## AIR QUALITY IMPACT ANALYSIS



WHEATLAND TUBE PROPERTY

4435 S WESTERN BOULEVARD
CHICAGO, ILLINOIS 60609

ECS PROJECT NO. 53:3398

> FOR

BROOKFIELD PROPERTIES

AUGUST 15, 2022

## EXECUTIVE SUMMARY

ECS has conducted an Air Quality Impact Analysis (AQIA) for the proposed Wheatland Tube Property project. The analysis was conducted in general accordance with EPA methodology for project level screening analysis and in conformity to the guidance of the reviewing agency, the Chicago Department of Public Health (CDPH). The models utilized were the current versions of the EPA recommended models for Project Level Analysis, including MOVES3 and AERMOD version 21112.

Based on the model outputs, using worst-case scenario inputs and conservative post-processing, the project appears to be below the criteria for further consideration of air quality impacts. The model results indicated that the ambient concentrations of $\mathrm{PM}_{2.5}, \mathrm{PM}_{10}$, and $\mathrm{NO}_{2}$ were below the threshold established by the EPA National Ambient Air Quality Standards (NAAQS). Based on these findings, ECS concludes that the proposed project would not be expected to cause an exceedance of the NAAQS in the study area.

The executive summary is an integral portion of this report, and ECS recommends the report be read in its entirety.
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### 1.0 BACKGROUND

According to information received from Brookfield Properties, the Wheatland Tube Property located at 4435 S Western Boulevard ("the Property") is proposed to be redeveloped. ECS understands that the site is currently zoned as an industrial site for purposes of warehousing. The Municipal Code of Chicago Section 17-9-0117-G (Code), adopted in March 2021, requires for certain projects on industrial properties for "newly-established uses or existing uses that change or increase their area, bulk, or function", an Air Quality Impact Analysis (AQIA) must be submitted for review by the Chicago Department of Public Heath (CDPH) before a zoning certification may be issued. Brookfield Properties has requested ECS Midwest, LLC (ECS) to prepare an AQIA for the proposed redevelopment of the property.

### 1.1 General Project Description

The Property is currently improved with three (3) single-story industrial buildings, which currently operate as the Wheatland Tube Company. The general design concept for the proposed redevelopment will include razing the existing buildings and construction of three larger buildings encompassing approximately 588,880 square feet of warehouse/distribution space. The redevelopment would include approximately 753 passenger vehicle parking spaces, 37 truck parking spaces, and 89 loading docks. A proposed site plan is included in Appendix 1.

### 2.0 STATEMENT OF OBJECTIVES

The objective of this AQIA is to identify the projected impacts of the proposed project on ambient air quality in order to fulfill the AQIA requirement of the Code.

### 3.0 SCOPE OF WORK

The general scope of work is defined in the CDPH document, Air Quality Impact Evaluation Interim Guidance (DRAFT), September 2021.

### 3.1 Pollutants

The Clean Air Act requires the EPA to set NAAQS standards for six principal pollutants, designated Criteria Pollutants. These pollutants are carbon monoxide ( CO ), lead ( Pb ), nitrogen dioxide $\left(\mathrm{NO}_{2}\right)$, ozone $\left(\mathrm{O}_{3}\right)$, particulate matter (PM), and sulfur dioxide $\left(\mathrm{SO}_{2}\right)$. Particulate matter is further divided into fine particulate matter less than 2.5 microns ( $\mathrm{PM}_{2.5}$ ) and coarse particulate matter less than 10 microns ( $\mathrm{PM}_{10}$ ). Each regional jurisdiction must meet the standards for each of these pollutants. For the purpose of project air quality impact analysis, the CDPH requirements include assessing the impacts of the proposed development on three of these criteria pollutants, namely $\mathrm{PM}_{2.5}, \mathrm{PM}_{10}$, and $\mathrm{NO}_{2}$.

According to the EPA, $\mathrm{PM}_{2.5}$ emissions are generally produced by three processes. First, it is directly emitted from combustion processes, including the tailpipes of cars, trucks and other vehicles, as well as stationary fuel-burning sources. Secondly, it is re-entrained due to wind or vehicle movement from materials found on the roadway (typically known as fugitive dust). Thirdly, it is created by a chemical reaction from precursor emissions such as sulfur dioxide $\left(\mathrm{SO}_{2}\right)$, nitrogen oxides (NOx),
volatile organic compounds (VOCs) and ammonia (NH3). The first two sources are generally known as primary emissions of $\mathrm{PM}_{2.5}$, while the third is referred to as secondary formation and generally occurs some distance from the original emission source.

Like $\mathrm{PM}_{2.5}, \mathrm{PM}_{10}$ is created by certain fuel-burning sources, particularly unfiltered or coarse fuel such as coal, wood, or certain grades of diesel. Other sources of $\mathrm{PM}_{10}$ include fugitive dust from construction sites, mining, or quarry operations; landfill activities; industrial or manufacturing processes; and natural sources such as wildfires, pollen, and microorganisms.

Nitrogen dioxide $\left(\mathrm{NO}_{2}\right)$ is one of many oxides of nitrogen $\left(\mathrm{NO}_{\mathrm{x}}\right)$ formed during high-temperature combustion when oxygen combines with nitrogen. Although all oxides of nitrogen are considered reactive, $\mathrm{NO}_{2}$ is the most stable. The exhaust gases of cars, trucks, and other petroleum-fueled combustion is the primary source of nitrogen oxide pollution. $\mathrm{NO}_{2}$ is used as an indicator for oxides of nitrogen as a precursor for $\mathrm{PM}_{2.5}$ formation, and is also a directly regulated pollutant.

The table below shows the NAAQS standards for $\mathrm{PM}_{2.5}, \mathrm{PM}_{10}$, and $\mathrm{NO}_{2}$ emissions.
NAAQS Threshold Limits and Forms

| Pollutant | Threshold | Averaging Time | Form of Calculation |
| :---: | :---: | :---: | :--- |
| $\mathbf{P M}_{\mathbf{2 . 5}}$ | $35 \mu \mathrm{~g} / \mathrm{m}^{3}$ | 24-Hour | 98th percentile averaged over 3 years |
|  | $12 \mu \mathrm{~g} / \mathrm{m}^{3}$ | Annual | Highest annual average over 3 years |
| $\mathbf{P M}_{\mathbf{1 0}}$ | $150 \mu \mathrm{~g} / \mathrm{m}^{3}$ | 24-Hour | Highest second-high over 3 years |
| $\mathbf{N O}_{\mathbf{2}}{ }^{*}$ | $188 \mu \mathrm{~g} / \mathrm{m}^{3}$ | 1-Hour | 98th percentile averaged over 3 years |
|  | $100 \mu \mathrm{~g} / \mathrm{m}^{3}$ | Annual | Highest annual average of daily <br> maximum 1-Hour values over 3 years |

*EPA presents $\mathrm{NO}_{2}$ limits in parts per billion (ppb). Values have been converted from ppb to $\mu \mathrm{g} / \mathrm{m}^{3}$ using the following formula:
$\mu \mathrm{g} / \mathrm{m}^{3}=$ molecular weight * concentration (ppb) / 24.45 (given: molecular weight of $\mathrm{NO}_{2}$ is 46.0055)
$46.0055^{*} 100 \mathrm{ppb} / 24.5=188.2 \mu \mathrm{~g} / \mathrm{m}^{3}$ )
This formula assumes temperature of 25 degrees celsius and 1.0 atmosphere of pressure.

