$ |
| $1: 00$ | 0 | 0 | $\mathbf{0}$ | 2 | 2 | $\mathbf{4}$ |
| $2: 00$ | 0 | 0 | $\mathbf{0}$ | 2 | 2 | $\mathbf{4}$ |
| $3: 00$ | 0 | 0 | $\mathbf{0}$ | 2 | 2 | $\mathbf{4}$ |
| $4: 00$ | 0 | 0 | $\mathbf{0}$ | 1 | 1 | $\mathbf{2}$ |
| $5: 00$ | 0 | 0 | $\mathbf{0}$ | 0 | 0 | $\mathbf{0}$ |
| $6: 00$ | 0 | 0 | $\mathbf{0}$ | 0 | 0 | $\mathbf{0}$ |
| $7: 00$ | 2 | 1 | $\mathbf{3}$ | 0 | 0 | $\mathbf{0}$ |
| $8: 00$ | 2 | 2 | $\mathbf{4}$ | 0 | 0 | $\mathbf{0}$ |
| $9: 00$ | 3 | 3 | $\mathbf{6}$ | 0 | 0 | $\mathbf{0}$ |
| $10: 00$ | 2 | 3 | $\mathbf{5}$ | 0 | 0 | $\mathbf{0}$ |
| $11: 00$ | 1 | 1 | $\mathbf{2}$ | 0 | 0 | $\mathbf{0}$ |
| Based on daily truck trips (Table 1) and ITE's Hourly Distribution of Entering and Exiting Truck Trips tables. |  |  |  |  |  |  |

## 4. Projected Traffic Conditions

The total projected traffic volumes include the existing traffic volumes, increase in background traffic due to growth, and the traffic estimated to be generated by the proposed subject development.

## Development Traffic Assignment

The estimated weekday morning and weekday evening peak hour traffic volumes that will be generated by the proposed development were assigned to the street system in accordance with the previously described directional distribution (Figure 7). Figure 8 illustrates the traffic assignment of the new employee and delivery van vehicle trips for the development. Figure 9 illustrates the traffic assignment of the new truck trips for the development.

## Ambient Traffic Growth

To account for any additional increase in traffic due to other factors or developments not previously discussed, an ambient growth factor of 0.5 percent per year was also applied to the study area over a six-year period to represent Year 2028 no-build conditions. Furthermore, in order to account for the increase in population in the study area, bicycle and pedestrian volumes were increased by 10 percent at each intersection. Figure 10 illustrates the Year 2028 no-build volumes.

## Total Projected Traffic Volumes

The existing traffic volumes increased by the ambient growth in the area, were combined with the new peak hour traffic volumes generated by the subject development to determine the Year 2028 total traffic volumes, shown in Figure 11.





## 5. Traffic Analysis and Recommendations

The following provides an evaluation conducted for the weekday morning and weekday evening peak hours. The analysis includes conducting capacity analyses to determine how well the street system and access drives are projected to operate and whether any street improvements or modifications are required.

## Traffic Analyses

Intersection analyses were performed for the weekday morning and weekday evening peak hours for the existing, Year 2028 no-build, and Year 2028 total projected traffic volumes.

The traffic analyses were performed using the methodologies outlined in the Transportation Research Board's Highway Capacity Manual (HCM), $6^{\text {th }}$ Edition and analyzed using Synchro/SimTraffic 11 software. The analysis for the signalized intersections were conducted utilizing actual cycle lengths, phasings, and offsets.

The analyses for the unsignalized intersections determine the average control delay to vehicles at an intersection. Control delay is the elapsed time from a vehicle joining the queue at a stop sign (includes the time required to decelerate to a stop) until its departure from the stop sign and resumption of free flow speed. The methodology analyzes each intersection approach controlled by a stop sign and considers traffic volumes on all approaches and lane characteristics.

The ability of an intersection to accommodate traffic flow is expressed in terms of level of service, which is assigned a letter from A to F based on the average control delay experienced by vehicles passing through the intersection. The Highway Capacity Manual definitions for levels of service and the corresponding control delay for signalized intersections and unsignalized intersections are included in the Appendix of this report.

Summaries of the traffic analysis results showing the level of service and overall intersection delay (measured in seconds) for the existing, Year 2028 no-build, and Year 2028 total projected conditions are presented in Tables $\mathbf{3}$ through 6. A discussion of the intersections follows. Summary sheets for the capacity analyses are included in the Appendix.

Table 3
CAPACITY ANALYSIS RESULTS - PULASKI ROAD WITH ANN LURIE PLACE


Table 4
CAPACITY ANALYSIS RESULTS - KILDARE AVENUE WITH $47^{\text {TH }}$ STREET


Table 5
CAPACITY ANALYSIS RESULTS - KILDARE AVENUE WITH 42 ${ }^{\text {ND }}$ PLACE - ALL-WAY STOP SIGN CONTROLLED

| Intersection | Weekday Morning Peak Hour |  | Weekday Evening Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |
| Existing Conditions |  |  |  |  |
| - Overall | B | 11.6 | A | 9.0 |
| - Eastbound Approach | A | 9.5 | A | 8.0 |
| - Westbound Approach | B | 10.2 | A | 9.2 |
| - Northbound Approach | B | 12.9 | A | 10.0 |
| - Southbound Approach | A | 8.7 | A | 8.1 |
| Year 2028 No-Build Conditions |  |  |  |  |
| - Overall | B | 11.6 | A | 9.0 |
| - Eastbound Approach | A | 9.5 | A | 8.0 |
| - Westbound Approach | B | 10.2 | A | 9.2 |
| - Northbound Approach | B | 12.9 | A | 10.0 |
| - Southbound Approach | A | 8.7 | A | 8.1 |
| Year 2028 Total Projected Conditions |  |  |  |  |
| - Overall | B | 12.4 | A | 9.1 |
| - Eastbound Approach | A | 9.9 | A | 8.5 |
| - Westbound Approach | B | 11.5 | A | 9.3 |
| - Northbound Approach | B | 13.8 | A | 9.9 |
| - Southbound Approach | A | 9.1 | A | 8.3 |
| LOS = Level of Service Delay is measured in seconds. |  |  |  |  |

Table 6
CAPACITY ANALYSIS RESULTS - KILDARE AVENUE WITH $45^{\text {TH }}$ STREET - ALL-WAY STOP SIGN CONTROLLED

| Intersection | Weekday Morning Peak Hour ${ }^{1}$ |  | Weekday Evening Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |
| Existing Conditions |  |  |  |  |
| - Overall | C | 17.2 | A | 8.9 |
| - Eastbound Approach | C | 15.7 | A | 8.8 |
| - Westbound Approach | B | 10.6 | A | 8.1 |
| - Northbound Approach | C | 21.5 | A | 7.7 |
| - Southbound Approach | B | 10.6 | A | 9.6 |
| Year 2028 No-Build Conditions |  |  |  |  |
| - Overall | C | 17.2 | A | 8.9 |
| - Eastbound Approach | C | 15.7 | A | 8.8 |
| - Westbound Approach | B | 10.6 | A | 8.1 |
| - Northbound Approach | C | 21.5 | A | 7.7 |
| - Southbound Approach | B | 10.6 | A | 9.6 |
| Year 2028 Total Projected Conditions |  |  |  |  |
| - Overall | C | 19.2 | A | 9.1 |
| - Eastbound Approach | C | 16.2 | A | 8.9 |
| - Westbound Approach | B | 10.9 | A | 8.2 |
| - Northbound Approach | C | 24.9 | A | 7.8 |
| - Southbound Approach | B | 10.9 | A | 9.8 |
| 1 - Intersection operates differently during Major Hector P. Garcia MD High School peak periods. | $\text { LOS }=\text { Leve }$ <br> Delay is me | Service ed in secon |  |  |

## Discussion and Recommendations

The following summarizes how the intersections are projected to operate and identifies any street and traffic control improvements necessary to accommodate the development-generated traffic.

## Pulaski Road with Ann Lurie Place

The results of the capacity analysis indicate that overall, this intersection currently operates at Level of Service (LOS) B during the weekday morning peak hour and weekday evening peak hours. Further, all movements operate at LOS D or better during both peak hours and through movements on Pulaski Road operate at LOS B or better during both peak hours. Under Year 2028 no-build conditions, this intersection is projected to continue to operate at LOS B during both peak hours.

Under Year 2028 total projected traffic conditions, this intersection is projected to continue to operate at LOS B during the weekday morning and weekday evening peak hours with increases in delay of approximately one to two seconds over no build conditions. Further, all movements are projected to continue to operate at LOS D or better during both peak hours and through movements on Pulaski Road are projected to continue to operate at LOS B or better during both peak hours.

As previously indicated, during the peak pick-up and drop-off periods of the Major Hector P. Garcia MD High School, Kildare Avenue is restricted to one-way northbound traffic and queues on Kildare Avenue extended from the school pick-up and drop-off area onto $47^{\text {th }}$ Street. Given this congestion during these time periods, it expected that site traffic will avoid travelling on Kildare Avenue and seek an alternative route to and from the proposed development. In order to reflect this reassignment and to provide a conservative analysis, this intersection was also analyzed assuming that during the weekday morning peak hour all site generated traffic approaches and departs the site via this intersection. The results of this capacity analysis indicate that under Year 2028 total projected conditions, this intersection is projected to continue to operate at LOS B during the weekday morning peak hour and all movements are projected to operate at the same LOS as no-build conditions. It should be noted that the school's peak pick-up activities during the weekday afternoon occurs before the peak hour of roadway traffic and as such the school traffic will have a minimal impact on roadway operations during the weekday evening peak hour.

As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements or traffic signal modifications will be required as part of proposed development.

## Kildare Avenue with $47^{\text {th }}$ Street

The results of the capacity analysis indicate that overall, this intersection currently operates at LOS B during the weekday morning peak hour and weekday evening peak hours. Further, all movements operate at LOS C or better during both peak hours and through movements on $47^{\text {th }}$ Street operate at LOS B or better during both peak hours.

Under Year 2028 no-build conditions and Year 2028 total projected traffic conditions, this intersection is projected to continue to operate at LOS B during the weekday morning and weekday evening peak hours conditions. Further, all movements are projected to continue to operate at the same LOS during both peak hours and through movements on $47^{\text {th }}$ Street are projected to continue to operate at LOS B or better during both peak hours.

As previously mentioned, during the peak pick-up and drop-off periods of the Major Hector P. Garcia MD High School, Kildare Avenue is restricted to one-way northbound traffic and queues on Kildare Avenue extended from the school pick-up and drop-off area onto $47^{\text {th }}$ Street. Further, a traffic aid is stationed at this intersection to direct both vehicular and pedestrian traffic. While the results of the analysis indicate that this intersection has sufficient capacity to accommodate the existing and projected traffic volumes during the weekday morning peak hour, these results do not fully reflect the impact of drop-off activity. However, during these peak periods site traffic will seek alternative routes to and from the proposed development. Further, the school's peak pick-up activities occur during the weekday afternoon before the peak hour of roadway traffic and as such school operations will have a minimal impact on roadway operations during the weekday evening peak hour.

As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements or traffic signal modifications will be required as part of proposed development.

## Kildare Avenue with Ann Lurie Place

The results of the capacity analysis indicate that overall, this intersection currently operates at LOS B during the weekday morning peak hour and LOS A during the weekday evening peak hour. Further, all the intersection approaches operate at LOS B or better during both peak hours.

Under Year 2028 total projected conditions, this intersection overall is projected to continue to operate at LOS B during the weekday morning peak hour and LOS A during the weekday evening peak hour with increases in delay of less than one second. Further, all the intersection movements are projected to continue to operate the same LOS as existing conditions during both peak hours. As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements will be required as part of the proposed development.

## Kildare Avenue with $45^{\text {th }}$ Street

The results of the capacity analysis indicate that overall, this intersection currently operates at LOS C during the weekday morning peak hour and LOS A during the weekday evening peak hour. Further, all the intersection approaches operate at LOS C or better during both peak hours.

Under Year 2028 total projected conditions, this intersection overall is projected to continue to operate at LOS C during the weekday morning peak hour and LOS A during the weekday evening peak hour with increases in delay of approximately two and one seconds, respectively. Further, all the intersection movements are projected to continue to operate the same LOS as existing conditions during both peak hours.

As previously mentioned, during the peak pick-up and drop-off periods of the Major Hector P. Garcia MD High School, Kildare Avenue is restricted to a one-way northbound traffic. Further, a traffic aid is stationed at this intersection to direct both vehicular and pedestrian traffic. While the results of the analysis indicate that this intersection has sufficient capacity to accommodate the existing and projected traffic volumes during the weekday morning peak hour, these results do not fully reflect the impact of drop-off activity. However, during these peak periods site traffic will seek alternative routes to and from the proposed development. Further, the school's peak pick-up activities occur during the weekday afternoon before the peak hour of roadway traffic and as such school operations will have a minimal impact on roadway operations during the weekday evening peak hour.

As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements will be required as part of the proposed development.

Ann Lurie Place with the Site Access Drives
As proposed two full movement access drives will be provided off Ann Lurie Place located approximately 1,460 and 1,720 feet west of Kildare Avenue. The access drives will provide one inbound lane and one outbound lane with outbound movements under stop sign control.

Under existing conditions, Ann Lurie Place carries a limited volume of traffic along the site frontage and exclusively serve local developments. As such, outbound vehicles from the site access drives will be able to turn with limited delay.

## 6. Conclusion

Based on the preceding analyses and recommendations, the following conclusions have been made:

- During the peak pick-up and drop-off periods of the Major Hector P. Garcia MD High School, Kildare Avenue is restricted to a one-way northbound street with queues on Kildare Avenue extending from the school pick-up and drop-off area to $47^{\text {th }}$ Street. Traffic aides are stationed at the intersections of Kildare Avenue with $45^{\text {th }}$ Street and $47^{\text {th }}$ Street to assist with the traffic flow and pedestrian activities.
- During the school peak periods, site traffic will not approach and depart the site via the Kildare Avenue and $47^{\text {th }}$ Street intersection.
- The signalized intersection of Pulaski Road with Ann Lurie Place has sufficient reserve capacity to accommodate site traffic and can accommodate all site-generated traffic during school peak periods.
- The signalized intersection of Kildare Avenue with $47^{\text {th }}$ Street has sufficient reserve capacity to accommodate site traffic. While this intersection will operate differently during school peak periods, this intersection will operate at a good LOS outside of school peak periods and site-generated traffic will not turn at this intersection during the school peak periods.
- The unsignalized intersections along Kildare Avenue have sufficient reserve capacity to accommodate site-generated traffic and no traffic control improvements will be required as part of the development.
- The proposed access system will be adequate in accommodating the traffic estimated to be generated by the development.