### 3.2 Modeling Process

To assess the impact of the proposed development on these three pollutants of concern, ECS conducted modeling of the proposed project's vehicular traffic on site and upon the surrounding roadway intersections, as well as stationary emissions sources on site. The modeling performed was based on the project details received from the client. ECS compiled information about the proposed development and identified stationary and mobile sources of air emissions associated with the site. Each of these sources was then quantified and modeled under conservative or "worst-case" conditions to identify potential air quality impacts.

### 3.3 Project Details

The project is located in the Stockyards Industrial Corridor neighborhood in Southwest Chicago, which is served by principal arteries including Western Avenue, Western Boulevard and 47th Street. Based on 2018 traffic volume information from Illinois Department of Transportation (IDOT), the daily traffic volume on Western Avenue was 19,800 vehicles north of 47th Street and 22,800 vehicles south of 47th Street. IDOT considers Western Avenue as a Strategic Regional Arterial (SRA) route. Western Boulevard was not considered a SRA route and was shown to carry an average daily traffic of 15,400 vehicles.

The project location is in the northeast quadrant of the intersection of Western Boulevard with 47th Street. The project area is bounded by industrial properties to the north, railroad right-of-way to the east, West 47th Street to the south, and South Western Boulevard to the west. Table 3-1 summarizes the existing and future proposed conditions for the project site.

Table 3-1: Project Summary

|  | Existing | Proposed |
| :---: | :---: | :---: |
| Year | 2021 | 2027 |
| Site Area | Approximately 32.54 acres | Approximately 32.54 acres |
| Buildings | Three (3) single-story industrial buildings | Three (3) warehouse buildings with integrated office and distribution space |
| Enclosed Space | Approximately 366,500 square feet | Approximately 588,880 square feet |
| Parking Area(s) | Paved asphalt surface parking (unmarked)/few loading docks | Approximately 753 passenger vehicle parking spaces, 37 truck parking spaces, and 89 loading docks |

### 3.4 Analysis Domain

A Traffic Impact Study (TIS) was independently prepared for the Proposed Warehouse/Distribution Development at the Wheatland Tube Property by Kenig, Lindgren, O'Hara, Aboona, Inc. (KLOA). According to the traffic study, the base study year was 2021. The traffic study horizon year for the project was 2027. Therefore 2027 was determined to be project horizon year for the AQIA.

The TIS included six roadway intersections surrounding the development and a proposed new site entrance. According to EPA guidance, if the intersections with the greatest traffic impacts from the development do not exceed the National Ambient Air Quality Standards (NAAQS), then lesser traveled intersections are also unlikely to exceed the NAAQS. The KLOA TIS presented six intersections and the proposed future site entrance. The study area is represented by the following list of intersections:

- Intersection 1: Western Avenue \& 45th Street
- Intersection 2: Western Boulevard \& 45th Street/Site Access
- Intersection 3: Western Avenue \& 47th Street
- Intersection 4: Western Boulevard \& 47th Street
- Intersection 5: Oakley Avenue/Site Access \& 47th Street
- Intersection 6: Oakley Avenue \& 43rd Street

ECS ranked these intersections for total traffic volume and level of service for the morning and afternoon peak hours. The intersection ranking by traffic volume was $4,3,2,1,5,6$. The intersection ranking by worst levels of service was $4,3,5,6,1$, and 2 . These rankings indicate that the intersections along Western Boulevard, Western Avenue, 45th Street, and 47th Street represent the highest traffic impacts resulting from the project. Based on the EPA guidance, if these intersections do not exceed the NAAQS as a result of the project, then lesser impacted intersections are also unlikely to exceed the NAAQS as a result of the project. Based on this assessment, ECS selected the area of the roadways approaching and departing intersections 1-5 and surrounding the project site as the geographic domain for modeling air quality impacts.

### 4.0 METHODOLOGY

The modeling was performed generally in accordance with the guidance of CDPH as well as the U.S. Environmental Protection Agency (EPA) document, Transportation Conformity Guidance for Quantitative Hot-Spot Analyses in $P M_{2.5}$ and $P M_{10}$ Nonattainment and Maintenance Areas, EPA-420-B-21-037. This modeling generates an estimate of concentrations that could potentially occur in the project vicinity due to additional pollution generated by the project. These concentrations are then compared to the EPA National Ambient Air Quality Standards (NAAQS).

### 4.1 MOVES Emissions Factors

The emissions factors for local area $\mathrm{PM}_{2.5}, \mathrm{PM}_{10}$, and $\mathrm{NO}_{2}$ emissions due to development of this project were generated using the EPA MOVES computer model. MOVES stands for the Motor Vehicle Emission Simulator, a computer program designed by the EPA to estimate pollution emission rates for motor vehicle fleets under user-specified conditions. MOVES emissions factors were provided by CDPH in spreadsheet format to be utilized in AQIA projects. The project-specific emissions factors were obtained by applying the MOVES model emissions factors for $\mathrm{PM}_{2.5}, \mathrm{PM}_{10}$, and $\mathrm{NO}_{2}$ obtained from CDPH to project-specific vehicle activity data information obtained from KLOA.

The horizon year for the traffic study was 2027, therefore year 2027 was selected as the analysis year for the MOVES model. ECS utilized the trip generation rates and vehicle types presented in the traffic study to model the vehicle activity. Based on CDPH guidance, the most likely vehicle type and the most likely fuel type for each vehicle was applied. The vehicle types included passenger vehicles and short-haul combination trucks. Passenger vehicles were assumed to be gasoline fuel. Short-haul combination trucks were assumed to be diesel fuel.

For the purpose of modeling, the activity of the vehicles are defined in "links", with each link representing a segment of vehicle movement or idling time. The emissions factors derived for each link were based on vehicle speeds, distance traveled, or time spent idling. For this project, the following assumptions were made for vehicle activity:

- Vehicles in free-flow roadways were assumed to travel at 30 miles per hour (based on local roadway speed limits and traffic condition)
- Vehicles approaching signalized intersections were assumed to travel at 10 miles per hour for the distance defined in the KLOA TIS as the 50th percentile queue length
- Vehicles were assumed to idle at 0 miles per hour for the time period defined as the approach delay in the KLOA TIS for that intersection approach
- Vehicles accelerating from an intersection were assumed to travel at an average speed of 15 miles per hour for approximately seven seconds

The acceleration time assumption is calculated from the time a vehicle with a nominal acceleration of 1.4 meters per second squared would take to reach 30 miles per hour. The nominal acceleration of 1.4 meters per second squared was derived from the document Acceleration Characteristics of Starting Vehicles, Transportation Research Board 79th Annual Meeting, Paper No. 00-0980 (2000).

The vehicle activity in the on-site parking areas was estimated based on projected vehicle trip generation provided in the KLOA TIS.

- Vehicles in the parking area were assumed to travel at 5 miles per hour
- Each passenger vehicle entering the east parking lot at Buildings 1 and 2 was assumed to travel 370 meters ( 1,214 feet)
- Each vehicle entering the lots at Building 3 was assumed to travel 90 meters ( 295 feet)
- Each vehicle was assumed to idle for three minutes
- Vehicle parking lot activity was assumed to be active at peak hour rates for 24 hours per day

The moving and idling emissions were combined to provide the source emission factor for each parking area. This methodology is believed to be conservative because most vehicles will likely not travel this distance or idle for this period of time in the site parking areas. In addition, the peak hour activity rates are not projected to persist for the entire morning and afternoon of each day, but are modeled as persistent to present a conservative worst-case scenario.

The truck activity was based on the hourly truck trip generation rate provided in the KLOA TIS.

- Trucks moving on site were assumed to travel at 5 miles per hour
- Each truck was assumed to travel for 365 meters (1,200 feet) within the truck movement area
- Each truck was assumed to idle for five minutes

The moving and idling emissions were combined to provide the source emission factor for the truck movement area. This methodology is believed to be conservative because most vehicles will likely not travel this distance or idle for this period of time in the site parking areas, particularly in light of no-idle provisions in the truck parking and loading area.

### 4.2 Dispersion Modeling

The project level analysis of $\mathrm{PM}_{2.5}, \mathrm{PM}_{10}$, and $\mathrm{NO}_{2}$ pollution was conducted using the link emission rates provided by the MOVES emission factors as inputs for the American Meteorology Society (AMS)/EPA Regulatory Model (AERMOD) in general accordance with EPA and CDPH guidance. AERMOD is the EPA's regulatory dispersion model for transportation and local hot-spot projects. Modeling and analysis of air quality impacts using AERMOD requires project-specific inputs for meteorology, terrain, vehicle and other pollution source activity, building geometry, background pollutant concentrations, receptor locations, and output post-processing.

### 4.2.1 Meteorology

Because emissions and dispersion characteristics are heavily influenced by factors such as wind, temperature, and humidity, the AERMOD models requires input of both surface and upper air weather data. The weather input for the model was obtained from commercial sources and was compiled following EPA guidance. Based on the project location, ECS utilized five years of National Weather Service observational data from Chicago Midway Airport, encompassing years 2016 through 2020 for this analysis. The specific weather inputs are included with the model data files, which are submitted with this report in electronic format.

### 4.2.2 Terrain and Building Geometry

The AERMOD model requires a terrain preprocessor (AERMAP) to determine the terrain elevations and characteristics. The terrain inputs for AERMAP were obtained from the United States Geological Survey (USGS) National Elevation Dataset (NED) 30 meter resolution in geotiff format. The AERMAP output is included in the electronic data files with this document.

The project layout, roadway geometry, and building geometry for the project area was prepared using Geographic Information System (GIS) software. GIS data for the project vicinity was obtained from the Cook County GIS service (https://gis.cookcountyil.gov). A project-specific GIS map of the study intersections was prepared in accordance with EPA guidance to identify the link and building geometry. The geospatial coordinates were then exported to spreadsheet format to generate Cartesian grid AERMOD inputs for roadway links and site area sources.

### 4.2.3 Roadway Vehicle Activity Emissions Modeling

Peak hour vehicle trips generated by the proposed warehouse/distribution facility were calculated by KLOA based on generation rates contained in Trip Generation Manual, 10th Edition, published by the Institute of Transportation Engineers (ITE). According to the traffic study, it is estimated that 20 percent of the traffic approaching or departing the development will be trucks, with the remaining 80 percent being passenger vehicles. The complete TIS prepared by KLOA is included in the Appendix for reference.

The passenger vehicle traffic associated with the development was assumed to operate on roadways between 6:00 am and 6:00 pm, with morning peak hour rates applied from 6:00 am until 12:00 pm , and evening peak hour rates applied from 12:00 pm to 6:00 pm. This approach is conservative because peak hour activity is only projected to occur for one hour during the morning and one hour during the evening.

The heavy duty truck vehicle activity for this project was assumed to operate 24 hours a day, with morning peak hour rates applied from 12:00 am until 12:00 pm, and evening peak hour rates applied from 12:00 pm to 12:00 am. This approach is conservative because peak hour activity is only projected to occur for one hour during the morning and one hour during the evening, and truck activity levels in other hours would be expected to be less than the peak hour.

Based on the project information and EPA guidance, AERMOD model input was prepared for the study area roadway links. Utilizing the same intersection geometry, four sets of roadway link sources were created for the AERMOD model. The first set included the passenger vehicles for the morning peak hour. The second set included the passenger vehicles for the evening peak hour. The third set included the heavy-duty trucks for the morning peak hour, and the fourth set included the heavy duty trucks for the evening peak hour. Therefore, a total of four sets of links were prepared for the AERMOD model:

- Passenger Car Morning Peak Hour
- Passenger Car Evening Peak Hour
- Truck Morning Peak Hour
- Truck Evening Peak Hour

Passenger car and short-haul combination truck links on roadways were modeled as volume sources in AERMOD. For sources that were longer than could be captured in a single volume source, line-volume sources were used to create adjacent volume sources. Based on CDPH guidance, the model parameters assumed the passenger vehicle volume source height was 3.1 meters and the truck volume source height was 6.46 meters; the plume width was the width of the travel portion of the roadway plus 6 meters; the release height was one-half the height of the volume source; and the initial vertical and lateral dimensions of the plume were the volume width or height divided by 2.15.

### 4.2.4 Facility Emissions

The exhaust from vehicle movement on the facility grounds, and vehicles utilizing the proposed parking facilities of the project is included in the emissions analysis. A diagram of the modeled site layout and the related emissions sources is presented in the Appendix.