## Appendix

Traffic Count Summary Sheets Preliminary Site Plan ITE Trip Generation Worksheets Level of Service Criteria Capacity Analysis Summary Sheets

## Traffic Count Summary Sheets

Rosemont, Illinois, United States 60018 (847)518-9990 abowen@kloainc.com

Count Name: Kildare Rd with 45th St TMC Site Code:
Start Date: 05/18/2022
Page No: 1


| \% Lights | 100.0 | 92.8 | 88.8 | 80.2 | - | 90.6 | 100.0 | 89.5 | 76.5 | 92.0 | - | 88.1 | 100.0 | 98.2 | 96.2 | 94.8 | - | 96.4 | 0.0 | 87.7 | 93.7 | 83.0 | - | 90.2 | 92.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Buses | 0 | 5 | 0 | 3 | - | 8 | 0 | 0 | 0 | 0 | - | 0 | 0 | 2 | 0 | 1 | - | 3 | 0 | 0 | 1 | 11 | - | 12 | 23 |
| \% Buses | 0.0 | 0.9 | 0.0 | 3.5 | - | 1.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.9 | 0.0 | 0.5 | - | 0.4 | 0.0 | 0.0 | 0.2 | 5.2 | - | 1.5 | 0.8 |
| Single-Unit Trucks | 0 | 24 | 17 | 8 | - | 49 | 0 | 5 | 16 | 12 | - | 33 | 0 | 1 | 7 | 4 | - | 12 | 1 | 6 | 18 | 17 | - | 42 | 136 |
| $\begin{aligned} & \hline \text { \% Single-Unit } \\ & \text { Trucks } \\ & \hline \end{aligned}$ | 0.0 | 4.3 | 9.0 | 9.3 | - | 5.9 | 0.0 | 8.8 | 23.5 | 7.4 | - | 11.3 | 0.0 | 0.5 | 1.7 | 1.9 | - | 1.4 | 100.0 | 7.4 | 3.5 | 8.0 | - | 5.2 | 4.9 |
| Articulated Trucks | 0 | 11 | 4 | 5 | - | 20 | 0 | 1 | 0 | 1 | - | 2 | 0 | 1 | 9 | 5 | - | 15 | 0 | 4 | 11 | 8 | - | 23 | 60 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | 0.0 | 2.0 | 2.1 | 5.8 | - | 2.4 | 0.0 | 1.8 | 0.0 | 0.6 | - | 0.7 | 0.0 | 0.5 | 2.2 | 2.4 | - | 1.8 | 0.0 | 4.9 | 2.2 | 3.8 | - | 2.9 | 2.2 |
| Bicycles on Road | 0 | 0 | 0 | 1 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 1 | - | 1 | 0 | 0 | 2 | 0 | - | 2 | 4 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \\ \hline \end{gathered}$ | 0.0 | 0.0 | 0.0 | 1.2 | - | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | 0.5 | - | 0.1 | 0.0 | 0.0 | 0.4 | 0.0 | - | 0.2 | 0.1 |
| Pedestrians | - | - | - | - | 20 | - | - | - | - | - | 12 | - | - | - | - | - | 14 | - | - | - | - | - | 5 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |

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Count Name: Kildare Rd with 45th St TMC Site Code:
Start Date: 05/18/2022
Page No: 3

Turning Movement Peak Hour Data (7:15 AM)

| Start Time | 45th St <br> Eastbound |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Kildare Rd Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \\ & \hline \end{aligned}$ |  |
| 7:15 AM | 0 | 69 | 11 | 7 | 0 | 87 | 0 | 3 | 8 | 19 | 1 | 30 | 0 | 23 | 33 | 12 | 0 | 68 | 0 | 4 | 13 | 4 | 0 | 21 | 206 |
| 7:30 AM | 0 | 57 | 5 | 2 | 1 | 64 | 0 | 2 | 8 | 14 | 3 | 24 | 0 | 61 | 61 | 19 | 6 | 141 | 0 | 15 | 4 | 11 | 0 | 30 | 259 |
| 7:45 AM | 0 | 65 | 8 | 1 | 3 | 74 | 0 | 0 | 7 | 15 | 3 | 22 | 0 | 57 | 33 | 20 | 2 | 110 | 0 | 20 | 1 | 10 | 0 | 31 | 237 |
| 8:00 AM | 0 | 51 | 2 | 6 | 1 | 59 | 0 | 4 | 5 | 18 | 1 | 27 | 0 | 38 | 45 | 36 | 2 | 119 | 0 | 1 | 19 | 13 | 0 | 33 | 238 |
| Total | 0 | 242 | 26 | 16 | 5 | 284 | 0 | 9 | 28 | 66 | 8 | 103 | 0 | 179 | 172 | 87 | 10 | 438 | 0 | 40 | 37 | 38 | 0 | 115 | 940 |
| Approach \% | 0.0 | 85.2 | 9.2 | 5.6 | - | - | 0.0 | 8.7 | 27.2 | 64.1 | - | - | 0.0 | 40.9 | 39.3 | 19.9 | - | - | 0.0 | 34.8 | 32.2 | 33.0 | - | - | - |
| Total \% | 0.0 | 25.7 | 2.8 | 1.7 | - | 30.2 | 0.0 | 1.0 | 3.0 | 7.0 | - | 11.0 | 0.0 | 19.0 | 18.3 | 9.3 | - | 46.6 | 0.0 | 4.3 | 3.9 | 4.0 | - | 12.2 | - |
| PHF | 0.000 | 0.877 | 0.591 | 0.571 | - | 0.816 | 0.000 | 0.563 | 0.875 | 0.868 | - | 0.858 | 0.000 | 0.734 | 0.705 | 0.604 | - | 0.777 | 0.000 | 0.500 | 0.487 | 0.731 | - | 0.871 | 0.907 |
| Lights | 0 | 227 | 20 | 15 | - | 262 | 0 | 8 | 17 | 62 | - | 87 | 0 | 177 | 171 | 87 | - | 435 | 0 | 39 | 34 | 31 | - | 104 | 888 |
| \% Lights | - | 93.8 | 76.9 | 93.8 | - | 92.3 | - | 88.9 | 60.7 | 93.9 | - | 84.5 | - | 98.9 | 99.4 | 100.0 | - | 99.3 | - | 97.5 | 91.9 | 81.6 | - | 90.4 | 94.5 |
| Buses | 0 | 2 | 0 | 0 | - | 2 | 0 | 0 | 0 | 0 | - | 0 | 0 | 1 | 0 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 3 |
| \% Buses | - | 0.8 | 0.0 | 0.0 | - | 0.7 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.6 | 0.0 | 0.0 | - | 0.2 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.3 |
| Single-Unit Trucks | 0 | 9 | 5 | 1 | - | 15 | 0 | 1 | 11 | 3 | - | 15 | 0 | 1 | 0 | 0 | - | 1 | 0 | 0 | 2 | 6 | - | 8 | 39 |
| $\begin{gathered} \text { \% Single-Unit } \\ \text { Trucks } \end{gathered}$ | - | 3.7 | 19.2 | 6.3 | - | 5.3 | - | 11.1 | 39.3 | 4.5 | - | 14.6 | - | 0.6 | 0.0 | 0.0 | - | 0.2 | - | 0.0 | 5.4 | 15.8 | - | 7.0 | 4.1 |
| Articulated Trucks | 0 | 4 | 1 | 0 | - | 5 | 0 | 0 | 0 | 1 | - | 1 | 0 | 0 | 1 | 0 | - | 1 | 0 | 1 | 0 | 1 | - | 2 | 9 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 1.7 | 3.8 | 0.0 | - | 1.8 | - | 0.0 | 0.0 | 1.5 | - | 1.0 | - | 0.0 | 0.6 | 0.0 | - | 0.2 | - | 2.5 | 0.0 | 2.6 | - | 1.7 | 1.0 |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | 0 | - | 1 | 1 |
| \% Bicycles on Road | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 2.7 | 0.0 | - | 0.9 | 0.1 |
| Pedestrians | - | - | - | - | 5 | - | - | - | - | - | 8 | - | - | - | - | - | 10 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | - | - | - |

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Count Name: Kildare Rd with 45th St TMC Site Code:
Slart Date: 05/18/2022
Page No: 4

Turning Movement Peak Hour Data (3:45 PM)

| Start Time | 45th St <br> Eastbound |  |  |  |  |  | 45th St Westbound |  |  |  |  |  | Kildare Rd <br> Northbound |  |  |  |  |  | Kildare Rd Southbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { Tpp. } \\ & \text { Tol } \end{aligned}$ | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. Total | Int. Total |
| 3:45 PM | 1 | 1 | 26 | 14 | 3 | 42 | 0 | 2 | 1 | 1 | 1 | 4 | 0 | 2 | 0 | 21 | 0 | 23 | 0 | 1 | 43 | 10 | 0 | 54 | 123 |
| 4:00 PM | 0 | 12 | 12 | 5 | 2 | 29 | 0 | 6 | 1 | 3 | 0 | 10 | 1 | 3 | 12 | 6 | 0 | 22 | 0 | 1 | 41 | 5 | 0 | 47 | 108 |
| 4:15 PM | 0 | 3 | 9 | 4 | 0 | 16 | 2 | 6 | 4 | 2 | 0 | 14 | 0 | 0 | 0 | 6 | 0 | 6 | 0 | 3 | 29 | 8 | 0 | 40 | 76 |
| 4:30 PM | 0 | 0 | 12 | 8 | 0 | 20 | 1 | 3 | 4 | 1 | 0 | 9 | 0 | 2 | 1 | 12 | 0 | 15 | 0 | 1 | 34 | 9 | 0 | 44 | 88 |
| Total | 1 | 16 | 59 | 31 | 5 | 107 | 3 | 17 | 10 | 7 | 1 | 37 | 1 | 7 | 13 | 45 | 0 | 66 | 0 | 6 | 147 | 32 | 0 | 185 | 395 |
| Approach \% | 0.9 | 15.0 | 55.1 | 29.0 | - | - | 8.1 | 45.9 | 27.0 | 18.9 | - | - | 1.5 | 10.6 | 19.7 | 68.2 | - | - | 0.0 | 3.2 | 79.5 | 17.3 | - | - | - |
| Total \% | 0.3 | 4.1 | 14.9 | 7.8 | - | 27.1 | 0.8 | 4.3 | 2.5 | 1.8 | - | 9.4 | 0.3 | 1.8 | 3.3 | 11.4 | - | 16.7 | 0.0 | 1.5 | 37.2 | 8.1 | - | 46.8 | - |
| PHF | 0.250 | 0.333 | 0.567 | 0.554 | - | 0.637 | 0.375 | 0.708 | 0.625 | 0.583 | - | 0.661 | 0.250 | 0.583 | 0.271 | 0.536 | - | 0.717 | 0.000 | 0.500 | 0.855 | 0.800 | $-$ | 0.856 | 0.803 |
| Lights | 1 | 14 | 55 | 26 | - | 96 | 3 | 17 | 10 | 7 | - | 37 | 1 | 7 | 13 | 40 | - | 61 | 0 | 5 | 143 | 25 | - | 173 | 367 |
| \% Lights | 100.0 | 87.5 | 93.2 | 83.9 | - | 89.7 | 100.0 | 100.0 | 100.0 | 100.0 | - | 100.0 | 100.0 | 100.0 | 100.0 | 88.9 | - | 92.4 | - | 83.3 | 97.3 | 78.1 | - | 93.5 | 92.9 |
| Buses | 0 | 0 | 0 | 1 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 1 | - | 1 | 0 | 0 | 0 | 3 | - | 3 | 5 |
| \% Buses | 0.0 | 0.0 | 0.0 | 3.2 | - | 0.9 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | 2.2 | - | 1.5 | - | 0.0 | 0.0 | 9.4 | - | 1.6 | 1.3 |
| Single-Unit Trucks | 0 | 2 | 3 | 1 | - | 6 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 1 | - | 1 | 0 | 0 | 2 | 2 | - | 4 | 11 |
| $\begin{gathered} \text { \% Single-Unit } \\ \text { Trucks } \\ \hline \end{gathered}$ | 0.0 | 12.5 | 5.1 | 3.2 | - | 5.6 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | 2.2 | - | 1.5 | - | 0.0 | 1.4 | 6.3 | - | 2.2 | 2.8 |
| Articulated Trucks | 0 | 0 | 1 | 2 | - | 3 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 3 | - | 3 | 0 | 1 | 2 | 2 | - | 5 | 11 |
| \% Articulated Trucks | 0.0 | 0.0 | 1.7 | 6.5 | - | 2.8 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | 6.7 | - | 4.5 | - | 16.7 | 1.4 | 6.3 | - | 2.7 | 2.8 |
| Bicycles on Road | 0 | 0 | 0 | 1 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | $\checkmark$ | 0 | 1 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \\ \hline \end{gathered}$ | 0.0 | 0.0 | 0.0 | 3.2 | - | 0.9 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.3 |
| Pedestrians | - | - | - | - | 5 | - | - | - | - | - | 1 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

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Count Name: Kildare Rd with 47th St TMC Site Code:
Slart Date: 05/18/2022
Page No: 1

| Start Time | 47th St <br> Eastbound |  |  |  |  |  | 47th St <br> Westbound |  |  |  |  |  | ent |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | Northbound Approach Northbound | Kildare Rd <br> Southbound |  |  |  |  |  | Int. Total |
|  | U-Turn | Left | Thru | Right | Peds | App. <br> Total |  |  |  |  |  |  | U-Turn |  | Left |  | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. Total |
| 6:00 AM | 0 | 15 | 68 | 1 | 1 | 84 | 0 | 1 | 96 | 5 | 0 | 102 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 1 | 6 | 1 | 13 | 199 |
| 6:15 AM | 0 | 19 | 79 | 4 | 1 | 102 | 0 | 3 | 81 | 9 | 0 | 93 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 8 | 1 | 11 | 206 |
| 6:30 AM | 0 | 16 | 78 | 2 | 1 | 96 | 0 | 2 | 81 | 14 | 0 | 97 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 3 | 1 | 5 | 198 |
| 6:45 AM | 0 | 39 | 94 | 3 | 2 | 136 | 0 | 1 | 95 | 24 | 1 | 120 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 8 | 0 | 3 | 0 | 11 | 267 |
| Hourly Total | 0 | 89 | 319 | 10 | 5 | 418 | 0 | 7 | 353 | 52 | 1 | 412 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 17 | 3 | 20 | 3 | 40 | 870 |
| 7:00 AM | 0 | 47 | 117 | 2 | 2 | 166 | 0 | 1 | 101 | 43 | 2 | 145 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 11 | 4 | 6 | 2 | 21 | 332 |
| 7:15 AM | 0 | 57 | 71 | 6 | 25 | 134 | 0 | 3 | 81 | 70 | 19 | 154 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 9 | 1 | 9 | 18 | 19 | 307 |
| 7:30 AM | 0 | 44 | 53 | 15 | 85 | 112 | 0 | 2 | 53 | 64 | 123 | 119 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 93 | 0 | 231 |
| 7:45 AM | 0 | 48 | 99 | 10 | 60 | 157 | 0 | 6 | 61 | 64 | 90 | 131 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 87 | 0 | 288 |
| Hourly Total | 0 | 196 | 340 | 33 | 172 | 569 | 0 | 12 | 296 | 241 | 234 | 549 | 0 | 0 | 0 | 0 | 15 | 0 | 0 | 20 | 5 | 15 | 200 | 40 | 1158 |
| 8:00 AM | 0 | 64 | 108 | 8 | 7 | 180 | 0 | 1 | 91 | 71 | 24 | 163 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 23 | 11 | 17 | 18 | 51 | 394 |
| 8:15 AM | 0 | 30 | 99 | 2 | 1 | 131 | 0 | 5 | 107 | 26 | 9 | 138 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 16 | 3 | 14 | 2 | 33 | 302 |
| 8:30 AM | 0 | 30 | 101 | 5 | 3 | 136 | 0 | 3 | 88 | 18 | 4 | 109 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 6 | 2 | 9 | 10 | 17 | 262 |
| 8:45 AM | 0 | 26 | 103 | 7 | 2 | 136 | 0 | 0 | 81 | 10 | 0 | 91 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 2 | 3 | 3 | 1 | 8 | 235 |
| Hourly Total | 0 | 150 | 411 | 22 | 13 | 583 | 0 | 9 | 367 | 125 | 37 | 501 | 0 | 0 | 0 | 0 | 17 | 0 | 0 | 47 | 19 | 43 | 31 | 109 | 1193 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | , | - | - |
| 3:00 PM | 0 | 9 | 84 | 7 | 0 | 100 | 0 | 5 | 103 | 9 | 4 | 117 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 12 | 5 | 29 | 2 | 46 | 263 |
| 3:15 PM | 0 | 10 | 102 | 7 | 2 | 119 | 0 | 6 | 117 | 7 | 3 | 130 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 10 | 7 | 19 | 2 | 36 | 285 |
| 3:30 PM | 0 | 14 | 102 | 5 | 2 | 121 | 1 | 9 | 123 | 5 | 2 | 138 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 22 | 17 | 49 | 2 | 88 | 347 |
| 3:45 PM | 0 | 4 | 122 | 4 | 7 | 130 | 0 | 4 | 140 | 3 | 8 | 147 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 44 | 20 | 38 | 4 | 102 | 379 |
| Hourly Total | 0 | 37 | 410 | 23 | 11 | 470 | 1 | 24 | 483 | 24 | 17 | 532 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 88 | 49 | 135 | 10 | 272 | 1274 |
| 4:00 PM | 0 | 12 | 149 | 9 | 2 | 170 | 0 | 4 | 138 | 6 | 0 | 148 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 21 | 10 | 34 | 1 | 65 | 383 |
| 4:15 PM | 0 | 5 | 94 | 3 | 0 | 102 | 0 | 7 | 129 | 0 | 1 | 136 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 11 | 7 | 22 | 2 | 40 | 278 |
| 4:30 PM | 0 | 11 | 131 | 6 | 0 | 148 | 0 | 4 | 164 | 6 | 0 | 174 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 23 | 11 | 20 | 0 | 54 | 376 |
| 4:45 PM | 0 | 14 | 120 | 4 | 2 | 138 | 0 | 8 | 157 | 4 | 0 | 169 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 12 | 15 | 17 | 1 | 44 | 351 |
| Hourly Total | 0 | 42 | 494 | 22 | 4 | 558 | 0 | 23 | 588 | 16 | 1 | 627 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 67 | 43 | 93 | 4 | 203 | 1388 |
| 5:00 PM | 0 | 6 | 147 | 5 | 0 | 158 | 0 | 5 | 149 | 1 | 1 | 155 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 25 | 8 | 29 | 0 | 62 | 375 |
| 5:15 PM | 0 | 7 | 135 | 5 | 0 | 147 | 0 | 3 | 134 | 4 | 1 | 141 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 9 | 19 | 2 | 45 | 333 |
| 5:30 PM | 0 | 7 | 117 | 6 | 0 | 130 | 0 | 7 | 142 | 5 | 0 | 154 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 7 | 9 | 14 | 0 | 30 | 314 |
| 5:45 PM | 0 | 8 | 121 | 8 | 0 | 137 | 0 | 5 | 133 | 2 | 1 | 140 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 12 | 10 | 18 | 0 | 40 | 317 |
| Hourly Total | 0 | 28 | 520 | 24 | 0 | 572 | 0 | 20 | 558 | 12 | 3 | 590 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 61 | 36 | 80 | 2 | 177 | 1339 |
| Grand Total | 0 | 542 | 2494 | 134 | 205 | 3170 | 1 | 95 | 2645 | 470 | 293 | 3211 | 0 | 0 | 0 | 0 | 72 | 0 | 0 | 300 | 155 | 386 | 250 | 841 | 7222 |
| Approach \% | 0.0 | 17.1 | 78.7 | 4.2 | - | - | 0.0 | 3.0 | 82.4 | 14.6 | - | - | 0.0 | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 35.7 | 18.4 | 45.9 | - | - | - |
| Total \% | 0.0 | 7.5 | 34.5 | 1.9 | - | 43.9 | 0.0 | 1.3 | 36.6 | 6.5 | - | 44.5 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 4.2 | 2.1 | 5.3 | - | 11.6 | - |
| Lights | 0 | 524 | 2333 | 130 | - | 2987 | 1 | 90 | 2478 | 462 | - | 3031 | 0 | 0 | 0 | 0 | - | 0 | 0 | 281 | 155 | 352 | - | 788 | 6806 |