Based on the proposed parking facility layout, the parking facilities for this project were modeled as area sources. The site was assumed to operate for 24 hours a day, with morning peak hour rates applied from 12:00 am until 12:00 pm, and evening peak hour rates applied from 12:00 pm to 12:00 am. This approach is conservative because peak hour activity is only projected to occur for one hour during the morning and one hour during the evening.

The on-site heavy duty truck activity for this project was modeled as an area source. The truck parking, loading, and movement area was assumed to operate 24 hours a day. The hourly distribution for truck activity was obtained from the traffic study by KLOA. Details of truck activity are provided in Section 4.1.

Because no tenant has been selected for the site and no specific build-out plans have been proposed, ECS assumed a conservative heating scenario for each building with natural gas furnace for heating and natural gas boilers for hot water. The buildings were projected to utilize natural gas furnaces in the warehouse areas foir heating, with Building 1 utilizing a total of 6.6 million British Thermal Unit (BTU) natural gas heaters during peah hour (MBTUH), Building 2 utilizing 4.3 MBTUH for heating, and Building 3 utilizing 1.4 MBTUH for heating. The emissions from heating and hot water use were conservatively estimated using information from the Department of Energy (DOE) and EPA AP-42: Compilation of Air Emission Factors. The heating and hot water usage were assumed to operate 24 hours a day, 365 days per year. This is a conservative assumption because the facility is not expected
to require heating every day of the year, and hot water use will likely not be at peak occupancy levels at all hours and on all days of the week. In addition, the building is proposed to achieve Leadership in Energy and Environmental Design (LEED) certification. Due to the emissions reduction requirements associated with LEED, if fossil fuel heating is used, the actual energy use and associated emissions would likely be significantly less than the average emissions calculated based on DOE data.

Based on communication with the client, no manufacturing emissions are anticipated associated with the proposed development. No standby power generation has been proposed. Forklifts associated with the site are anticipated to be electrically powered. Based on this communication, no other emission sources were identified by ECS associated with the development.

The CDPH requirements specify consideration of all phases of the development, from construction to operation. Anticipated construction emissions associated with the development project potentially include heavy-duty machine movement. The construction phase is not anticipated to generate significant site traffic compared to the post-development phase. Another potential emission source could be fugitive dust from vehicle movement, earthwork, and demolition operations. Based on communication with the client, potential fugitive dust emissions during construction will be mitigated with appropriate prevention and control methods as good engineering practice, and as required by CDPH and the provisions of the construction permit. Based on the project description, any activities that could potentially generate construction emissions were anticipated to be transient and short-term during the construction phase of the project. Based on this assessment, the post-development phase is considered to represent the worst-case condition. Therefore, air quality impact analysis was conducted for post-development conditions based on complete build-out in 2027, and construction phase emissions were not directly assessed.

### 4.2.5 Receptor Locations

The AERMOD model calculates pollution concentrations at theoretical target locations referred to as "receptors". Receptors are virtual representations of geographic locations in the project vicinity where pollutant concentrations are calculated by dispersion modeling.

In accordance with the CDPH guidance, the following receptor inputs were used to establish the in the modeling:

- Fenceline receptors were place no more than 25 meters apart
- Nested Cartesian receptor grid with the grid spacing below:
- No more than 50 meters apart to a distance of 0.5 kilometers (km)
- No more than 100 meters apart between 0.5 and 1.5 km
- No more than 250 meters apart between 1.5 and 3 km
- No more than 500 meters apart from 3 to 5 km
- Receptors were located in all publicly accessible locations
- Terrain elevations were assigned to each source and receptor using the EPA's AERMAP terrain processing tool
- Receptors were not placed on the grounds of the project site due to the presence of a perimeter fence at the site

After running an initial assessment utilizing the above receptor parameters, ECS prepared a "heat map" indicating the modeled impacts at each receptor location. Based on the illustrated contours of the impacts using the nested Cartesian grid described above, ECS reduced the modeled area to the defined area of greatest impact. To ensure that the results captured the greatest impact locations, a
 distance of 0.5 kilometers, and a 100 meter grid to a distance of 1 kilometer to illustrate the contours of the pollution dispersion. This nested grid meets the requirements of the CPDH guidance to 1 kilometer, and no significant impacts were detected at a distance greater than one kilometer. Both wide-scale and near-scale contour maps of the nested grid are included in the appendix for reference. The contours clearly demonstrate decreasing concentrations approaching zero at the perimeter of the receptor grid.

### 4.2.6 Background Concentrations

Ambient monitoring data for the Chicago Metropolitan area was obtained from the EPA "AirData" Air Quality System database. The monitor data were averaged over the three years prior to the project (2019-2021). The monitors identified by the IEPA within the "Chicago-Naperville-Elgin, IL-IN-WI" Core Based Statistical Areas (CBSA) were evaluated to find the closest monitoring station for the criteria pollutant nearest the Project site. All results were identified as having no excluded events occurring.

Monitor data was obtained from the Com Ed Maintenance Building Trailer monitor located at 7801 Lawndale for $\mathrm{NO}_{2}$ and $\mathrm{PM}_{2.5}$ background concentrations. The Village Hall monitor located at 50th Street and Glencoe was selected to provide PM $_{10}$ background concentration data. These locations were selected as the nearest in proximity to the site with the monitoring parameters that meet the data completeness requirements.

For the annual $\mathrm{PM}_{2.5}$ and $\mathrm{NO}_{2}$ standards, the background concentration is derived from the average of the most recent three years of annual concentrations. For the 24 -hour $\mathrm{PM}_{2.5}$ standard, the background concentration is derived from the three-year average of the 98th percentile of the annual distribution of 24 -hour average concentrations. For the one-hour $\mathrm{NO}_{2}$ standard, the background concentration is derived from the three-year average of the 98th percentile of the annual distribution of daily highest 1 -hour concentrations. For the 24 -hour $\mathrm{PM}_{10}$ standard, the background concentration is derived from the average of the second-high annual concentration over the past three years.

### 4.2.7 Post-Processing

In accordance with the EPA and CDPH guidance, AERMOD was used to calculate emission dispersion based on meteorological and other input data. The output concentrations at each receptor were converted to the appropriate regulatory unit and form for each pollutant, with the background concentrations added to the peak receptor value to arrive at the project design concentration. The project design concentration is the highest predicted future concentration of pollutants based on the anticipated project-related emissions combined with ambient background concentrations. The project $\mathrm{PM}_{2.5}, \mathrm{PM}_{10}$, and $\mathrm{NO}_{2}$ modeled design concentration values were compared to the EPA NAAQS for the selected pollutants.

### 5.0 RESULTS

### 5.1 Link Emissions Factors

Based on the emission factors generated by MOVES and the vehicle activity projections by KLOA, the $\mathrm{PM}_{2.5}, \mathrm{PM}_{10}$, and $\mathrm{NO}_{2}$ emissions factors were calculated for each roadway link and on-site area source. The link emissions factor results are summarized in Table 5-1 located in the appendix.

### 5.2 Dispersion Modeling Results

The AERMOD model output presented estimated impacts from the pollutants of concern from passenger vehicle and truck emissions both on- and off-site. The peak concentrations at each receptor were added to the background values as discussed in Section 4.2. The highest modeled concentration for each pollutant is presented in the following table. The table includes the site-generated modeled impact, the ambient background concentration, and the combined project design concentration. The project design concentration is compared to the NAAQS threshold limits.

Project Design Concentrations and NAAQS

| Pollutant | Averaging <br> Period | Peak Modeled <br> Concentration <br> $\left(\boldsymbol{\mu g} / \mathbf{m}^{\mathbf{3}}\right)$ | Ambient <br> Background <br> $\left(\boldsymbol{\mu g} / \mathbf{m}^{\mathbf{3}}\right)$ | Project Design <br> Concentration <br> $\left(\boldsymbol{\mu g} / \mathbf{m}^{\mathbf{3}}\right)$ | NAAQS <br> $\left(\boldsymbol{\mu g} / \mathbf{m}^{\mathbf{3}}\right)$ | Exceed <br> NAAQS? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24 -hour | 0.70 | 19.7 | $\mathbf{2 0 . 4}$ | 35 | No |
|  | Annual | 0.14 | 8.4 | $\mathbf{8 . 5}$ | 12 | No |
| PM10 | 24 -hour | 0.65 | 112.3 | $\mathbf{1 1 3 . 0}$ | 150 | No |
|  | 1 -hour | 32.78 | 98.0 | $\mathbf{1 3 0 . 8}$ | 188 | No |
|  | Annual | 4.58 | 25.0 | $\mathbf{2 9 . 6}$ | 100 | No |

Based on the AERMOD results, the project design concentration of each pollutant was below the relevant NAAQS. Based on the calculated project design concentrations, the project appears to meet the conformity requirements for air quality in the project vicinity and the Greater Chicago Metropolitan Area.

### 6.0 CONCLUSION

ECS has conducted an AQIA analysis for the proposed Wheatland Tube Property project. The analysis was conducted in general accordance with EPA methodology for project level screening analysis, and in conformity to the guidance of the reviewing agency, the CDPH AQD. The models utilized were the current versions of the EPA recommended models for Project Level Analysis, including MOVES3 and AERMOD version 21112.

Based on the model outputs, using worst-case scenario inputs and conservative assumptions, the project design concentrations were below the EPA threshold. The peak concentration at each receptor, with the background concentration applied, predicted that the total concentrations following development of the project would be below the EPA NAAQS for each modeled pollutant.

Based on these findings, ECS concludes that the proposed project would not be expected to cause or significantly contribute to an exceedance of the NAAQS in the study area.

### 7.0 LIMITATIONS

The conclusions presented within this report are based upon the results of EPA-approved computer models prepared in accordance with guidance provided by the reviewing agency, the CDPH AQD. The models were prepared based on information obtained from the client and other parties designated by the client. All conclusions and recommendations pertaining to the subject site are limited to materials reviewed at the time this study was undertaken. No other warranty, expressed or implied, is made with regard to the conclusions and recommendations presented within this report.

This letter is provided for the exclusive use of Brookfield Properties and their prospective partners. This letter is not intended to be used or relied upon in connection with other projects or by other unidentified third parties. The use of this letter by any undesignated third party or parties would be at such party's sole risk and ECS disclaims liability for any such third party use or reliance. ECS has not completed or used any form of predetermined language to report the conclusions of this work and it is our understanding that we will not be required to do so. Compensation for this investigation is not contingent upon results, and ECS has conducted this Air Quality Analysis objectively without reference to any particular outcome desired by the client.

Appendix I: Proposed Site Plan


## Appendix II: Figures

## PROJECT TITLE:

Area and Volume Sources Layout
Wheatland Tube Company Site, Chicago, IL


PROJECT TITLE:
PM 2.5 Peak 24-Hour Concentrations
Wheatland Tube Company Site, Chicago, IL


PLOT FILE OF HIGH 1ST HIGH 24-HR VALUES FOR SOURCE GROUP: ALL
$\mathrm{ug} / \mathrm{m}^{\wedge} 3$
Max: 0.704 [ug/m^3] at $(354250.63,571609.48)$

| 0.050 | 0.100 | 0.150 | 0.200 | 0.250 | $0.300 \quad 0.350$ | 0.400 | $0.450 \quad 0.500$ | $0.550 \quad 0.6$ |  | 0.650 | 0.700 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| COMMENTS: |  |  |  |  | SOURCES: $282$ |  | COMPANY NAME: <br> ECS Midwest, LLC |  |  |  |  |
|  |  |  |  |  | RECEPTORS: $943$ |  | MODELER: <br> B. Rhett |  |  |  |  |
|  |  |  |  |  | OUTPUT TYPE: <br> Concentration |  | SCALE: <br> 0 $\qquad$ | $1: 12,000$ 0.4 km |  |  |  |
|  |  |  |  |  | MAX: <br> $0.704 \mathrm{ug} / \mathrm{m}^{\wedge} 3$ |  | DATE: <br> 8/15/2022 |  | PROJECT NO.:53:3398 |  |  |

## PROJECT TITLE:

## PM 2.5 Peak 24-Hour Concentrations

## Wheatland Tube Company Site, Chicago, IL



PLOT FILE OF HIGH 1ST HIGH 24-HR VALUES FOR SOURCE GROUP: ALL
$u g / m^{\wedge} 3$
Max: $0.704\left[\mathrm{ug} / \mathrm{m}^{\wedge} 3\right]$ at $(354250.63,571609.48)$


PM 2.5 Annual Average Concentrations Wheatland Tube Company Site, Chicago, IL


PLOT FILE OF ANNUAL VALUES AVERAGED ACROSS 5 YEARS FOR SOURCE GROUP: ALL
$\mathrm{ug} / \mathrm{m}^{\wedge} 3$
Max: $0.127\left[\mathrm{ug} / \mathrm{m}^{\wedge} 3\right]$ at $(354160.00,571315.00)$


PM 2.5 Annual Average Concentrations
Wheatland Tube Company Site, Chicago, IL


PLOT FILE OF ANNUAL VALUES AVERAGED ACROSS 5 YEARS FOR SOURCE GROUP: ALL
$\mathrm{ug} / \mathrm{m}^{\wedge} 3$
Max: $0.127\left[\mathrm{ug} / \mathrm{m}^{\wedge} 3\right]$ at $(354160.00,571315.00)$