| \% Lights | - | 96.7 | 93.5 | 97.0 | - | 94.2 | 100.0 | 94.7 | 93.7 | 98.3 | - | 94.4 | - | - | - | - | - | - | - | 93.7 | 100.0 | 91.2 | - | 93.7 | 94.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Buses | 0 | 0 | 26 | 2 | - | 28 | 0 | 4 | 25 | 3 | - | 32 | 0 | 0 | 0 | 0 | - | 0 | 0 | 6 | 0 | 4 | - | 10 | 70 |
| \% Buses | - | 0.0 | 1.0 | 1.5 | - | 0.9 | 0.0 | 4.2 | 0.9 | 0.6 | - | 1.0 | - | - | - | - | - | - | - | 2.0 | 0.0 | 1.0 | - | 1.2 | 1.0 |
| Single-Unit Trucks | 0 | 5 | 92 | 2 | - | 99 | 0 | 0 | 81 | 3 | - | 84 | 0 | 0 | 0 | 0 | - | 0 | 0 | 5 | 0 | 20 | - | 25 | 208 |
| \% Single-Unit Trucks | - | 0.9 | 3.7 | 1.5 | - | 3.1 | 0.0 | 0.0 | 3.1 | 0.6 | - | 2.6 | - | - | - | - | - | - | - | 1.7 | 0.0 | 5.2 | - | 3.0 | 2.9 |
| Articulated Trucks | 0 | 13 | 41 | 0 | - | 54 | 0 | 1 | 61 | 2 | - | 64 | 0 | 0 | 0 | 0 | - | 0 | 0 | 7 | 0 | 10 | - | 17 | 135 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 2.4 | 1.6 | 0.0 | - | 1.7 | 0.0 | 1.1 | 2.3 | 0.4 | - | 2.0 | - | - | - | - | - | - | - | 2.3 | 0.0 | 2.6 | - | 2.0 | 1.9 |
| Bicycles on Road | 0 | 0 | 2 | 0 | - | 2 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 1 | 0 | 0 | - | 1 | 3 |
| \% Bicycles on Road | - | 0.0 | 0.1 | 0.0 | - | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | - | - | - | - | - | - | - | 0.3 | 0.0 | 0.0 | - | 0.1 | 0.0 |
| Pedestrians | - | - | - | - | 205 | - | - | - | - | - | 293 | - | - | - | - | - | 72 | - | - | - | - | - | 250 | - | - |
| \% Pedestrians | $-$ | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |

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Count Name: Kildare Rd with 47th St TMC Site Code:
Start Date: 05/18/2022
Page No: 3

Turning Movement Peak Hour Data (7:15 AM)

| Start Time | 47th St <br> Eastbound |  |  |  |  |  |  | Turn | West | St St ound | ent | eak | Hour | Data | 7.15 orthboun North | AM) <br> Approach ound |  |  | Kildare Rd Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. |  |
| 7:15 AM | 0 | 57 | 71 | 6 | 25 | 134 | 0 | 3 | 81 | 70 | 19 | 154 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 9 | 1 | 9 | 18 | 19 | 307 |
| 7:30 AM | 0 | 44 | 53 | 15 | 85 | 112 | 0 | 2 | 53 | 64 | 123 | 119 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 93 | 0 | 231 |
| 7:45 AM | 0 | 48 | 99 | 10 | 60 | 157 | 0 | 6 | 61 | 64 | 90 | 131 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 87 | 0 | 288 |
| 8:00 AM | 0 | 64 | 108 | 8 | 7 | 180 | 0 | 1 | 91 | 71 | 24 | 163 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 23 | 11 | 17 | 18 | 51 | 394 |
| Total | 0 | 213 | 331 | 39 | 177 | 583 | 0 | 12 | 286 | 269 | 256 | 567 | 0 | 0 | 0 | 0 | 18 | 0 | 0 | 32 | 12 | 26 | 216 | 70 | 1220 |
| Approach \% | 0.0 | 36.5 | 56.8 | 6.7 | - | - | 0.0 | 2.1 | 50.4 | 47.4 | - | - | 0.0 | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 45.7 | 17.1 | 37.1 | - | - | - |
| Total \% | 0.0 | 17.5 | 27.1 | 3.2 | - | 47.8 | 0.0 | 1.0 | 23.4 | 22.0 | - | 46.5 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 2.6 | 1.0 | 2.1 | - | 5.7 | - |
| PHF | 0.000 | 0.832 | 0.766 | 0.650 | - | 0.810 | 0.000 | 0.500 | 0.786 | 0.947 | - | 0.870 | 0.000 | 0.000 | 0.000 | 0.000 | - | 0.000 | 0.000 | 0.348 | 0.273 | 0.382 | - | 0.343 | 0.774 |
| Lights | 0 | 212 | 306 | 38 | - | 556 | 0 | 11 | 265 | 267 | - | 543 | 0 | 0 | 0 | 0 | - | 0 | 0 | 31 | 12 | 24 | - | 67 | 1166 |
| \% Lights | - | 99.5 | 92.4 | 97.4 | - | 95.4 | - | 91.7 | 92.7 | 99.3 | - | 95.8 | - | - | - | - | - | - | - | 96.9 | 100.0 | 92.3 | - | 95.7 | 95.6 |
| Buses | 0 | 0 | 2 | 0 | - | 2 | 0 | 0 | 2 | 1 | - | 3 | 0 | 0 | 0 | 0 | - | 0 | 0 | 1 | 0 | 0 | - | 1 | 6 |
| \% Buses | - | 0.0 | 0.6 | 0.0 | - | 0.3 | - | 0.0 | 0.7 | 0.4 | - | 0.5 | - | - | - | - | - | - | - | 3.1 | 0.0 | 0.0 | - | 1.4 | 0.5 |
| Single-Unit Trucks | 0 | 0 | 10 | 1 | - | 11 | 0 | 0 | 10 | 1 | - | 11 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 2 | - | 2 | 24 |
| \% Single-Unit Trucks | - | 0.0 | 3.0 | 2.6 | - | 1.9 | - | 0.0 | 3.5 | 0.4 | - | 1.9 | - | - | - | - | - | . | - | 0.0 | 0.0 | 7.7 | - | 2.9 | 2.0 |
| Articulated Trucks | 0 | 1 | 13 | 0 | - | 14 | 0 | 1 | 9 | 0 | - | 10 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 24 |
| \% Articulated Trucks | - | 0.5 | 3.9 | 0.0 | - | 2.4 | - | 8.3 | 3.1 | 0.0 | - | 1.8 | - | . | - | - | - | - | . | 0.0 | 0.0 | 0.0 | - | 0.0 | 2.0 |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 |
| $\begin{gathered} \% \text { Bicycles on } \\ \text { Road } \end{gathered}$ | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | - | . | . | - | - | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 |
| Pedestrians | - | - | - | - | 177 | - | - | - | - | - | 256 | - | - | - | - | - | 18 | $\cdot$ | - | - | - | - | 216 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |

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Count Name: Kildare Rd with 47th St TMC Site Code:
Slart Date: 05/18/2022
Page No: 4

Turning Movement Peak Hour Data (3:45 PM)

| Start Time | 47th St <br> Eastbound |  |  |  |  |  | 47th St <br> Westbound |  |  |  |  |  | Northbound Approach Northbound |  |  |  |  |  | Kildare Rd Southbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App } \\ & \text { Total } \end{aligned}$ | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { Tpp. } \\ & \text { Tot } \end{aligned}$ | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { Appi } \\ & \text { Total } \end{aligned}$ | Int. Total |
| 3:45 PM | 0 | 4 | 122 | 4 | 7 | 130 | 0 | 4 | 140 | 3 | 8 | 147 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 44 | 20 | 38 | 4 | 102 | 379 |
| 4:00 PM | 0 | 12 | 149 | 9 | 2 | 170 | 0 | 4 | 138 | 6 | 0 | 148 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 21 | 10 | 34 | 1 | 65 | 383 |
| 4:15 PM | 0 | 5 | 94 | 3 | 0 | 102 | 0 | 7 | 129 | 0 | 1 | 136 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 11 | 7 | 22 | 2 | 40 | 278 |
| 4:30 PM | 0 | 11 | 131 | 6 | 0 | 148 | 0 | 4 | 164 | 6 | 0 | 174 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 23 | 11 | 20 | 0 | 54 | 376 |
| Total | 0 | 32 | 496 | 22 | 9 | 550 | 0 | 19 | 571 | 15 | 9 | 605 | 0 | 0 | 0 | 0 | 14 | 0 | 0 | 99 | 48 | 114 | 7 | 261 | 1416 |
| Approach \% | 0.0 | 5.8 | 90.2 | 4.0 | - | - | 0.0 | 3.1 | 94.4 | 2.5 | - | - | 0.0 | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 37.9 | 18.4 | 43.7 | - | - | - |
| Total \% | 0.0 | 2.3 | 35.0 | 1.6 | - | 38.8 | 0.0 | 1.3 | 40.3 | 1.1 | - | 42.7 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 7.0 | 3.4 | 8.1 | - | 18.4 | - |
| PHF | 0.000 | 0.667 | 0.832 | 0.611 | - | 0.809 | 0.000 | 0.679 | 0.870 | 0.625 | - | 0.869 | 0.000 | 0.000 | 0.000 | 0.000 | - | 0.000 | 0.000 | 0.563 | 0.600 | 0.750 | - | 0.640 | 0.924 |
| Lights | 0 | 29 | 468 | 21 | - | 518 | 0 | 18 | 536 | 14 | - | 568 | 0 | 0 | 0 | 0 | - | 0 | 0 | 95 | 48 | 110 | - | 253 | 1339 |
| \% Lights | - | 90.6 | 94.4 | 95.5 | - | 94.2 | - | 94.7 | 93.9 | 93.3 | - | 93.9 | - | - | - | - | - | - | - | 96.0 | 100.0 | 96.5 | - | 96.9 | 94.6 |
| Buses | 0 | 0 | 5 | 0 | - | 5 | 0 | 1 | 6 | 0 | - | 7 | 0 | 0 | 0 | 0 | - | 0 | 0 | 1 | 0 | 0 | - | 1 | 13 |
| \% Buses | - | 0.0 | 1.0 | 0.0 | - | 0.9 | - | 5.3 | 1.1 | 0.0 | - | 1.2 | - | - | - | - | - | - | - | 1.0 | 0.0 | 0.0 | - | 0.4 | 0.9 |
| Single-Unit Trucks | 0 | 1 | 19 | 1 | - | 21 | 0 | 0 | 14 | 0 | - | 14 | 0 | 0 | 0 | 0 | - | 0 | 0 | 1 | 0 | 2 | - | 3 | 38 |
| \% Single-Unit Trucks | - | 3.1 | 3.8 | 4.5 | - | 3.8 | - | 0.0 | 2.5 | 0.0 | - | 2.3 | - | - | - | - | - | . | - | 1.0 | 0.0 | 1.8 | - | 1.1 | 2.7 |
| Articulated Trucks | 0 | 2 | 4 | 0 | - | 6 | 0 | 0 | 15 | 1 | - | 16 | 0 | 0 | 0 | 0 | - | 0 | 0 | 2 | 0 | 2 | - | 4 | 26 |
| \% Articulated Trucks | - | 6.3 | 0.8 | 0.0 | - | 1.1 | - | 0.0 | 2.6 | 6.7 | - | 2.6 | - | - | - | - | - | - | - | 2.0 | 0.0 | 1.8 | - | 1.5 | 1.8 |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 |
| $\begin{gathered} \% \text { Bicycles on } \\ \text { Road } \end{gathered}$ | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | . | - | . | . | - | . | . | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 |
| Pedestrians | - | - | - | - | 9 | - | - | - | - | - | 9 | - | - | - | - | - | 14 | - | - | - | - | - | 7 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |

## (847)518-9990

Count Name: Pulaski Rd with Ann Lurie P Site Code:
Page No: 05/18/2022
Page No: 1

Turning Movement Data


| Articulated Trucks | 0 | 57 | 14 | - | 71 | 0 | 10 | 157 | - | 167 | 0 | 88 | 75 | - | 163 | 401 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% Articulated Trucks | - | 11.0 | 3.2 | - | 7.4 | 0.0 | 1.5 | 2.4 | - | 2.3 | - | 1.9 | 14.9 | - | 3.1 | 3.0 |
| Bicycles on Road | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | - | 1 | 0 | 1 | 0 | - | 1 | 2 |
| \% Bicycles on Road | - | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | - | 0.0 | 0.0 |
| Pedestrians | - | - | - | 30 | - | - | - | - | 3 | - | - | - | - | 28 | - | - |
| \% Pedestrians | - | - | - | 100.0 | - | - | - | - | 100.0 | - | - | - | - | 100.0 | - | - |

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Count Name: Pulaski Rd with Ann Lurie PI Site Code:
Start Nate: 05/18/2022
Page No: 3

Turning Movement Peak Hour Data (7:15 AM)

| Start Time | Ann Lurie PI Eastbound |  |  |  |  | 崖 | ( | , | a | AIV) | Pulaski Rd <br> Southbound |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Pulaski Rd <br> Northbound |  |  |  |  |  |  |  |  |  |  |
|  | U-Turn | Left | Right | Peds | App. Total | U-Turn | Left | Thru | Peds | App. Total | U-Turn | Thru | Right | Peds | App. Total |  |
| 7:15 AM | 0 | 32 | 14 | 0 | 46 | 0 | 26 | 348 | 0 | 374 | 0 | 186 | 31 | 0 | 217 | 637 |
| 7:30 AM | 0 | 44 | 10 | 0 | 54 | 0 | 25 | 379 | 0 | 404 | 0 | 178 | 46 | 1 | 224 | 682 |
| 7:45 AM | 0 | 43 | 6 | 0 | 49 | 0 | 34 | 396 | 0 | 430 | 0 | 181 | 40 | 0 | 221 | 700 |
| 8:00 AM | 0 | 37 | 19 | 0 | 56 | 0 | 41 | 345 | 0 | 386 | 0 | 219 | 42 | 2 | 261 | 703 |
| Total | 0 | 156 | 49 | 0 | 205 | 0 | 126 | 1468 | 0 | 1594 | 0 | 764 | 159 | 3 | 923 | 2722 |
| Approach \% | 0.0 | 76.1 | 23.9 | - | - | 0.0 | 7.9 | 92.1 | - | - | 0.0 | 82.8 | 17.2 | - | - | - |
| Total \% | 0.0 | 5.7 | 1.8 | - | 7.5 | 0.0 | 4.6 | 53.9 | - | 58.6 | 0.0 | 28.1 | 5.8 | - | 33.9 | $\checkmark$ |
| PHF | 0.000 | 0.886 | 0.645 | - | 0.915 | 0.000 | 0.768 | 0.927 | - | 0.927 | 0.000 | 0.872 | 0.864 | - | 0.884 | 0.968 |
| Lights | 0 | 124 | 42 | - | 166 | 0 | 116 | 1363 | - | 1479 | 0 | 718 | 122 | - | 840 | 2485 |
| \% Lights | - | 79.5 | 85.7 | - | 81.0 | - | 92.1 | 92.8 | - | 92.8 | - | 94.0 | 76.7 | - | 91.0 | 91.3 |
| Buses | 0 | 2 | 0 | - | 2 | 0 | 0 | 5 | - | 5 | 0 | 3 | 1 | $\checkmark$ | 4 | 11 |
| \% Buses | - | 1.3 | 0.0 | - | 1.0 | - | 0.0 | 0.3 | - | 0.3 | - | 0.4 | 0.6 | - | 0.4 | 0.4 |
| Single-Unit Trucks | 0 | 17 | 2 | - | 19 | 0 | 5 | 63 | - | 68 | 0 | 24 | 19 | - | 43 | 130 |
| \% Single-Unit Trucks | - | 10.9 | 4.1 | - | 9.3 | - | 4.0 | 4.3 | - | 4.3 | - | 3.1 | 11.9 | - | 4.7 | 4.8 |
| Articulated Trucks | 0 | 13 | 5 | $\checkmark$ | 18 | 0 | 5 | 37 | - | 42 | 0 | 19 | 17 | - | 36 | 96 |
| \% Articulated Trucks | - | 8.3 | 10.2 | - | 8.8 | - | 4.0 | 2.5 | - | 2.6 | - | 2.5 | 10.7 | - | 3.9 | 3.5 |
| Bicycles on Road | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 |
| \% Bicycles on Road | - | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | - | 0.0 | 0.0 |
| Pedestrians | - | - | - | 0 | - | $-$ | - | - | 0 | - | - | - | - | 3 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | - | - | - | - | 100.0 | - | - |