Highest Second-High 24-hour PM10 Concentrations Wheatland Tube Company Site, Chicago, IL


PLOT FILE OF HIGH 2ND HIGH 24-HR VALUES FOR SOURCE GROUP: ALL
$u g / m^{\wedge} 3$
Max: $0.655\left[\mathrm{ug} / \mathrm{m}^{\wedge} 3\right]$ at $(354210.00,571615.00)$


Highest Second-High 24-hour PM10 Concentrations Wheatland Tube Company Site, Chicago, IL


PLOT FILE OF HIGH 2ND HIGH 24-HR VALUES FOR SOURCE GROUP: ALL
$\mathrm{ug} / \mathrm{m}^{\wedge} 3$
Max: $0.655\left[\mathrm{ug} / \mathrm{m}^{\wedge} 3\right]$ at $(354210.00,571615.00)$


PROJECT TITLE:
Peak 98th Percentile 1-hour NO2 Concentrations

## Wheatland Tube Company Site, Chicago, IL



PLOT FILE OF 8TH-HIGHEST MAX DAILY 1-HR VALUES AVERAGED OVER 5 YEARS FOR SOURCE GROUP: ALL
$\mathrm{ug} / \mathrm{m}^{\wedge} 3$
Max: $32.8\left[\mathrm{ug} / \mathrm{m}^{\wedge} 3\right]$ at $(354110.00,571165.00)$


## PROJECT TITLE:

Peak 98th Percentile 1-hour NO2 Concentrations

## Wheatland Tube Company Site, Chicago, IL



PLOT FILE OF 8TH-HIGHEST MAX DAILY 1-HR VALUES AVERAGED OVER 5 YEARS FOR SOURCE GROUP: ALL
$\mathrm{ug} / \mathrm{m}^{\wedge} 3$
Max: $32.8\left[\mathrm{ug} / \mathrm{m}^{\wedge} 3\right]$ at $(354110.00,571165.00)$


## Appendix III: Traffic Study

## Traffic Impact Study

## Proposed Warehouse/Distribution Development



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## I. Executive Summary

This report summarizes the results of a traffic impact study conducted by Kenig, Lindgren, O’Hara, Aboona, Inc. (KLOA, Inc.) for a proposed warehouse/distribution development to be built in Chicago, Illinois. The objectives of the traffic study are as follows:

- Determine the existing vehicular, pedestrian, bicycle, and public transportation conditions in the study area to establish a base condition.
- Assess the impact that the proposed development will have on transportation conditions in the area.
- Determine any street, access, bicycle, and pedestrian modifications and/or improvements that will be necessary to effectively accommodate and mitigate future conditions.

Vehicle, pedestrian, and bicycle counts were conducted during the weekday morning and weekday evening peak periods at the intersections of Western Avenue with $45^{\text {th }}$ Street and $47^{\text {th }}$ Street, Western Boulevard with $45^{\text {th }}$ Street and $47^{\text {th }}$ Street, $43^{\text {rd }}$ Street with Oakley Avenue, and $47^{\text {th }}$ Street with Oakley Avenue in order to determine the general peak hour of traffic activity during these time periods.

As proposed, the site will be redeveloped with approximately 588,880 square feet of warehouse/distribution space in three buildings. Access to the site will be provided via $45^{\text {th }}$ Street, Oakley Avenue, a proposed access drive on $47^{\text {th }}$ Street that will replace an existing Wheatland Tube Company access drive, and a proposed access drive on Western Boulevard.

Based on the preceding analyses and recommendations, the following conclusions have been made:

- Area intersections have sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no roadway improvements or traffic control modifications are required.
- The proposed access system will be adequate in accommodating the traffic estimated to be generated by the development.
- The proposed development will replace the Wheatland Tube Company which operates with a similar access system and generates truck traffic.


## 1. Introduction

This report summarizes the methodologies, results, and findings of a traffic impact study conducted by Kenig, Lindgren, O’Hara, Aboona, Inc. (KLOA, Inc.) for a proposed warehouse/distribution development to be located in Chicago, Illinois. The site, which currently contains the Wheatland Tube Company, is located in the northeast quadrant of the intersection of Western Boulevard with $47^{\text {th }}$ Street. As proposed, the site will be redeveloped with approximately 588,880 square feet of warehouse/distribution space in three buildings. Access to the site will be provided via $45^{\text {th }}$ Street, $47^{\text {th }}$ Street, Western Boulevard, Western Avenue and Oakley Avenue

The purpose of this study was to examine existing traffic conditions, assess the impact that the proposed development will have on traffic conditions in the area, and determine if any determine if any improvements to the transportation system are required to accommodate the proposed development. Figure 1 shows the location of the site in relation to the area street system. Figure 2 shows an aerial view of the site.

The sections of this report present the following:

- Existing street conditions
- A description of the proposed development
- Directional distribution of the development traffic
- Vehicle trip generation for the development
- Future traffic conditions including access to the development.
- Traffic analyses for the weekday morning and weekday evening peak hours
- Evaluation and recommendations with respect to adequacy of the site access, on-site circulation, and adjacent street system.

Traffic capacity analyses were conducted for the weekday morning and weekday evening peak hours for the following conditions:

1. Year 2021 Base Conditions - Analyzes the capacity of the existing roadway system using peak hour traffic volumes conducted in 2021 and adjusted to represent pre-pandemic conditions.
2. Year 2027 Total Projected Conditions - Analyzes the capacity of the future roadway system using the projected traffic volumes that include the Year 2021 base traffic volumes, ambient area growth not attributable to any particular development, and the additional traffic estimated to be generated by the proposed development.


Site Location
Figure 1


## 2. Existing Conditions

Existing transportation conditions in the vicinity of the site were documented based on field visits conducted by KLOA, Inc. in order to obtain a database for projecting future conditions. The following provides a description of the geographical location of the site, physical characteristics of the area street system including lane usage and traffic control devices, and existing peak hour traffic volumes.

## Site Location

The site, which currently contains the Wheatland Tube Company is generally bounded by Bevolution Group and the 4425 Western Boulevard industrial building to the north, the CSX Transportation railroad tracks to the east, Home Depot, 555 International, and Western Boulevard to the west, and the $47^{\text {th }}$ Street to the south. The area offers a mixture of residential, industrial, and commercial uses. Chase Mechanical, Surplus Tiles Direct, Altman Machinery Company, and KD Steel are located north of the site. A BP gas station and Advance Auto Parts are located in the northeast quadrant of the intersection of Western Boulevard and $47^{\text {th }}$ Street.

## Existing Street System Characteristics

The characteristics of the existing streets near the development are described below and illustrated in Figure 3. All streets are under the jurisdiction of the Chicago Department of Transportation (CDOT) unless otherwise noted.

Western Avenue is a north-south, principal arterial street that provides two lanes in each direction and runs parallel to Western Boulevard. At its signalized intersection with $45^{\text {th }}$ Street, Western Avenue provides a through lane and a shared through/right-turn lane on the northbound approach and a through lane and a shared through/left-turn lane on the southbound approach. All legs of this intersection provide high visibility crosswalks. At its signalized intersection with $47^{\text {th }}$ Street, Western Avenue provides an exclusive left-turn lane, a through lane, and a shared through/rightturn lane on both approaches. All legs of this intersection provide high visibility crosswalks. Parking is generally permitted on the west side of the street. Western Avenue is under the jurisdiction of the Illinois Department of Transportation (IDOT), is designated as a Strategic Regional Arterial (SRA) route, and carries and Annual Average Daily Traffic of 19,800 vehicles north of $47^{\text {th }}$ Steet and 22,800 vehicles south of $47^{\text {th }}$ Street (IDOT 2018).

Western Boulevard is a north-south, major collector street that provides two lanes in each direction and runs parallel to Western Avenue. At its signalized intersection with $45^{\text {th }}$ Street, Western Boulevard provides a shared through/left-turn lane and a shared through/right-turn lane on both approaches. All legs of this intersection provide high visibility crosswalks. At its signalized intersection with $47^{\text {th }}$ Street, Western Boulevard provides an exclusive left-turn lane, a through lane, and a shared through/right-turn lane on both approaches. All legs of this intersection provide high visibility crosswalks. Parking is generally permitted on the east side of the street except for Monday through Friday 7:00 A.M to 9:00 A.M. and 4:00 P.M. to 6:00 P.M. Western Boulevard is under the jurisdiction of IDOT, is not designated as an SRA route, and carries and Annual Average Daily Traffic of 15,400 vehicles.


47th Street is an east-west, minor arterial street that generally provides one lane in each direction. At its signalized intersection with Western Avenue, $47^{\text {th }}$ Street provides a shared through/left-turn lane and a shared through/right-turn lane on the eastbound approach and an exclusive left turn lane and a shared through/right-turn lane on the westbound approach. All legs of this intersection provide high visibility crosswalks. At its signalized intersection with Western Boulevard, $4^{\text {th }}$ Street provides an exclusive left turn lane and a shared through/right-turn lane on the eastbound approach and a shared through/left-turn lane and a shared through/right-turn lane on the westbound approach. At its unsignalized intersection with Oakley Avenue and the site access drive, $47^{\text {th }}$ Street provides one lane in each direction and no exclusive turn lanes. The east and south legs of this intersection provide high visibility crosswalks. Parking is generally permitted on both sides of the street. West of Western Boulevard, $47^{\text {th }}$ Street is under the jurisdiction of the Cook County Department of Transportation and Highways (CCDOTH). East of Western Boulevard, $47^{\text {th }}$ Street is under the jurisdiction of CDOT. $47^{\text {th }}$ Street carries an AADT of 11,800 vehicles east of $47^{\text {th }}$ Street and 19,300 vehicles west of $47^{\text {th }}$ Street (IDOT 2018).
$45^{\text {th }}$ Street is an east-west, local street that extends west from Oakley Avenue and provides one lane in each direction. West of Western Avenue, $45^{\text {th }}$ Street operates in a one-way eastbound only direction. At its signalized intersection with Western Avenue, $45^{\text {th }}$ Street provides a shared left-turn/through/right-turn lane on the eastbound approach and a shared left-turn/right-turn lane on the westbound approach. All legs of this intersection provide high visibility crosswalks. At its signalized intersection with Western Boulevard, $45^{\text {th }}$ Street provides a shared left-turn through/right-turn lane on both approaches. Parking is generally permitted on both sides of the street west of Western Boulevard.
$43^{\text {rd }}$ Street is an east-west, major collector street that generally provides one lane in each direction. At its unsignalized intersection with Oakley Avenue, $43^{\text {rd }}$ Street provides one lane in each direction and no exclusive turn lanes. Parking is generally permitted on both sides of the street. $43^{\text {rd }}$ Street carries an AADT of 7,800 vehicles (IDOT 2018).

Oakley Avenue is a north south, local street that generally provides one lane in each direction. The northern segment of Oakley Avenue extends from $43^{\text {rd }}$ Street to $45^{\text {th }}$ Street and the southern segment extends from $47^{\text {th }}$ Street to $49^{\text {th }}$ Street. At its unsignalized intersection with $43^{\text {rd }}$ Street, Oakley Avenue provides a shared left-turn/right-turn lane on the northbound approach. At its unsignalized intersection with $47^{\text {th }}$ Street, Oakley Avenue provides a shared left-turn/through/right-turn lane on the northbound approach and is under stop sign control. Parking is generally permitted on both sides of the street.

## Alternative Modes of Transportation

Accessibility to and from the area is enhanced by the various alternative modes of transportation serving the area as summarized below.

Public Transportation. The area is served by the Chicago Transit Authority (CTA) rapid transit via the Western Orange Line station located approximately 1,500 feet southwest of the site. The CTA Orange Line provides rapid transit rail service between the "Loop" and Midway Airport. Service is provided seven days a week and on holidays.

In addition, the following bus routes serve the immediate area and have stops near the facility:
Route $47\left(47^{\text {th }}\right)$ provides service along $47^{\text {th }}$ Street from Lake Park Avenue to Midway Airport. Service is provided seven days a week and on holidays from approximately 4:00 A.M. to 12:30 A.M. Notable stops include the CTA Green, Red, and Orange lines and Tilden High School.

Route 48 (South Damen) provides service along South Damen Avenue from the Western Avenue Orange Line station to $87^{\text {th }}$ Street. Service is provided Monday through Friday from approximately 6:30 A.M. to 9:30 A.M. and 2:00 P.M. to 6:30 P.M.

Route 49 (Western) provides service along Western Avenue from Berwyn Avenue to $79^{\text {th }}$ Street. Service is generally provided 24-hours a day every day of the week, including holidays (Night Owl Service provided on Route N49). Notable stops include the CTA Brown, Blue (O’Hare and Forest Park Branches), Pink, and Orange lines as well as multiple Metra stations.

Route X49 (Western Express) provides service along Western Avenue from Berwyn Avenue to $79^{\text {th }}$ Street. This route makes limited stops during the weekday morning (5:30 A.M. to 10:15 A.M.) and evening (2:30 P.M. to 7:00 P.M.) rush hours.