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Count Name: Pulaski Rd with Ann Lurie PI Site Code:
Start Date: 05/18/2022
Page No: 4

Turning Movement Peak Hour Data (3:45 PM)

| Start Time | Turning Movement Peak Hour Data (3:45 PM) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Ann Lurie PI <br> Eastbound |  |  |  |  | Pulaski RdNorthbound |  |  |  |  | Pulaski Rd Southbound |  |  |  |  | Int. Total |
|  | U-Turn | Left | Right | Peds | App. Total | U-Turn | Left | Thru | Peds | App. Total | U-Turn | Thru | Right | Peds | App. Total |  |
| 3:45 PM | 0 | 28 | 32 | 1 | 60 | 0 | 55 | 304 | 0 | 359 | 0 | 316 | 17 | 0 | 333 | 752 |
| 4:00 PM | 0 | 26 | 33 | 4 | 59 | 1 | 40 | 334 | 0 | 375 | 0 | 326 | 20 | 5 | 346 | 780 |
| 4:15 PM | 0 | 15 | 30 | 5 | 45 | 0 | 28 | 291 | 0 | 319 | 0 | 286 | 15 | 3 | 301 | 665 |
| 4:30 PM | 0 | 21 | 33 | 4 | 54 | 0 | 40 | 332 | 0 | 372 | 0 | 314 | 12 | 4 | 326 | 752 |
| Total | 0 | 90 | 128 | 14 | 218 | 1 | 163 | 1261 | 0 | 1425 | 0 | 1242 | 64 | 12 | 1306 | 2949 |
| Approach \% | 0.0 | 41.3 | 58.7 | - | - | 0.1 | 11.4 | 88.5 | - | - | 0.0 | 95.1 | 4.9 | - | - | - |
| Total \% | 0.0 | 3.1 | 4.3 | - | 7.4 | 0.0 | 5.5 | 42.8 | - | 48.3 | 0.0 | 42.1 | 2.2 | - | 44.3 | - |
| PHF | 0.000 | 0.804 | 0.970 | - | 0.908 | 0.250 | 0.741 | 0.944 | - | 0.950 | 0.000 | 0.952 | 0.800 | - | 0.944 | 0.945 |
| Lights | 0 | 80 | 126 | - | 206 | 1 | 158 | 1193 | - | 1352 | 0 | 1208 | 41 | - | 1249 | 2807 |
| \% Lights | - | 88.9 | 98.4 | - | 94.5 | 100.0 | 96.9 | 94.6 | - | 94.9 | - | 97.3 | 64.1 | - | 95.6 | 95.2 |
| Buses | 0 | 0 | 0 | - | 0 | 0 | 0 | 12 | - | 12 | 0 | 6 | 2 | - | 8 | 20 |
| \% Buses | - | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 1.0 | - | 0.8 | - | 0.5 | 3.1 | - | 0.6 | 0.7 |
| Single-Unit Trucks | 0 | 5 | 0 | - | 5 | 0 | 3 | 29 | - | 32 | 0 | 9 | 8 | - | 17 | 54 |
| \% Single-Unit Trucks | - | 5.6 | 0.0 | - | 2.3 | 0.0 | 1.8 | 2.3 | - | 2.2 | - | 0.7 | 12.5 | - | 1.3 | 1.8 |
| Articulated Trucks | 0 | 5 | 2 | - | 7 | 0 | 2 | 27 | - | 29 | 0 | 19 | 13 | - | 32 | 68 |
| \% Articulated Trucks | - | 5.6 | 1.6 | - | 3.2 | 0.0 | 1.2 | 2.1 | - | 2.0 | - | 1.5 | 20.3 | - | 2.5 | 2.3 |
| Bicycles on Road | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 |
| \% Bicycles on Road | - | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | - | 0.0 | 0.0 |
| Pedestrians | - | - | - | 14 | - | - | - | - | 0 | - | - | - | - | 12 | - | - |
| \% Pedestrians | - | - | - | 100.0 | - | - | - | - | - | - | - | - | - | 100.0 | - | - |

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Count Name: W Ann Lurie PI with Kildare Ave TMC
Site Code:
Start Date: 05/18/2022
Page No: 1

| Start Time | Turning Movement Data |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Ann Lurie PI Eastbound |  |  |  |  |  | Ann Lurie PI Westbound |  |  |  |  |  | Kildare Ave Northbound |  |  |  |  |  | Kildare Ave Southbound |  |  |  |  |  | Int. Total |
|  | U-Turn | Left | Thru | Right | Peds | App. <br> Tota | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { Tpp. } \\ & \text { Tot } \end{aligned}$ | U-Turn | Left | Thru | Right | Peds | App. |  |
| 6:00 AM | 0 | 2 | 8 | 2 | 0 | 12 | 0 | 13 | 8 | 0 | 0 | 21 | 0 | 2 | 16 | 8 | 0 | 26 | 0 | 0 | 7 | 0 | 1 | 7 | 66 |
| 6:15 AM | 0 | 0 | 6 | 5 | 0 | 11 | 0 | 15 | 5 | 1 | 0 | 21 | 0 | 3 | 14 | 6 | 0 | 23 | 0 | 4 | 11 | 0 | 0 | 15 | 70 |
| 6:30 AM | 0 | 0 | 6 | 3 | 0 | 9 | 0 | 18 | 6 | 2 | 0 | 26 | 0 | 3 | 38 | 19 | 0 | 60 | 0 | 2 | 5 | 1 | 0 | 8 | 103 |
| 6:45 AM | 0 | 0 | 7 | 3 | 0 | 10 | 0 | 27 | 4 | 1 | 1 | 32 | 0 | 4 | 50 | 22 | 0 | 76 | 0 | 1 | 8 | 3 | 1 | 12 | 130 |
| Hourly Total | 0 | 2 | 27 | 13 | 0 | 42 | 0 | 73 | 23 | 4 | 1 | 100 | 0 | 12 | 118 | 55 | 0 | 185 | 0 | 7 | 31 | 4 | 2 | 42 | 369 |
| 7:00 AM | 0 | 1 | 6 | 3 | 0 | 10 | 0 | 21 | 6 | 0 | 0 | 27 | 0 | 1 | 52 | 32 | 0 | 85 | 0 | 0 | 21 | 0 | 0 | 21 | 143 |
| 7:15 AM | 0 | 1 | 5 | 2 | 0 | 8 | 0 | 18 | 3 | 3 | 0 | 24 | 0 | 4 | 48 | 53 | 0 | 105 | 0 | 1 | 16 | 1 | 0 | 18 | 155 |
| 7:30 AM | 0 | 1 | 6 | 3 | 0 | 10 | 0 | 27 | 5 | 3 | 0 | 35 | 0 | 2 | 46 | 59 | 0 | 107 | 0 | 1 | 15 | 1 | 0 | 17 | 169 |
| 7:45 AM | 0 | 0 | 4 | 0 | 0 | 4 | 1 | 34 | 8 | 2 | 0 | 45 | 0 | 6 | 39 | 48 | 0 | 93 | 0 | 0 | 14 | 1 | 0 | 15 | 157 |
| Hourly Total | 0 | 3 | 21 | 8 | 0 | 32 | 1 | 100 | 22 | 8 | 0 | 131 | 0 | 13 | 185 | 192 | 0 | 390 | 0 | 2 | 66 | 3 | 0 | 71 | 624 |
| 8:00 AM | 0 | 0 | 9 | 3 | 0 | 12 | 0 | 32 | 5 | 3 | 0 | 40 | 0 | 6 | 29 | 41 | 0 | 76 | 0 | 3 | 19 | 2 | 0 | 24 | 152 |
| 8:15 AM | 0 | 0 | 12 | 2 | 0 | 14 | 0 | 22 | 9 | 3 | 0 | 34 | 0 | 2 | 31 | 22 | 0 | 55 | 0 | 1 | 9 | 3 | 0 | 13 | 116 |
| 8:30 AM | 0 | 2 | 7 | 1 | 0 | 10 | 0 | 18 | 4 | 1 | 0 | 23 | 0 | 4 | 33 | 23 | 0 | 60 | 0 | 1 | 11 | 1 | 0 | 13 | 106 |
| 8:45 AM | 0 | 0 | 4 | 2 | 0 | 6 | 0 | 20 | 5 | 3 | 1 | 28 | 0 | 3 | 13 | 24 | 1 | 40 | 0 | 1 | 7 | 0 | 0 | 8 | 82 |
| Hourly Total | 0 | 2 | 32 | 8 | 0 | 42 | 0 | 92 | 23 | 10 | 1 | 125 | 0 | 15 | 106 | 110 | 1 | 231 | 0 | 6 | 46 | 6 | 0 | 58 | 456 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 3:00 PM | 0 | 6 | 14 | 10 | 4 | 30 | 0 | 13 | 7 | 1 | 0 | 21 | 0 | 3 | 12 | 5 | 0 | 20 | 1 | 1 | 11 | 1 | 0 | 14 | 85 |
| 3:15 PM | 0 | 4 | 12 | 12 | 0 | 28 | 0 | 30 | 3 | 2 | 0 | 35 | 0 | 1 | 20 | 2 | 2 | 23 | 0 | 4 | 14 | 1 | 0 | 19 | 105 |
| 3:30 PM | 0 | 0 | 14 | 14 | 0 | 28 | 0 | 13 | 9 | 2 | 0 | 24 | 1 | 1 | 22 | 17 | 0 | 41 | 0 | 8 | 14 | 0 | 1 | 22 | 115 |
| 3:45 PM | 0 | 8 | 20 | 16 | 0 | 44 | 0 | 17 | 4 | 2 | 1 | 23 | 0 | 0 | 14 | 12 | 1 | 26 | 0 | 3 | 9 | 0 | 0 | 12 | 105 |
| Hourly Total | 0 | 18 | 60 | 52 | 4 | 130 | 0 | 73 | 23 | 7 | 1 | 103 | 1 | 5 | 68 | 36 | 3 | 110 | 1 | 16 | 48 | 2 | 1 | 67 | 410 |
| 4:00 PM | 0 | 2 | 11 | 15 | 1 | 28 | 0 | 21 | 2 | 2 | 0 | 25 | 0 | 3 | 25 | 13 | 1 | 41 | 0 | 2 | 10 | 0 | 0 | 12 | 106 |
| 4:15 PM | 0 | 2 | 3 | 1 | 0 | 6 | 0 | 24 | 0 | 1 | 0 | 25 | 0 | 1 | 10 | 6 | 0 | 17 | 0 | 1 | 11 | 0 | 0 | 12 | 60 |
| 4:30 PM | 0 | 0 | 4 | 3 | 1 | 7 | 0 | 18 | 0 | 1 | 0 | 19 | 0 | 3 | 11 | 14 | 0 | 28 | 0 | 0 | 12 | 0 | 0 | 12 | 66 |
| 4:45 PM | 0 | 0 | 6 | 3 | 0 | 9 | 0 | 17 | 5 | 2 | 0 | 24 | 0 | 2 | 7 | 11 | 0 | 20 | 0 | 0 | 13 | 1 | 0 | 14 | 67 |
| Hourly Total | 0 | 4 | 24 | 22 | 2 | 50 | 0 | 80 | 7 | 6 | 0 | 93 | 0 | 9 | 53 | 44 | 1 | 106 | 0 | 3 | 46 | 1 | 0 | 50 | 299 |
| 5:00 PM | 0 | 1 | 3 | 2 | 2 | 6 | 0 | 28 | 4 | 2 | 0 | 34 | 0 | 1 | 14 | 10 | 0 | 25 | 0 | 0 | 9 | 0 | 0 | 9 | 74 |
| 5:15 PM | 0 | 3 | 4 | 10 | 0 | 17 | 0 | 13 | 6 | 1 | 0 | 20 | 0 | 1 | 10 | 10 | 0 | 21 | 0 | 1 | 5 | 0 | 0 | 6 | 64 |
| 5:30 PM | 0 | 0 | 4 | 5 | 0 | 9 | 0 | 20 | 1 | 2 | 0 | 23 | 0 | 0 | 7 | 15 | 0 | 22 | 0 | 0 | 6 | 1 | 0 | 7 | 61 |
| 5:45 PM | 0 | 1 | 7 | 4 | 0 | 12 | 0 | 19 | 4 | 1 | 0 | 24 | 0 | 4 | 13 | 8 | 0 | 25 | 0 | 0 | 3 | 2 | 0 | 5 | 66 |
| Hourly Total | 0 | 5 | 18 | 21 | 2 | 44 | 0 | 80 | 15 | 6 | 0 | 101 | 0 | 6 | 44 | 43 | 0 | 93 | 0 | 1 | 23 | 3 | 0 | 27 | 265 |
| Grand Total | 0 | 34 | 182 | 124 | 8 | 340 | 1 | 498 | 113 | 41 | 3 | 653 | 1 | 60 | 574 | 480 | 5 | 1115 | 1 | 35 | 260 | 19 | 3 | 315 | 2423 |
| Approach \% | 0.0 | 10.0 | 53.5 | 36.5 | - | - | 0.2 | 76.3 | 17.3 | 6.3 | - | - | 0.1 | 5.4 | 51.5 | 43.0 | - | - | 0.3 | 11.1 | 82.5 | 6.0 | - | - | - |
| Total \% | 0.0 | 1.4 | 7.5 | 5.1 | - | 14.0 | 0.0 | 20.6 | 4.7 | 1.7 | - | 27.0 | 0.0 | 2.5 | 23.7 | 19.8 | - | 46.0 | 0.0 | 1.4 | 10.7 | 0.8 | - | 13.0 | $\checkmark$ |
| Lights | 0 | 33 | 99 | 104 | - | 236 | 0 | 412 | 49 | 15 | - | 476 | 1 | 40 | 543 | 433 | - | 1017 | 1 | 24 | 243 | 15 | - | 283 | 2012 |


| \% Lights | - | 97.1 | 54.4 | 83.9 | - | 69.4 | 0.0 | 82.7 | 43.4 | 36.6 | - | 72.9 | 100.0 | 66.7 | 94.6 | 90.2 | - | 91.2 | 100.0 | 68.6 | 93.5 | 78.9 | - | 89.8 | 83.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Buses | 0 | 0 | 0 | 2 | - | 2 | 0 | 12 | 0 | 0 | - | 12 | 0 | 0 | 2 | 4 | - | 6 | 0 | 0 | 3 | 0 | - | 3 | 23 |
| \% Buses | - | 0.0 | 0.0 | 1.6 | $-$ | 0.6 | 0.0 | 2.4 | 0.0 | 0.0 | - | 1.8 | 0.0 | 0.0 | 0.3 | 0.8 | - | 0.5 | 0.0 | 0.0 | 1.2 | 0.0 | - | 1.0 | 0.9 |
| Single-Unit Trucks | 0 | 0 | 42 | 10 | - | 52 | 0 | 36 | 36 | 4 | - | 76 | 0 | 11 | 18 | 13 | - | 42 | 0 | 2 | 11 | 1 | - | 14 | 184 |
| $\begin{gathered} \hline \text { \% Single-Unit } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 0.0 | 23.1 | 8.1 | - | 15.3 | 0.0 | 7.2 | 31.9 | 9.8 | - | 11.6 | 0.0 | 18.3 | 3.1 | 2.7 | - | 3.8 | 0.0 | 5.7 | 4.2 | 5.3 | - | 4.4 | 7.6 |
| Articulated Trucks | 0 | 1 | 40 | 7 | - | 48 | 1 | 37 | 28 | 22 | - | 88 | 0 | 9 | 11 | 29 | - | 49 | 0 | 9 | 3 | 3 | - | 15 | 200 |
| $\begin{gathered} \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 2.9 | 22.0 | 5.6 | - | 14.1 | 100.0 | 7.4 | 24.8 | 53.7 | - | 13.5 | 0.0 | 15.0 | 1.9 | 6.0 | - | 4.4 | 0.0 | 25.7 | 1.2 | 15.8 | - | 4.8 | 8.3 |
| Bicycles on Road | 0 | 0 | 1 | 1 | - | 2 | 0 | 1 | 0 | 0 | - | 1 | 0 | 0 | 0 | 1 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 4 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \\ \hline \end{gathered}$ | - | 0.0 | 0.5 | 0.8 | - | 0.6 | 0.0 | 0.2 | 0.0 | 0.0 | - | 0.2 | 0.0 | 0.0 | 0.0 | 0.2 | - | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.2 |
| Pedestrians | - | - | - | - | 8 | - | - | - | - | - | 3 | - | - | - | - | - | 5 | - | - | - | - | - | 3 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |

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Count Name: W Ann Lurie PI with Kildare Ave TMC
Site Code:
Date: 05/18/2022
Page No: 3

Turning Movement Peak Hour Data (7:15 AM)

| Start Time | Ann Lurie PI Eastbound |  |  |  |  |  | Ann Lurie PI Westbound |  |  |  |  |  | Kildare Ave Northbound |  |  |  |  |  | Kildare Ave Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \end{aligned}$ | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total |  |
| 7:15 AM | 0 | 1 | 5 | 2 | 0 | 8 | 0 | 18 | 3 | 3 | 0 | 24 | 0 | 4 | 48 | 53 |  | 105 | 0 | 1 | 16 | 1 | 0 | 18 | 155 |
| 7:30 AM | 0 | 1 | 6 | 3 | 0 | 10 | 0 | 27 | 5 | 3 | 0 | 35 | 0 | 2 | 46 | 59 | 0 | 107 | 0 | 1 | 15 | 1 | 0 | 17 | 169 |
| 7:45 AM | 0 | 0 | 4 | 0 | 0 | 4 | 1 | 34 | 8 | 2 | 0 | 45 | 0 | 6 | 39 | 48 | 0 | 93 | 0 | 0 | 14 | 1 | 0 | 15 | 157 |
| 8:00 AM | 0 | 0 | 9 | 3 | 0 | 12 | 0 | 32 | 5 | 3 | 0 | 40 | 0 | 6 | 29 | 41 |  | 76 | 0 | 3 | 19 | 2 | 0 | 24 | 152 |
| Total | 0 | 2 | 24 | 8 | 0 | 34 | 1 | 111 | 21 | 11 | 0 | 144 | 0 | 18 | 162 | 201 | 0 | 381 | 0 | 5 | 64 | 5 | 0 | 74 | 633 |
| Approach \% | 0.0 | 5.9 | 70.6 | 23.5 | - | - | 0.7 | 77.1 | 14.6 | 7.6 | - | - | 0.0 | 4.7 | 42.5 | 52.8 | - | - | 0.0 | 6.8 | 86.5 | 6.8 | - | - | - |
| Total \% | 0.0 | 0.3 | 3.8 | 1.3 | - | 5.4 | 0.2 | 17.5 | 3.3 | 1.7 | - | 22.7 | 0.0 | 2.8 | 25.6 | 31.8 | - | 60.2 | 0.0 | 0.8 | 10.1 | 0.8 | - | 11.7 | - |
| PHF | 0.000 | 0.500 | 0.667 | 0.667 | - | 0.708 | 0.250 | 0.816 | 0.656 | 0.917 | - | 0.800 | 0.000 | 0.750 | 0.844 | 0.852 | - | 0.890 | 0.000 | 0.417 | 0.842 | 0.625 | - | 0.771 | 0.936 |
| Lights | 0 | 1 | 5 | 6 | - | 12 | 0 | 96 | 8 | 2 | - | 106 | 0 | 13 | 156 | 184 | - | 353 | 0 | 1 | 62 | 4 | - | 67 | 538 |
| \% Lights | - | 50.0 | 20.8 | 75.0 | - | 35.3 | 0.0 | 86.5 | 38.1 | 18.2 | - | 73.6 | - | 72.2 | 96.3 | 91.5 | - | 92.7 | - | 20.0 | 96.9 | 80.0 | - | 90.5 | 85.0 |
| Buses | 0 | 0 | 0 | 0 | - | 0 | 0 | 2 | 0 | 0 | - | 2 | 0 | 0 | 0 | 3 | - | 3 | 0 | 0 | 0 | 0 | - | 0 | 5 |
| \% Buses | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 1.8 | 0.0 | 0.0 | - | 1.4 | - | 0.0 | 0.0 | 1.5 | - | 0.8 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.8 |
| Single-Unit Trucks | 0 | 0 | 15 | 0 | - | 15 | 0 | 7 | 9 | 1 | - | 17 | 0 | 3 | 5 | 5 | - | 13 | 0 | 0 | 2 | 0 | - | 2 | 47 |
| \% Single-Unit Trucks | . | 0.0 | 62.5 | 0.0 | - | 44.1 | 0.0 | 6.3 | 42.9 | 9.1 | - | 11.8 | - | 16.7 | 3.1 | 2.5 | - | 3.4 | - | 0.0 | 3.1 | 0.0 | - | 2.7 | 7.4 |
| Articulated Trucks | 0 | 1 | 4 | 2 | - | 7 | 1 | 5 | 4 | 8 | - | 18 | 0 | 2 | 1 | 9 | - | 12 | 0 | 4 | 0 | 1 | - | 5 | 42 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 50.0 | 16.7 | 25.0 | - | 20.6 | 100.0 | 4.5 | 19.0 | 72.7 | - | 12.5 | - | 11.1 | 0.6 | 4.5 | - | 3.1 | . | 80.0 | 0.0 | 20.0 | - | 6.8 | 6.6 |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 1 | 0 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 1 |
| $\begin{gathered} \% \text { Bicycles on } \\ \text { Road } \end{gathered}$ | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 | - | 0.7 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.2 |
| Pedestrians | $\cdot$ | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

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Count Name: W Ann Lurie PI with Kildare Ave TMC
Site Code:
Start Date: 05/18/2022
Page No: 4

Turning Movement Peak Hour Data (3:45 PM)

| Start Time | Ann Lurie PI Eastbound |  |  |  |  |  | Ann Lurie PI Westbound |  |  |  |  |  | Kildare Ave <br> Northbound |  |  |  |  |  | Kildare Ave Southbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | Int. Total |
| 3:45 PM | 0 | 8 | 20 | 16 | 0 | 44 | 0 | 17 | 4 | 2 | 1 | 23 | 0 | 0 | 14 | 12 | 1 | 26 | 0 | 3 | 9 | 0 | 0 | 12 | 105 |
| 4:00 PM | 0 | 2 | 11 | 15 | 1 | 28 | 0 | 21 | 2 | 2 | 0 | 25 | 0 | 3 | 25 | 13 | 1 | 41 | 0 | 2 | 10 | 0 | 0 | 12 | 106 |
| 4:15 PM | 0 | 2 | 3 | 1 | 0 | 6 | 0 | 24 | 0 | 1 | 0 | 25 | 0 | 1 | 10 | 6 | 0 | 17 | 0 | 1 | 11 | 0 | 0 | 12 | 60 |
| 4:30 PM | 0 | 0 | 4 | 3 | 1 | 7 | 0 | 18 | 0 | 1 | 0 | 19 | 0 | 3 | 11 | 14 | 0 | 28 | 0 | 0 | 12 | 0 | 0 | 12 | 66 |
| Total | 0 | 12 | 38 | 35 | 2 | 85 | 0 | 80 | 6 | 6 | 1 | 92 | 0 | 7 | 60 | 45 | 2 | 112 | 0 | 6 | 42 | 0 | 0 | 48 | 337 |
| Approach \% | 0.0 | 14.1 | 44.7 | 41.2 | - | - | 0.0 | 87.0 | 6.5 | 6.5 | - | - | 0.0 | 6.3 | 53.6 | 40.2 | - | - | 0.0 | 12.5 | 87.5 | 0.0 | - | - | - |
| Total \% | 0.0 | 3.6 | 11.3 | 10.4 | - | 25.2 | 0.0 | 23.7 | 1.8 | 1.8 | - | 27.3 | 0.0 | 2.1 | 17.8 | 13.4 | - | 33.2 | 0.0 | 1.8 | 12.5 | 0.0 | - | 14.2 | - |
| PHF | 0.000 | 0.375 | 0.475 | 0.547 | - | 0.483 | 0.000 | 0.833 | 0.375 | 0.750 | - | 0.920 | 0.000 | 0.583 | 0.600 | 0.804 | - | 0.683 | 0.000 | 0.500 | 0.875 | 0.000 | - | 1.000 | 0.795 |
| Lights | 0 | 12 | 31 | 33 | - | 76 | 0 | 59 | 5 | 1 | - | 65 | 0 | 2 | 57 | 43 | - | 102 | 0 | 6 | 40 | 0 | - | 46 | 289 |
| \% Lights | - | 100.0 | 81.6 | 94.3 | - | 89.4 | - | 73.8 | 83.3 | 16.7 | - | 70.7 | - | 28.6 | 95.0 | 95.6 | - | 91.1 | - | 100.0 | 95.2 | - | - | 95.8 | 85.8 |
| Buses | 0 | 0 | 0 | 0 | - | 0 | 0 | 2 | 0 | 0 | - | 2 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | 0 | - | 1 | 3 |
| \% Buses | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 2.5 | 0.0 | 0.0 | - | 2.2 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 2.4 | - | - | 2.1 | 0.9 |
| Single-Unit Trucks | 0 | 0 | 2 | 1 | - | 3 | 0 | 9 | 1 | 2 | - | 12 | 0 | 2 | 1 | 1 | - | 4 | 0 | 0 | 0 | 0 | - | 0 | 19 |
| \% Single-Unit Trucks | - | 0.0 | 5.3 | 2.9 | - | 3.5 | - | 11.3 | 16.7 | 33.3 | - | 13.0 | - | 28.6 | 1.7 | 2.2 | - | 3.6 | . | 0.0 | 0.0 | - | - | 0.0 | 5.6 |
| Articulated Trucks | 0 | 0 | 5 | 1 | - | 6 | 0 | 10 | 0 | 3 | - | 13 | 0 | 3 | 2 | 1 | - | 6 | 0 | 0 | 1 | 0 | - | 1 | 26 |
| $\begin{aligned} & \hline \text { \% Articulated } \\ & \text { Trucks } \\ & \hline \end{aligned}$ | - | 0.0 | 13.2 | 2.9 | - | 7.1 | - | 12.5 | 0.0 | 50.0 | - | 14.1 | - | 42.9 | 3.3 | 2.2 | - | 5.4 | - | 0.0 | 2.4 | - | - | 2.1 | 7.7 |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 |
| $\begin{gathered} \hline \text { \% Bicycles on } \\ \text { Road } \\ \hline \end{gathered}$ | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | - | - | 0.0 | 0.0 |
| Pedestrians | - | - | - | - | 2 | $\cdot$ | - | - | - | - | 1 | - | - | - | - | - | 2 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | - | - | - |

## Preliminary Site Plan



DATA:


ITE Trip Generation Worksheets

# General Light Industrial <br> (110) 

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday

## Setting/Location: General Urban/Suburban

Number of Studies: 37
Avg. 1000 Sq. Ft. GFA: 45
Directional Distribution: 50\% entering, 50\% exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 4.87 | $0.34-43.86$ | 4.08 |

Data Plot and Equation


## General Light Industrial <br> (110)

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday,
Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

## Setting/Location: General Urban/Suburban

Number of Studies: 41
Avg. 1000 Sq. Ft. GFA: 65
Directional Distribution: $88 \%$ entering, $12 \%$ exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.74 | $0.02-4.46$ | 0.61 |

Data Plot and Equation


# General Light Industrial <br> (110) 

Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday,
Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.

## Setting/Location: General Urban/Suburban

Number of Studies: 40
Avg. 1000 Sq. Ft. GFA: 58
Directional Distribution: $14 \%$ entering, $86 \%$ exiting
Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.65 | $0.07-7.02$ | 0.56 |

Data Plot and Equation


## Level of Service Criteria

| Signalized Intersections |  |  |
| :---: | :---: | :---: |
| Level of Service | Interpretation | $\begin{array}{r} \text { Average Control } \\ \text { Delay } \\ \text { (seconds per vehicle) } \end{array}$ |
| A | Favorable progression. Most vehicles arrive during the green indication and travel through the intersection without stopping. | $\leq 10$ |
| B | Good progression, with more vehicles stopping than for Level of Service A. | >10-20 |
| C | Individual cycle failures (i.e., one or more queued vehicles are not able to depart as a result of insufficient capacity during the cycle) may begin to appear. Number of vehicles stopping is significant, although many vehicles still pass through the intersection without stopping. | >20-35 |
| D | The volume-to-capacity ratio is high and either progression is ineffective or the cycle length is too long. Many vehicles stop and individual cycle failures are noticeable. | > $35-55$ |
| E | Progression is unfavorable. The volume-to-capacity ratio is high and the cycle length is long. Individual cycle failures are frequent. | >55-80 |
| F | The volume-to-capacity ratio is very high, progression is very poor, and the cycle length is long. Most cycles fail to clear the queue. | >80.0 |
| Unsignalized Intersections |  |  |
| Level of Service Average T |  | tal Delay (SEC/VEH) |
|  | A | 0-10 |
|  | B | > $10-15$ |
|  | C | > 15-25 |
|  | D | > 25-35 |
|  | E | > $35-50$ |
|  | F | $>50$ |
| Source: Highway Capacity Manual, 2010. |  |  |

Capacity Analysis Summary Sheets 2022 Existing Weekday Morning Peak Hour Conditions


[^0]Synchro 11 Report


|  | 4 | $\rightarrow$ | \% | 7 |  |  | $4$ |  | $p$ | , | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  |  | * $\uparrow$ |  |  |  |  |  | * |  |
| Traffic Volume (vph) | 213 | 331 | 39 | 12 | 286 | 269 | 0 | 0 | 0 | 32 | 12 | 26 |
| Future Volume (vph) | 213 | 331 | 39 | 12 | 286 | 269 | 0 | 0 | 0 | 32 | 12 | 26 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 11 | 11 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 12 | 16 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 25 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 0.88 | 0.99 |  |  | 0.75 |  |  |  |  |  | 0.67 |  |
| Frt |  | 0.984 |  |  | 0.929 |  |  |  |  |  | 0.950 |  |
| Flt Protected | 0.950 |  |  |  | 0.999 |  |  |  |  |  | 0.978 |  |
| Satd. Flow (prot) | 1745 | 1669 | 0 | 0 | 2328 | 0 | 0 | 0 | 0 | 0 | 1704 | 0 |
| Flt Permitted | 0.286 |  |  |  | 0.941 |  |  |  |  |  | 0.978 |  |
| Satd. Flow (perm) | 460 | 1669 | 0 | 0 | 2192 | 0 | 0 | 0 | 0 | 0 | 1282 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 11 |  |  | 320 |  |  |  |  |  | 30 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 3304 |  |  | 1008 |  |  | 396 |  |  | 1322 |  |
| Travel Time (s) |  | 75.1 |  |  | 22.9 |  |  | 9.0 |  |  | 30.0 |  |
| Confl. Peds. (\#/hr) | 216 |  | 18 | 18 |  | 216 | 177 |  | 256 | 256 |  | 177 |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 0\% | 8\% | 3\% | 8\% | 7\% | 1\% | 0\% | 0\% | 0\% | 3\% | 0\% | 8\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 277 | 481 | 0 | 0 | 736 | 0 | 0 | 0 | 0 | 0 | 92 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA |  |  |  |  | Perm | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  |  |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  |  |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  |  |  |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 60.0 |  | 49.0 | 49.0 |  |  |  |  | 30.0 | 30.0 |  |
| Minimum Split (s) | 11.0 | 65.0 |  | 54.0 | 54.0 |  |  |  |  | 35.0 | 35.0 |  |
| Total Split (s) | 11.0 | 65.0 |  | 54.0 | 54.0 |  |  |  |  | 35.0 | 35.0 |  |
| Total Split (\%) | 11.0\% | 65.0\% |  | 54.0\% | 54.0\% |  |  |  |  | 35.0\% | 35.0\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  |  |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 0.0 | 2.0 |  | 2.0 | 2.0 |  |  |  |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 |  |
| Total Lost Time (s) | 3.0 | 5.0 |  |  | 5.0 |  |  |  |  |  | 5.0 |  |
| Lead/Lag | Lead |  |  | Lag | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  |  |  |  | Max | Max |  |
| Act Effct Green (s) | 62.0 | 60.0 |  |  | 49.0 |  |  |  |  |  | 30.0 |  |
| Actuated g/C Ratio | 0.62 | 0.60 |  |  | 0.49 |  |  |  |  |  | 0.30 |  |


|  | 4 |  |  | 7 |  |  | , | 4 | 7 | * | $\pm$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.71 | 0.48 |  |  | 0.59 |  |  |  |  |  | 0.23 |  |
| Control Delay | 20.8 | 12.9 |  |  | 12.0 |  |  |  |  |  | 19.9 |  |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 |  |
| Total Delay | 20.8 | 12.9 |  |  | 12.0 |  |  |  |  |  | 19.9 |  |
| LOS | C | B |  |  | B |  |  |  |  |  | B |  |
| Approach Delay |  | 15.8 |  |  | 12.0 |  |  |  |  |  | 19.9 |  |
| Approach LOS |  | B |  |  | B |  |  |  |  |  | B |  |
| Queue Length 50th (ft) | 73 | 155 |  |  | 92 |  |  |  |  |  | 29 |  |
| Queue Length 95th (ft) | 94 | 183 |  |  | 104 |  |  |  |  |  | 56 |  |
| Internal Link Dist (ft) |  | 3224 |  |  | 928 |  |  | 316 |  |  | 1242 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 388 | 1005 |  |  | 1237 |  |  |  |  |  | 405 |  |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Reduced v/c Ratio | 0.71 | 0.48 |  |  | 0.59 |  |  |  |  |  | 0.23 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 11 (11\%), Referenced to phase 2: and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.71 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 14.3 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 128.3\% |  |  |  | ICU Level of Service H |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 2: 47th Street \& Kildare Avenue


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 11.6 |
| Intersection LOS | B |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ${ }_{\text {¢ }}$ |  |  | $\dagger$ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 2 | 24 | 8 | 112 | 21 | 11 | 18 | 162 | 201 | 5 | 64 | 5 |
| Future Vol, veh/h | 2 | 24 | 8 | 112 | 21 | 11 | 18 | 162 | 201 | 5 | 64 | 5 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles, \% | 50 | 79 | 25 | 13 | 62 | 82 | 28 | 4 | 8 | 8 | 3 | 2 |
| Mvmt Flow | 2 | 26 | 9 | 119 | 22 | 12 | 19 | 172 | 214 | 5 | 68 | 5 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 9.5 |  |  | 10.2 |  |  | 12.9 |  |  | 8.7 |  |  |
| HCM LOS | A |  |  | B |  |  | B |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $5 \%$ | $6 \%$ | $78 \%$ | $7 \%$ |
| Vol Thu, $\%$ | $43 \%$ | $71 \%$ | $15 \%$ | $86 \%$ |
| Vol Right, \% | $53 \%$ | $24 \%$ | $8 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 18 | 34 | 144 | 74 |
| LT Vol | 2 | 112 | 5 |  |
| Through Vol | 162 | 24 | 21 | 64 |
| RT Vol | 201 | 8 | 11 | 5 |
| Lane Flow Rate | 405 | 36 | 153 | 79 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.529 | 0.061 | 0.232 | 0.11 |
| Departure Headway (Hd) | 4.695 | 6.027 | 5.447 | 5.02 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 766 | 589 | 654 | 709 |
| Service Time | 2.742 | 4.114 | 3.518 | 3.09 |
| HCM Lane V/C Ratio | 0.529 | 0.061 | 0.234 | 0.111 |
| HCM Control Delay | 12.9 | 9.5 | 10.2 | 8.7 |
| HCM Lane LOS | B | A | B | A |
| HCM 95th-tile Q | 3.1 | 0.2 | 0.9 | 0.4 |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 17.2 |
| Intersection LOS | C |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | * |  |  | \$ |  |  | \& |  |
| Traffic Vol, veh/h | 242 | 26 | 16 | 9 | 28 | 66 | 179 | 172 | 87 | 40 | 37 | 38 |
| Future Vol, veh/h | 242 | 26 | 16 | 9 | 28 | 66 | 179 | 172 | 87 | 40 | 37 | 38 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, \% | 6 | 23 | 6 | 11 | 39 | 6 | 1 | 1 | 0 | 3 | 5 | 18 |
| Mvmt Flow | 266 | 29 | 18 | 10 | 31 | 73 | 197 | 189 | 96 | 44 | 41 | 42 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 15.7 |  |  | 10.6 |  |  | 21.5 |  |  | 10.6 |  |  |
| HCM LOS | C |  |  | B |  |  | C |  |  | B |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $41 \%$ | $85 \%$ | $9 \%$ | $35 \%$ |
| Vol Thru, \% | $39 \%$ | $9 \%$ | $27 \%$ | $32 \%$ |
| Vol Right, \% | $20 \%$ | $6 \%$ | $64 \%$ | $33 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 438 | 284 | 103 | 115 |
| LT Vol | 179 | 242 | 9 | 40 |
| Through Vol | 172 | 26 | 28 | 37 |
| RT Vol | 87 | 16 | 66 | 38 |
| Lane Flow Rate | 481 | 312 | 113 | 126 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.724 | 0.526 | 0.191 | 0.209 |
| Departure Headway (Hd) | 5.413 | 6.063 | 6.077 | 5.966 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 664 | 593 | 585 | 596 |
| Service Time | 3.475 | 4.132 | 4.169 | 4.056 |
| HCM Lane V/C Ratio | 0.724 | 0.526 | 0.193 | 0.211 |
| HCM Control Delay | 21.5 | 15.7 | 10.6 | 10.6 |
| HCM Lane LOS | C | C | B | B |
| HCM 95th-tile Q | 6.2 | 3.1 | 0.7 | 0.8 |

# Capacity Analysis Summary Sheets 2022 Existing Weekday Evening Peak Hour Conditions 




|  | $\psi$ | $\rightarrow$ |  | 4 |  |  | 4 | 4 | 7 |  | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  |  | $\uparrow \uparrow$ |  |  |  |  |  | \& |  |
| Traffic Volume (vph) | 32 | 496 | 22 | 19 | 571 | 15 | 0 | 0 | 0 | 99 | 48 | 114 |
| Future Volume (vph) | 32 | 496 | 22 | 19 | 571 | 15 | 0 | 0 | 0 | 99 | 48 | 114 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 11 | 11 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 12 | 16 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 25 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 0.99 | 1.00 |  |  | 1.00 |  |  |  |  |  | 0.98 |  |
| Frt |  | 0.994 |  |  | 0.996 |  |  |  |  |  | 0.941 |  |
| Flt Protected | 0.950 |  |  |  | 0.998 |  |  |  |  |  | 0.981 |  |
| Satd. Flow (prot) | 1601 | 1719 | 0 | 0 | 3275 | 0 | 0 | 0 | 0 | 0 | 1904 | 0 |
| Flt Permitted | 0.328 |  |  |  | 0.930 |  |  |  |  |  | 0.981 |  |
| Satd. Flow (perm) | 550 | 1719 | 0 | 0 | 3051 | 0 | 0 | 0 | 0 | 0 | 1889 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 5 |  |  | 4 |  |  |  |  |  | 46 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 3304 |  |  | 1008 |  |  | 396 |  |  | 1322 |  |
| Travel Time (s) |  | 75.1 |  |  | 22.9 |  |  | 9.0 |  |  | 30.0 |  |
| Confl. Peds. (\#/hr) | 7 |  | 14 | 14 |  | 7 | 9 |  | 9 | 9 |  | 9 |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 9\% | 6\% | 5\% | 5\% | 6\% | 0\% | 0\% | 0\% | 0\% | 4\% | 0\% | 4\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 35 | 563 | 0 | 0 | 658 | 0 | 0 | 0 | 0 | 0 | 284 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA |  |  |  |  | Perm | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  |  |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  |  |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  |  |  |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 50.0 |  | 42.0 | 42.0 |  |  |  |  | 25.0 | 25.0 |  |
| Minimum Split (s) | 8.0 | 55.0 |  | 47.0 | 47.0 |  |  |  |  | 30.0 | 30.0 |  |
| Total Split (s) | 8.0 | 55.0 |  | 47.0 | 47.0 |  |  |  |  | 30.0 | 30.0 |  |
| Total Split (\%) | 9.4\% | 64.7\% |  | 55.3\% | 55.3\% |  |  |  |  | 35.3\% | 35.3\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  |  |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 0.0 | 2.0 |  | 2.0 | 2.0 |  |  |  |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 |  |
| Total Lost Time (s) | 3.0 | 5.0 |  |  | 5.0 |  |  |  |  |  | 5.0 |  |
| Lead/Lag | Lead |  |  | Lag | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  |  |  |  | Max | Max |  |
| Act Effct Green (s) | 52.0 | 50.0 |  |  | 42.0 |  |  |  |  |  | 25.0 |  |
| Actuated g/C Ratio | 0.61 | 0.59 |  |  | 0.49 |  |  |  |  |  | 0.29 |  |



Splits and Phases: 2: 47th Street \& Kildare Avenue


| Intersection |  |
| :--- | :--- |
| Intersection Delay, s/veh | 9 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ${ }_{\text {¢ }}$ |  |  | ¢ |  |  | ¢ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 12 | 38 | 35 | 80 | 6 | 6 | 7 | 60 | 45 | 6 | 42 | 0 |
| Future Vol, veh/h | 12 | 38 | 35 | 80 | 6 | 6 | 7 | 60 | 45 | 6 | 42 | 0 |
| Peak Hour Factor | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles, \% | 0 | 18 | 6 | 26 | 17 | 89 | 71 | 5 | 4 | 0 | 5 | 0 |
| Mvmt Flow | 15 | 48 | 44 | 100 | 8 | 8 | 9 | 75 | 56 | 8 | 53 | 0 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 8 |  |  | 9.2 |  |  | 10 |  |  | 8.1 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $6 \%$ | $14 \%$ | $87 \%$ | $12 \%$ |
| Vol Thu, $\%$ | $54 \%$ | $45 \%$ | $7 \%$ | $88 \%$ |
| Vol Right, $\%$ | $40 \%$ | $41 \%$ | $7 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 112 | 85 | 92 | 48 |
| LT Vol | 7 | 12 | 80 | 6 |
| Through Vol | 60 | 38 | 6 | 42 |
| RT Vol | 45 | 35 | 6 | 0 |
| Lane Flow Rate | 140 | 106 | 115 | 60 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.213 | 0.129 | 0.164 | 0.078 |
| Departure Headway (Hd) | 5.488 | 4.37 | 5.136 | 4.657 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 654 | 820 | 69 | 768 |
| Service Time | 3.52 | 2.399 | 3.165 | 2.694 |
| HCM Lane V/C Ratio | 0.214 | 0.129 | 0.165 | 0.078 |
| HCM Control Delay | 10 | 8 | 9.2 | 8.1 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.8 | 0.4 | 0.6 | 0.3 |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 8.9 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ${ }_{\text {¢ }}$ |  |  | ¢ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 17 | 59 | 31 | 20 | 10 | 7 | 8 | 13 | 45 | 6 | 147 | 32 |
| Future Vol, veh/h | 17 | 59 | 31 | 20 | 10 | 7 | 8 | 13 | 45 | 6 | 147 | 32 |
| Peak Hour Factor | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles, \% | 12 | 7 | 13 | 0 | 0 | 0 | 0 | 0 | 1 | 17 | 3 | 22 |
| Mvmt Flow | 21 | 74 | 39 | 25 | 13 | 9 | 10 | 16 | 56 | 8 | 184 | 40 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 8.8 |  |  | 8.1 |  |  | 7.7 |  |  | 9.6 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $12 \%$ | $16 \%$ | $54 \%$ | $3 \%$ |
| Vol Thru, \% | $20 \%$ | $55 \%$ | $27 \%$ | $79 \%$ |
| Vol Right, \% | $68 \%$ | $29 \%$ | $19 \%$ | $17 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 66 | 107 | 37 | 185 |
| LT Vol | 8 | 17 | 20 | 6 |
| Through Vol | 13 | 59 | 10 | 147 |
| RT Vol | 45 | 31 | 7 | 32 |
| Lane Flow Rate | 82 | 134 | 46 | 231 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.097 | 0.176 | 0.062 | 0.297 |
| Departure Headway (Hd) | 4.221 | 4.746 | 4.792 | 4.617 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 848 | 756 | 746 | 779 |
| Service Time | 2.253 | 2.779 | 2.829 | 2.643 |
| HCM Lane V/C Ratio | 0.097 | 0.177 | 0.062 | 0.297 |
| HCM Control Delay | 7.7 | 8.8 | 8.1 | 9.6 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.3 | 0.6 | 0.2 | 1.2 |



|  | 4 |  | 4 | $\dagger$ | $\ddagger$ | / |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |  |
| v/c Ratio | 0.71 |  | 0.34 | 0.62 | 0.48 |  |  |
| Control Delay | 51.1 |  | 7.3 | 9.6 | 11.9 |  |  |
| Queue Delay | 0.0 |  | 0.0 | 0.0 | 0.0 |  |  |
| Total Delay | 51.1 |  | 7.3 | 9.6 | 11.9 |  |  |
| LOS | D |  | A | A | B |  |  |
| Approach Delay | 51.1 |  |  | 9.4 | 11.9 |  |  |
| Approach LOS | D |  |  | A | B |  |  |
| Queue Length 50th (ft) | 131 |  | 23 | 255 | 172 |  |  |
| Queue Length 95th (ft) | 202 |  | 49 | 386 | 248 |  |  |
| Internal Link Dist (ft) | 1944 |  |  | 1455 | 9038 |  |  |
| Turn Bay Length (ft) |  |  | 110 |  |  |  |  |
| Base Capacity (vph) | 382 |  | 387 | 2495 | 2052 |  |  |
| Starvation Cap Reductn | 0 |  | 0 | 0 | 0 |  |  |
| Spillback Cap Reductn | 0 |  | 0 | 0 | 0 |  |  |
| Storage Cap Reductn | 0 |  | 0 | 0 | 0 |  |  |
| Reduced v/c Ratio | 0.55 |  | 0.34 | 0.62 | 0.48 |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |
| Offset: 85 (77\%), Referenced to phase 2:NBTL and 6:SBT, Start of Green |  |  |  |  |  |  |  |
| Natural Cycle: 95 |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.71 |  |  |  |  |  |  |  |
| Intersection Signal Delay: 13.3 |  |  |  | Intersection LOS: B |  |  |  |
| Intersection Capacity Utilization 82.8\% |  |  |  | ICU Level of Service E |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |
| Splits and Phases: 1: Pulaski Road \& Ann Lurie Place |  |  |  |  |  |  |  |
| $T_{02(R)}$ |  |  |  |  |  |  |  |
| 78 s |  |  |  |  |  |  | 32 s |
|  |  |  |  |  |  |  |  |


|  | 4 | $\rightarrow$ |  |  |  |  |  | 4 |  | - |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  |  | * $\uparrow$ |  |  |  |  |  | \& |  |
| Traffic Volume (vph) | 213 | 341 | 39 | 12 | 295 | 269 | 0 | 0 | 0 | 32 | 12 | 26 |
| Future Volume (vph) | 213 | 341 | 39 | 12 | 295 | 269 | 0 | 0 | 0 | 32 | 12 | 26 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 11 | 11 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 12 | 16 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 25 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 0.88 | 0.99 |  |  | 0.75 |  |  |  |  |  | 0.66 |  |
| Frt |  | 0.985 |  |  | 0.930 |  |  |  |  |  | 0.950 |  |
| Flt Protected | 0.950 |  |  |  | 0.999 |  |  |  |  |  | 0.978 |  |
| Satd. Flow (prot) | 1745 | 1670 | 0 | 0 | 2325 | 0 | 0 | 0 | 0 | 0 | 1697 | 0 |
| Flt Permitted | 0.281 |  |  |  | 0.941 |  |  |  |  |  | 0.978 |  |
| Satd. Flow (perm) | 452 | 1670 | 0 | 0 | 2188 | 0 | 0 | 0 | 0 | 0 | 1270 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 10 |  |  | 312 |  |  |  |  |  | 30 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 3304 |  |  | 1008 |  |  | 396 |  |  | 1322 |  |
| Travel Time (s) |  | 75.1 |  |  | 22.9 |  |  | 9.0 |  |  | 30.0 |  |
| Confl. Peds. (\#/hr) | 238 |  | 20 | 20 |  | 238 | 195 |  | 272 | 272 |  | 195 |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 0\% | 8\% | 3\% | 8\% | 7\% | 1\% | 0\% | 0\% | 0\% | 3\% | 0\% | 8\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 277 | 494 | 0 | 0 | 748 | 0 | 0 | 0 | 0 | 0 | 92 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA |  |  |  |  | Perm | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  |  |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  |  |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  |  |  |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 60.0 |  | 49.0 | 49.0 |  |  |  |  | 30.0 | 30.0 |  |
| Minimum Split (s) | 11.0 | 65.0 |  | 54.0 | 54.0 |  |  |  |  | 35.0 | 35.0 |  |
| Total Split (s) | 11.0 | 65.0 |  | 54.0 | 54.0 |  |  |  |  | 35.0 | 35.0 |  |
| Total Split (\%) | 11.0\% | 65.0\% |  | 54.0\% | 54.0\% |  |  |  |  | 35.0\% | 35.0\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  |  |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 0.0 | 2.0 |  | 2.0 | 2.0 |  |  |  |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 |  |
| Total Lost Time (s) | 3.0 | 5.0 |  |  | 5.0 |  |  |  |  |  | 5.0 |  |
| Lead/Lag | Lead |  |  | Lag | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  |  |  |  | Max | Max |  |
| Act Effct Green (s) | 62.0 | 60.0 |  |  | 49.0 |  |  |  |  |  | 30.0 |  |
| Actuated g/C Ratio | 0.62 | 0.60 |  |  | 0.49 |  |  |  |  |  | 0.30 |  |


|  | 4 |  |  | 7 |  |  | , | 4 | 7 | * | $\pm$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.72 | 0.49 |  |  | 0.61 |  |  |  |  |  | 0.23 |  |
| Control Delay | 21.5 | 13.1 |  |  | 12.5 |  |  |  |  |  | 20.0 |  |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 |  |
| Total Delay | 21.5 | 13.1 |  |  | 12.5 |  |  |  |  |  | 20.0 |  |
| LOS | C | B |  |  | B |  |  |  |  |  | B |  |
| Approach Delay |  | 16.1 |  |  | 12.5 |  |  |  |  |  | 20.0 |  |
| Approach LOS |  | B |  |  | B |  |  |  |  |  | B |  |
| Queue Length 50th (ft) | 73 | 162 |  |  | 98 |  |  |  |  |  | 29 |  |
| Queue Length 95th (ft) | 94 | 189 |  |  | 110 |  |  |  |  |  | 56 |  |
| Internal Link Dist (ft) |  | 3224 |  |  | 928 |  |  | 316 |  |  | 1242 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 383 | 1006 |  |  | 1231 |  |  |  |  |  | 402 |  |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Reduced v/c Ratio | 0.72 | 0.49 |  |  | 0.61 |  |  |  |  |  | 0.23 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 11 (11\%), Referenced to phase 2: and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.72 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 14.7 |  |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 128.3\% |  |  |  |  | ICU Level of Service H |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 2: 47th Street \& Kildare Avenue


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 11.6 |
| Intersection LOS | B |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ${ }_{\text {¢ }}$ |  |  | $\dagger$ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 2 | 24 | 8 | 112 | 21 | 11 | 18 | 162 | 201 | 5 | 64 | 5 |
| Future Vol, veh/h | 2 | 24 | 8 | 112 | 21 | 11 | 18 | 162 | 201 | 5 | 64 | 5 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles, \% | 50 | 79 | 25 | 13 | 62 | 82 | 28 | 4 | 8 | 8 | 3 | 2 |
| Mvmt Flow | 2 | 26 | 9 | 119 | 22 | 12 | 19 | 172 | 214 | 5 | 68 | 5 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 9.5 |  |  | 10.2 |  |  | 12.9 |  |  | 8.7 |  |  |
| HCM LOS | A |  |  | B |  |  | B |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $5 \%$ | $6 \%$ | $78 \%$ | $7 \%$ |
| Vol Thu, $\%$ | $43 \%$ | $71 \%$ | $15 \%$ | $86 \%$ |
| Vol Right, \% | $53 \%$ | $24 \%$ | $8 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 18 | 34 | 144 | 74 |
| LT Vol | 2 | 112 | 5 |  |
| Through Vol | 162 | 24 | 21 | 64 |
| RT Vol | 201 | 8 | 11 | 5 |
| Lane Flow Rate | 405 | 36 | 153 | 79 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.529 | 0.061 | 0.232 | 0.11 |
| Departure Headway (Hd) | 4.695 | 6.027 | 5.447 | 5.02 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 766 | 589 | 654 | 709 |
| Service Time | 2.742 | 4.114 | 3.518 | 3.09 |
| HCM Lane V/C Ratio | 0.529 | 0.061 | 0.234 | 0.111 |
| HCM Control Delay | 12.9 | 9.5 | 10.2 | 8.7 |
| HCM Lane LOS | B | A | B | A |
| HCM 95th-tile Q | 3.1 | 0.2 | 0.9 | 0.4 |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 17.2 |
| Intersection LOS | C |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | * |  |  | \$ |  |  | \& |  |
| Traffic Vol, veh/h | 242 | 26 | 16 | 9 | 28 | 66 | 179 | 172 | 87 | 40 | 37 | 38 |
| Future Vol, veh/h | 242 | 26 | 16 | 9 | 28 | 66 | 179 | 172 | 87 | 40 | 37 | 38 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, \% | 6 | 23 | 6 | 11 | 39 | 6 | 1 | 1 | 0 | 3 | 5 | 18 |
| Mvmt Flow | 266 | 29 | 18 | 10 | 31 | 73 | 197 | 189 | 96 | 44 | 41 | 42 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 15.7 |  |  | 10.6 |  |  | 21.5 |  |  | 10.6 |  |  |
| HCM LOS | C |  |  | B |  |  | C |  |  | B |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $41 \%$ | $85 \%$ | $9 \%$ | $35 \%$ |
| Vol Thru, \% | $39 \%$ | $9 \%$ | $27 \%$ | $32 \%$ |
| Vol Right, \% | $20 \%$ | $6 \%$ | $64 \%$ | $33 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 438 | 284 | 103 | 115 |
| LT Vol | 179 | 242 | 9 | 40 |
| Through Vol | 172 | 26 | 28 | 37 |
| RT Vol | 87 | 16 | 66 | 38 |
| Lane Flow Rate | 481 | 312 | 113 | 126 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.724 | 0.526 | 0.191 | 0.209 |
| Departure Headway (Hd) | 5.413 | 6.063 | 6.077 | 5.966 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 664 | 593 | 585 | 596 |
| Service Time | 3.475 | 4.132 | 4.169 | 4.056 |
| HCM Lane V/C Ratio | 0.724 | 0.526 | 0.193 | 0.211 |
| HCM Control Delay | 21.5 | 15.7 | 10.6 | 10.6 |
| HCM Lane LOS | C | C | B | B |
| HCM 95th-tile Q | 6.2 | 3.1 | 0.7 | 0.8 |

# Capacity Analysis Summary Sheets 

 2028 No Build Weekday Evening Peak Hour Conditions


Splits and Phases: 1: Pulaski Road \& Ann Lurie Place


|  | 4 | $\rightarrow$ |  |  |  |  |  | 4 |  | - |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  |  | * $\uparrow$ |  |  |  |  |  | \& |  |
| Traffic Volume (vph) | 32 | 511 | 22 | 19 | 588 | 15 | 0 | 0 | 0 | 99 | 48 | 114 |
| Future Volume (vph) | 32 | 511 | 22 | 19 | 588 | 15 | 0 | 0 | 0 | 99 | 48 | 114 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 11 | 11 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 12 | 16 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 25 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 0.99 | 1.00 |  |  | 1.00 |  |  |  |  |  | 0.98 |  |
| Frt |  | 0.994 |  |  | 0.996 |  |  |  |  |  | 0.941 |  |
| Flt Protected | 0.950 |  |  |  | 0.998 |  |  |  |  |  | 0.981 |  |
| Satd. Flow (prot) | 1601 | 1719 | 0 | 0 | 3275 | 0 | 0 | 0 | 0 | 0 | 1903 | 0 |
| Flt Permitted | 0.319 |  |  |  | 0.930 |  |  |  |  |  | 0.981 |  |
| Satd. Flow (perm) | 534 | 1719 | 0 | 0 | 3050 | 0 | 0 | 0 | 0 | 0 | 1886 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 4 |  |  | 4 |  |  |  |  |  | 46 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 3304 |  |  | 1008 |  |  | 396 |  |  | 1322 |  |
| Travel Time (s) |  | 75.1 |  |  | 22.9 |  |  | 9.0 |  |  | 30.0 |  |
| Confl. Peds. (\#/hr) | 8 |  | 15 | 15 |  | 8 | 10 |  | 10 | 10 |  | 10 |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 9\% | 6\% | 5\% | 5\% | 6\% | 0\% | 0\% | 0\% | 0\% | 4\% | 0\% | 4\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 35 | 579 | 0 | 0 | 676 | 0 | 0 | 0 | 0 | 0 | 284 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA |  |  |  |  | Perm | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  |  |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  |  |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  |  |  |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 50.0 |  | 42.0 | 42.0 |  |  |  |  | 25.0 | 25.0 |  |
| Minimum Split (s) | 8.0 | 55.0 |  | 47.0 | 47.0 |  |  |  |  | 30.0 | 30.0 |  |
| Total Split (s) | 8.0 | 55.0 |  | 47.0 | 47.0 |  |  |  |  | 30.0 | 30.0 |  |
| Total Split (\%) | 9.4\% | 64.7\% |  | 55.3\% | 55.3\% |  |  |  |  | 35.3\% | 35.3\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  |  |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 0.0 | 2.0 |  | 2.0 | 2.0 |  |  |  |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 |  |
| Total Lost Time (s) | 3.0 | 5.0 |  |  | 5.0 |  |  |  |  |  | 5.0 |  |
| Lead/Lag | Lead |  |  | Lag | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  |  |  |  | Max | Max |  |
| Act Effct Green (s) | 52.0 | 50.0 |  |  | 42.0 |  |  |  |  |  | 25.0 |  |
| Actuated g/C Ratio | 0.61 | 0.59 |  |  | 0.49 |  |  |  |  |  | 0.29 |  |


|  | 4 |  |  | 7 |  |  | , | 4 | 7 | $\pm$ | $\pm$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.09 | 0.57 |  |  | 0.45 |  |  |  |  |  | 0.48 |  |
| Control Delay | 7.1 | 13.6 |  |  | 15.1 |  |  |  |  |  | 23.8 |  |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 |  |
| Total Delay | 7.1 | 13.6 |  |  | 15.1 |  |  |  |  |  | 23.8 |  |
| LOS | A | B |  |  | B |  |  |  |  |  | C |  |
| Approach Delay |  | 13.2 |  |  | 15.1 |  |  |  |  |  | 23.8 |  |
| Approach LOS |  | B |  |  | B |  |  |  |  |  | C |  |
| Queue Length 50th (ft) | 7 | 175 |  |  | 116 |  |  |  |  |  | 103 |  |
| Queue Length 95th (ft) | 18 | 268 |  |  | 161 |  |  |  |  |  | 177 |  |
| Internal Link Dist (ft) |  | 3224 |  |  | 928 |  |  | 316 |  |  | 1242 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 389 | 1012 |  |  | 1509 |  |  |  |  |  | 587 |  |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Reduced v/c Ratio | 0.09 | 0.57 |  |  | 0.45 |  |  |  |  |  | 0.48 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 85 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 85 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 11 (13\%), Referenced to phase 2: and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 85 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.57 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 15.9 |  |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 72.1\% |  |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 2: 47th Street \& Kildare Avenue


| Intersection |  |
| :--- | :--- |
| Intersection Delay, s/veh | 9 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ${ }_{\text {¢ }}$ |  |  | ¢ |  |  | ¢ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 12 | 38 | 35 | 80 | 6 | 6 | 7 | 60 | 45 | 6 | 42 | 0 |
| Future Vol, veh/h | 12 | 38 | 35 | 80 | 6 | 6 | 7 | 60 | 45 | 6 | 42 | 0 |
| Peak Hour Factor | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles, \% | 0 | 18 | 6 | 26 | 17 | 89 | 71 | 5 | 4 | 0 | 5 | 0 |
| Mvmt Flow | 15 | 48 | 44 | 100 | 8 | 8 | 9 | 75 | 56 | 8 | 53 | 0 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 8 |  |  | 9.2 |  |  | 10 |  |  | 8.1 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $6 \%$ | $14 \%$ | $87 \%$ | $12 \%$ |
| Vol Thu, $\%$ | $54 \%$ | $45 \%$ | $7 \%$ | $88 \%$ |
| Vol Right, $\%$ | $40 \%$ | $41 \%$ | $7 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 112 | 85 | 92 | 48 |
| LT Vol | 7 | 12 | 80 | 6 |
| Through Vol | 60 | 38 | 6 | 42 |
| RT Vol | 45 | 35 | 6 | 0 |
| Lane Flow Rate | 140 | 106 | 115 | 60 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.213 | 0.129 | 0.164 | 0.078 |
| Departure Headway (Hd) | 5.488 | 4.37 | 5.136 | 4.657 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 654 | 820 | 69 | 768 |
| Service Time | 3.52 | 2.399 | 3.165 | 2.694 |
| HCM Lane V/C Ratio | 0.214 | 0.129 | 0.165 | 0.078 |
| HCM Control Delay | 10 | 8 | 9.2 | 8.1 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.8 | 0.4 | 0.6 | 0.3 |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 8.9 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ¢ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 17 | 59 | 31 | 20 | 10 | 7 | 8 | 13 | 45 | 6 | 147 | 32 |
| Future Vol, veh/h | 17 | 59 | 31 | 20 | 10 | 7 | 8 | 13 | 45 | 6 | 147 | 32 |
| Peak Hour Factor | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles, \% | 12 | 7 | 13 | 0 | 0 | 0 | 0 | 0 | 11 | 17 | 3 | 22 |
| Mvmt Flow | 21 | 74 | 39 | 25 | 13 | 9 | 10 | 16 | 56 | 8 | 184 | 40 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 8.8 |  |  | 8.1 |  |  | 7.7 |  |  | 9.6 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $12 \%$ | $16 \%$ | $54 \%$ | $3 \%$ |
| Vol Thru, \% | $20 \%$ | $55 \%$ | $27 \%$ | $79 \%$ |
| Vol Right, \% | $68 \%$ | $29 \%$ | $19 \%$ | $17 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 66 | 107 | 37 | 185 |
| LT Vol | 8 | 17 | 20 | 6 |
| Through Vol | 13 | 59 | 10 | 147 |
| RT Vol | 45 | 31 | 7 | 32 |
| Lane Flow Rate | 82 | 134 | 46 | 231 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.097 | 0.176 | 0.062 | 0.297 |
| Departure Headway (Hd) | 4.221 | 4.746 | 4.792 | 4.617 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 848 | 756 | 746 | 779 |
| Service Time | 2.253 | 2.779 | 2.829 | 2.643 |
| HCM Lane V/C Ratio | 0.097 | 0.177 | 0.062 | 0.297 |
| HCM Control Delay | 7.7 | 8.8 | 8.1 | 9.6 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.3 | 0.6 | 0.2 | 1.2 |

# Capacity Analysis Summary Sheets 2028 Projected Weekday Morning Peak Hour Conditions 



[^1]Synchro 11 Report

|  | 4 |  | 4 | 4 | $\ddagger$ | / |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |  |
| v/c Ratio | 0.72 |  | 0.42 | 0.63 | 0.50 |  |  |
| Control Delay | 51.7 |  | 8.6 | 9.8 | 12.3 |  |  |
| Queue Delay | 0.0 |  | 0.0 | 0.0 | 0.0 |  |  |
| Total Delay | 51.7 |  | 8.6 | 9.8 | 12.3 |  |  |
| LOS | D |  | A | A | B |  |  |
| Approach Delay | 51.7 |  |  | 9.7 | 12.3 |  |  |
| Approach LOS | D |  |  | A | B |  |  |
| Queue Length 50th (ft) | 137 |  | 29 | 261 | 186 |  |  |
| Queue Length 95th (ft) | 210 |  | 59 | 386 | 259 |  |  |
| Internal Link Dist (ft) | 1944 |  |  | 1455 | 9038 |  |  |
| Turn Bay Length (ft) |  |  | 110 |  |  |  |  |
| Base Capacity (vph) | 381 |  | 376 | 2481 | 2033 |  |  |
| Starvation Cap Reductn | 0 |  | 0 | 0 | 0 |  |  |
| Spillback Cap Reductn | 0 |  | 0 | 0 | 0 |  |  |
| Storage Cap Reductn | 0 |  | 0 | 0 | 0 |  |  |
| Reduced v/c Ratio | 0.58 |  | 0.42 | 0.63 | 0.50 |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |
| Offset: 85 (77\%), Referenced to phase 2:NBTL and 6:SBT, Start of Green |  |  |  |  |  |  |  |
| Natural Cycle: 95 |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.72 |  |  |  |  |  |  |  |
| Intersection Signal Delay: 13.7 |  |  |  | Intersection LOS: B |  |  |  |
| Intersection Capacity Utilization 84.8\% |  |  |  | ICU Level of Service E |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |
| Splits and Phases: 1: Pulaski Road \& Ann Lurie Place |  |  |  |  |  |  |  |
| $T_{02(R)}$ |  |  |  |  |  |  |  |
| 78 s |  |  |  |  |  |  | 32 s |
|  |  |  |  |  |  |  |  |


|  | 4 | $\rightarrow$ |  |  |  |  |  | 4 |  | - |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{\beta}$ |  |  | * $\uparrow$ |  |  |  |  |  | \& |  |
| Traffic Volume (vph) | 227 | 341 | 39 | 12 | 295 | 283 | 0 | 0 | 0 | 34 | 12 | 28 |
| Future Volume (vph) | 227 | 341 | 39 | 12 | 295 | 283 | 0 | 0 | 0 | 34 | 12 | 28 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 11 | 11 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 12 | 16 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 25 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 0.88 | 0.99 |  |  | 0.74 |  |  |  |  |  | 0.66 |  |
| Frt |  | 0.985 |  |  | 0.928 |  |  |  |  |  | 0.949 |  |
| Flt Protected | 0.950 |  |  |  | 0.999 |  |  |  |  |  | 0.978 |  |
| Satd. Flow (prot) | 1745 | 1670 | 0 | 0 | 2299 | 0 | 0 | 0 | 0 | 0 | 1698 | 0 |
| Flt Permitted | 0.272 |  |  |  | 0.941 |  |  |  |  |  | 0.978 |  |
| Satd. Flow (perm) | 440 | 1670 | 0 | 0 | 2165 | 0 | 0 | 0 | 0 | 0 | 1269 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 10 |  |  | 329 |  |  |  |  |  | 31 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 3304 |  |  | 1008 |  |  | 396 |  |  | 1322 |  |
| Travel Time (s) |  | 75.1 |  |  | 22.9 |  |  | 9.0 |  |  | 30.0 |  |
| Confl. Peds. (\#/hr) | 238 |  | 20 | 20 |  | 238 | 195 |  | 272 | 272 |  | 195 |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 0\% | 8\% | 3\% | 8\% | 7\% | 1\% | 0\% | 0\% | 0\% | 3\% | 0\% | 7\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 295 | 494 | 0 | 0 | 767 | 0 | 0 | 0 | 0 | 0 | 96 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA |  |  |  |  | Perm | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  |  |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  |  |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  |  |  |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 60.0 |  | 49.0 | 49.0 |  |  |  |  | 30.0 | 30.0 |  |
| Minimum Split (s) | 11.0 | 65.0 |  | 54.0 | 54.0 |  |  |  |  | 35.0 | 35.0 |  |
| Total Split (s) | 11.0 | 65.0 |  | 54.0 | 54.0 |  |  |  |  | 35.0 | 35.0 |  |
| Total Split (\%) | 11.0\% | 65.0\% |  | 54.0\% | 54.0\% |  |  |  |  | 35.0\% | 35.0\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  |  |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 0.0 | 2.0 |  | 2.0 | 2.0 |  |  |  |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 |  |
| Total Lost Time (s) | 3.0 | 5.0 |  |  | 5.0 |  |  |  |  |  | 5.0 |  |
| Lead/Lag | Lead |  |  | Lag | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  |  |  |  | Max | Max |  |
| Act Effct Green (s) | 62.0 | 60.0 |  |  | 49.0 |  |  |  |  |  | 30.0 |  |
| Actuated g/C Ratio | 0.62 | 0.60 |  |  | 0.49 |  |  |  |  |  | 0.30 |  |

[^2]|  | 4 |  |  | 7 |  |  | , | 4 | 7 | $\pm$ | $\pm$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.78 | 0.49 |  |  | 0.62 |  |  |  |  |  | 0.24 |  |
| Control Delay | 26.1 | 13.1 |  |  | 12.6 |  |  |  |  |  | 20.0 |  |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 |  |
| Total Delay | 26.1 | 13.1 |  |  | 12.6 |  |  |  |  |  | 20.0 |  |
| LOS | C | B |  |  | B |  |  |  |  |  | C |  |
| Approach Delay |  | 18.0 |  |  | 12.6 |  |  |  |  |  | 20.0 |  |
| Approach LOS |  | B |  |  | B |  |  |  |  |  | C |  |
| Queue Length 50th (ft) | 79 | 162 |  |  | 100 |  |  |  |  |  | 31 |  |
| Queue Length 95th (ft) | 100 | 189 |  |  | 112 |  |  |  |  |  | 58 |  |
| Internal Link Dist (ft) |  | 3224 |  |  | 928 |  |  | 316 |  |  | 1242 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 377 | 1006 |  |  | 1228 |  |  |  |  |  | 402 |  |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Reduced v/c Ratio | 0.78 | 0.49 |  |  | 0.62 |  |  |  |  |  | 0.24 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 11 (11\%), Referenced to phase 2: and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.78 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 15.6 |  |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 128.3\% |  |  |  |  | ICU Level of Service H |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 2: 47th Street \& Kildare Avenue



[^3]Synchro 11 Report

|  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
|  |  |  |  |  |  |

Splits and Phases: 1: Pulaski Road \& Ann Lurie Place


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 12.4 |
| Intersection LOS | B |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | \$ |  |  | \$ |  |  | * |  |
| Traffic Vol, veh/h | 2 | 32 | 12 | 112 | 85 | 11 | 46 | 162 | 201 | 5 | 64 | 5 |
| Future Vol, veh/h | 2 | 32 | 12 | 112 | 85 | 11 | 46 | 162 | 201 | 5 | 64 | 5 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles, \% | 50 | 66 | 17 | 13 | 18 | 82 | 11 | 4 | 8 | 8 | 3 | 2 |
| Mvmt Flow | 2 | 34 | 13 | 119 | 90 | 12 | 49 | 172 | 214 | 5 | 68 | 5 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 9.9 |  |  | 11.5 |  |  | 13.8 |  |  | 9.1 |  |  |
| HCM LOS | A |  |  | B |  |  | B |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $11 \%$ | $4 \%$ | $54 \%$ | $7 \%$ |
| Vol Thru, \% | $40 \%$ | $70 \%$ | $41 \%$ | $86 \%$ |
| Vol Right, \% | $49 \%$ | $26 \%$ | $5 \%$ | $7 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 409 | 46 | 208 | 74 |
| LT Vol | 46 | 2 | 112 | 5 |
| Through Vol | 162 | 32 | 85 | 64 |
| RT Vol | 201 | 12 | 11 | 5 |
| Lane Flow Rate | 435 | 49 | 221 | 79 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.565 | 0.086 | 0.344 | 0.118 |
| Departure Headway (Hd) | 4.674 | 6.305 | 5.59 | 5.406 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 761 | 571 | 646 | 664 |
| Service Time | 2.76 | 4.317 | 3.596 | 3.425 |
| HCM Lane V/C Ratio | 0.572 | 0.086 | 0.342 | 0.119 |
| HCM Control Delay | 13.8 | 9.9 | 11.5 | 9.1 |
| HCM Lane LOS | B | A | B | A |
| HCM 95th-tile Q | 3.6 | 0.3 | 1.5 | 0.4 |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 19.2 |
| Intersection LOS | C |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \& |  |  | \& |  |  | * |  |  | * |  |
| Traffic Vol, veh/h | 242 | 26 | 16 | 9 | 28 | 66 | 179 | 200 | 87 | 40 | 41 | 38 |
| Future Vol, veh/h | 242 | 26 | 16 | 9 | 28 | 66 | 179 | 200 | 87 | 40 | 41 | 38 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, \% | 6 | 23 | 6 | 11 | 39 | 6 | 1 | 1 | 0 | 3 | 5 | 18 |
| Mvmt Flow | 266 | 29 | 18 | 10 | 31 | 73 | 197 | 220 | 96 | 44 | 45 | 42 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 16.2 |  |  | 10.9 |  |  | 24.9 |  |  | 10.9 |  |  |
| HCM LOS | C |  |  | B |  |  | C |  |  | B |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $38 \%$ | $85 \%$ | $9 \%$ | $34 \%$ |
| Vol Thru, \% | $43 \%$ | $9 \%$ | $27 \%$ | $34 \%$ |
| Vol Right, \% | $19 \%$ | $6 \%$ | $64 \%$ | $32 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 466 | 284 | 103 | 119 |
| LT Vol | 179 | 242 | 9 | 40 |
| Through Vol | 200 | 26 | 28 | 41 |
| RT Vol | 87 | 16 | 66 | 38 |
| Lane Flow Rate | 512 | 312 | 113 | 131 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.775 | 0.535 | 0.198 | 0.224 |
| Departure Headway (Hd) | 5.448 | 6.175 | 6.313 | 6.161 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 661 | 580 | 572 | 586 |
| Service Time | 3.526 | 4.266 | 4.322 | 4.161 |
| HCM Lane V/C Ratio | 0.775 | 0.538 | 0.198 | 0.224 |
| HCM Control Delay | 24.9 | 16.2 | 10.9 | 10.9 |
| HCM Lane LOS | C | C | B | B |
| HCM 95th-tile Q | 7.4 | 3.2 | 0.7 | 0.9 |

Capacity Analysis Summary Sheets 2028 Projected Weekday Evening Peak Hour Condition



Splits and Phases: 1: Pulaski Road \& Ann Lurie Place


|  | 4 | $\rightarrow$ |  |  |  |  |  | 4 |  | - |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 个 |  |  | * $\uparrow$ |  |  |  |  |  | \& |  |
| Traffic Volume (vph) | 33 | 511 | 22 | 19 | 588 | 16 | 0 | 0 | 0 | 121 | 48 | 106 |
| Future Volume (vph) | 33 | 511 | 22 | 19 | 588 | 16 | 0 | 0 | 0 | 121 | 48 | 106 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 11 | 11 | 12 | 12 | 11 | 12 | 12 | 12 | 12 | 12 | 16 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 25 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 0.99 | 1.00 |  |  | 1.00 |  |  |  |  |  | 0.98 |  |
| Frt |  | 0.994 |  |  | 0.996 |  |  |  |  |  | 0.948 |  |
| Flt Protected | 0.950 |  |  |  | 0.998 |  |  |  |  |  | 0.978 |  |
| Satd. Flow (prot) | 1601 | 1719 | 0 | 0 | 3275 | 0 | 0 | 0 | 0 | 0 | 1921 | 0 |
| Flt Permitted | 0.319 |  |  |  | 0.930 |  |  |  |  |  | 0.978 |  |
| Satd. Flow (perm) | 535 | 1719 | 0 | 0 | 3050 | 0 | 0 | 0 | 0 | 0 | 1900 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 4 |  |  | 4 |  |  |  |  |  | 38 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 3304 |  |  | 1008 |  |  | 396 |  |  | 1322 |  |
| Travel Time (s) |  | 75.1 |  |  | 22.9 |  |  | 9.0 |  |  | 30.0 |  |
| Confl. Peds. (\#/hr) | 8 |  | 15 | 15 |  | 8 | 10 |  | 10 | 10 |  | 10 |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 9\% | 6\% | 5\% | 5\% | 6\% | 0\% | 0\% | 0\% | 0\% | 4\% | 0\% | 3\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 36 | 579 | 0 | 0 | 677 | 0 | 0 | 0 | 0 | 0 | 299 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA |  |  |  |  | Perm | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  |  |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  |  |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  |  |  |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 50.0 |  | 42.0 | 42.0 |  |  |  |  | 25.0 | 25.0 |  |
| Minimum Split (s) | 8.0 | 55.0 |  | 47.0 | 47.0 |  |  |  |  | 30.0 | 30.0 |  |
| Total Split (s) | 8.0 | 55.0 |  | 47.0 | 47.0 |  |  |  |  | 30.0 | 30.0 |  |
| Total Split (\%) | 9.4\% | 64.7\% |  | 55.3\% | 55.3\% |  |  |  |  | 35.3\% | 35.3\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  |  |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 0.0 | 2.0 |  | 2.0 | 2.0 |  |  |  |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 |  |
| Total Lost Time (s) | 3.0 | 5.0 |  |  | 5.0 |  |  |  |  |  | 5.0 |  |
| Lead/Lag | Lead |  |  | Lag | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  |  |  |  | Max | Max |  |
| Act Effct Green (s) | 52.0 | 50.0 |  |  | 42.0 |  |  |  |  |  | 25.0 |  |
| Actuated g/C Ratio | 0.61 | 0.59 |  |  | 0.49 |  |  |  |  |  | 0.29 |  |


|  | 4 |  |  | 7 |  |  | , | 4 | 7 | $\pm$ | $\pm$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.09 | 0.57 |  |  | 0.45 |  |  |  |  |  | 0.51 |  |
| Control Delay | 7.1 | 13.6 |  |  | 15.1 |  |  |  |  |  | 25.2 |  |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 |  |
| Total Delay | 7.1 | 13.6 |  |  | 15.1 |  |  |  |  |  | 25.2 |  |
| LOS | A | B |  |  | B |  |  |  |  |  | C |  |
| Approach Delay |  | 13.2 |  |  | 15.1 |  |  |  |  |  | 25.2 |  |
| Approach LOS |  | B |  |  | B |  |  |  |  |  | C |  |
| Queue Length 50th (ft) | 7 | 175 |  |  | 116 |  |  |  |  |  | 114 |  |
| Queue Length 95th (ft) | 18 | 268 |  |  | 161 |  |  |  |  |  | 192 |  |
| Internal Link Dist (ft) |  | 3224 |  |  | 928 |  |  | 316 |  |  | 1242 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 390 | 1012 |  |  | 1509 |  |  |  |  |  | 585 |  |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  |  |  |  |  | 0 |  |
| Reduced v/c Ratio | 0.09 | 0.57 |  |  | 0.45 |  |  |  |  |  | 0.51 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 85 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 85 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 11 (13\%), Referenced to phase 2: and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 85 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.57 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 16.3 |  |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 72.8\% |  |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 2: 47th Street \& Kildare Avenue


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh $\quad 9.1$ |  |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ${ }_{\text {¢ }}$ |  |  | ¢ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 12 | 70 | 49 | 80 | 11 | 6 | 9 | 60 | 45 | 6 | 42 | 0 |
| Future Vol, veh/h | 12 | 70 | 49 | 80 | 11 | 6 | 9 | 60 | 45 | 6 | 42 | 0 |
| Peak Hour Factor | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles, \% | 0 | 13 | 4 | 26 | 27 | 83 | 56 | 5 | 4 | 0 | 5 | 0 |
| Mvmt Flow | 15 | 88 | 61 | 100 | 14 | 8 | 11 | 75 | 56 | 8 | 53 | 0 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 8.5 |  |  | 9.3 |  |  | 9.9 |  |  | 8.3 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $8 \%$ | $9 \%$ | $82 \%$ | $12 \%$ |
| Vol Thu, $\%$ | $53 \%$ | $53 \%$ | $11 \%$ | $88 \%$ |
| Vol Right, \% | $39 \%$ | $37 \%$ | $6 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 114 | 131 | 97 | 48 |
| LT Vol | 9 | 12 | 80 | 6 |
| Through Vol | 60 | 70 | 11 | 42 |
| RT Vol | 45 | 49 | 6 | 0 |
| Lane Flow Rate | 142 | 164 | 121 | 60 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.213 | 0.2 | 0.175 | 0.08 |
| Departure Headway (Hd) | 5.387 | 4.395 | 5.196 | 4.808 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 665 | 815 | 690 | 742 |
| Service Time | 3.429 | 2.426 | 3.232 | 2.855 |
| HCM Lane V/C Ratio | 0.214 | 0.201 | 0.175 | 0.081 |
| HCM Control Delay | 9.9 | 8.5 | 9.3 | 8.3 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.8 | 0.7 | 0.6 | 0.3 |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh $\quad 9.1$ |  |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ${ }_{\text {¢ }}$ |  |  | ¢ |  |  | ¢ |  |
| Traffic Vol, veh/h | 17 | 59 | 31 | 20 | 10 | 7 | 8 | 15 | 45 | 6 | 161 | 32 |
| Future Vol, veh/h | 17 | 59 | 31 | 20 | 10 | 7 | 8 | 15 | 45 | 6 | 161 | 32 |
| Peak Hour Factor | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles, \% | 12 | 7 | 13 | 0 | 0 | 0 | 0 | 0 | 11 | 17 | 2 | 22 |
| Mvmt Flow | 21 | 74 | 39 | 25 | 13 | 9 | 10 | 19 | 56 | 8 | 201 | 40 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 8.9 |  |  | 8.2 |  |  | 7.8 |  |  | 9.8 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $12 \%$ | $16 \%$ | $54 \%$ | $3 \%$ |
| Vol Thu, $\%$ | $22 \%$ | $55 \%$ | $27 \%$ | $81 \%$ |
| Vol Right, \% | $66 \%$ | $29 \%$ | $19 \%$ | $16 \%$ |
| Sign Control | 68 | 107 | 37 | 199 |
| Traffic Vol by Lane | 8 | 17 | 20 | 6 |
| LT Vol | 15 | 59 | 10 | 161 |
| Through Vol | 45 | 31 | 7 | 32 |
| RT Vol | 85 | 134 | 46 | 249 |
| Lane Flow Rate | 1 | 1 | 1 | 1 |
| Geometry Grp | 0.101 | 0.178 | 0.062 | 0.32 |
| Degree of Util (X) | 4.257 | 4.795 | 4.842 | 4.631 |
| Departure Headway (Hd) | Yes | Yes | Yes | Yes |
| Convergence, Y/N | 841 | 748 | 738 | 776 |
| Cap | 2.29 | 2.83 | 2.884 | 2.658 |
| Service Time | 0.101 | 0.179 | 0.062 | 0.321 |
| HCM Lane V/C Ratio | 7.8 | 8.9 | 8.2 | 9.8 |
| HCM Control Delay | A | A | A | A |
| HCM Lane LOS | 0.3 | 0.6 | 0.2 | 1.4 |


[^0]:    AMEX Existing Morning Peak 11:58 am 06/06/2022 22-173 - Ann Lurie Place Industrial
    ANB

[^1]:    AMPR Projected Morning Peak 3:16 pm 06/06/2022 22-173 - Ann Lurie Place Industrial
    ANB

[^2]:    AMPR Projected Morning Peak 3:16 pm 06/06/2022 22-173 - Ann Lurie Place Industrial ANB

[^3]:    AMPR - Alt Projected Morning Peak (All Pulaski) 3:26 pm 06/06/2022 22-173 - Ann Lurie Place Industrial
    ANB