Route 94 (California) provides service along California Avenue from Addison Street to $74^{\text {th }}$ Street. Service is provided seven days a week and on holidays from approximately 5:00 A.M. to 11:30 P.M. Notable stops include the CTA Green, Pink, and Orange lines and Mount Sinai Hospital.

Pedestrian Accommodations. Sidewalks are provided on both sides of $43^{\text {rd }}$ Street, $45^{\text {th }}$ Street, $47^{\text {th }}$ Street, and the southern segment of Oakley Avenue and on the west side of Western Avenue and the east side of Western Boulevard. High-visibility crosswalks are provided at all signalized intersection within the study area and on the east and south legs of the intersection of $47^{\text {th }}$ Street with Oakley Avenue.

Bike Facilities. According to the City of Chicago’s Streets for Cycling Plan 2020, Western Avenue and Western Boulevard are as a Crosstown Bike Route.

## Year 2021 Base Traffic Volumes

In order to determine current traffic conditions in the vicinity of the site, KLOA, Inc. conducted peak period traffic counts using Miovision Scout Video Collection Units on Tuesday, June 1 and 2, 2021 during the weekday morning (6:00 A.M. to 9:00 A.M.) and weekday evening (3:00 P.M. to 6:00 P.M.) peak periods at the following intersections:

- Western Avenue with $45^{\text {th }}$ Street
- Western Avenue with $47^{\text {th }}$ Street
- Western Boulevard with $45^{\text {th }}$ Street
- Western Boulevard with $47^{\text {th }}$ Street
- $\quad 43^{\text {rd }}$ Street with Oakley Avenue
- $\quad 47^{\text {th }}$ Street with Oakley Avenue and the site access drive

The results of the traffic counts indicated that the weekday morning peak hour of traffic occurs from 7:30 A.M. to 8:30 A.M. and the weekday evening peak hour of traffic occurs from 3:30 P.M. to 4:30 P.M. Copies of the traffic count summary sheets are included in the Appendix. In order to accurately represent Year 2021 conditions due to the ongoing pandemic, the traffic volumes were compared with hourly counts previously conducted by IDOT on Western Boulevard south of the site in 2018. Based on the comparison, the 2021 traffic counts were increased by 25 percent during the weekday morning peak hour only.

Figure 4 illustrates the Year 2021 base peak hour vehicle traffic volumes, inclusive of heavy vehicles. Figure 5 illustrates the Year 2021 base heavy vehicle peak hour traffic volumes. Figure 6 illustrates the existing pedestrian and bicycle volumes, showing direction of travel.




## 3. Traffic Characteristics of the Proposed Development

In order to properly evaluate future traffic conditions in the surrounding area, it was necessary to determine the traffic characteristics of the proposed development, including the directional distribution and volumes of traffic that it will generate.

## Proposed Development Plan

As proposed, the site will be developed with approximately 588,880 square feet of warehouse/distribution space in three buildings. Access to the development is proposed to be provided as follows:

- Via $45^{\text {th }}$ Street which is signalized with Western Avenue and Western Boulevard and Oakley Avenue which is unsignalized at its intersection with $43^{\text {rd }}$ Street.
- A full movement access drive on $47^{\text {th }}$ Street located approximately 500 feet east of Western Boulevard opposite Oakley Avenue. This access drive will provide one inbound lane and one outbound lane wide enough to accommodate truck turning movements with outbound movements under stop sign control. This access drive will replace an existing access drive at this location serving Wheatland Tube Company including its truck traffic.
- A full movement access drive on the east side of Western Boulevard located approximately 300 feet north of $45^{\text {th }}$ Street. This access drive, which will primarily serve the approximate 63,320 square-foot building, will provide one inbound lane and one outbound lane with outbound movements under stop sign control.

A copy of the preliminary site plan is included in the appendix.

## Directional Distribution

The directions from which employee and truck traffic will approach and depart the site was estimated based on existing travel patterns, as determined from the traffic counts and the proposed access system of the development. Figure 7 illustrates the directional distribution of traffic. It should be noted that all truck traffic is expected to approach and depart the site via $45^{\text {th }}$ Street, which has a signalized intersection with Western Boulevard and Western Avenue, or via the $47^{\text {th }}$ Street access drive which currently serves truck traffic from Wheatland Tube Company.


## Peak Hour Traffic Volumes

The total number of peak hour vehicle trips estimated to be generated by the proposed industrial development was based on vehicle trip generation rates contained in Trip Generation Manual, $11^{\text {th }}$ Edition, published by the Institute of Transportation Engineers (ITE) for Land-Use Code 150 (Warehouse). Table 1 summarizes the trips projected to be generated by the development during the peak hours and on a daily basis. Table 5 summarizes the trips projected to be generated by the development throughout the day. Copies of the ITE trip generation sheets are included in the Appendix.

Table 1
ESTIMATED DAILY AND PEAK HOUR SITE GENERATED TRAFFIC

| ITE <br> Land- <br> Use <br> Code | Type/Size | Weekday Morning Peak Hour |  |  | Weekday Evening Peak Hour |  |  | Daily Trips |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out | Total | In | Out | Total | In | Out |
| 150 | Warehouse (588,880 s.f.) | 72 | 22 | 94 | 27 | 70 | 97 | 485 | 485 |
|  | Trucks | 8 | 12 | 20 | 13 | 11 | 24 | 177 | 177 |
| Pass | nger Vehicles | 64 | 10 | 74 | 14 | 59 | 73 | 308 | 308 |

Table 2
ESTIMATED 24-HOUR SITE GENERATED TRAFFIC

| Hour | General Light Industrial (ITE Land-Use Code 150) - 588,880 s.f. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Trucks |  |  | Passenger Vehicles |  |  | Total |  |  |
|  | In | Out | Total | In | Out | Total | In | Out | Total |
| 0:00 | 1 | 1 | 2 | 0 | 1 | 1 | 1 | 2 | 3 |
| 1:00 | 1 | 0 | 1 | 0 | 4 | 4 | 1 | 4 | 5 |
| 2:00 | 2 | 2 | 4 | 0 | 0 | 0 | 2 | 2 | 4 |
| 3:00 | 3 | 1 | 4 | 0 | 1 | 1 | 3 | 2 | 5 |
| 4:00 | 3 | 6 | 9 | 3 | 0 | 3 | 6 | 6 | 12 |
| 5:00 | 6 | 6 | 12 | 13 | 5 | 18 | 19 | 11 | 30 |
| 6:00 | 9 | 6 | 15 | 35 | 8 | 43 | 44 | 14 | 58 |
| 7:00 | 6 | 14 | 20 | 35 | 8 | 43 | 41 | 22 | 63 |
| 8:00 | 8 | 12 | 20 | 29 | 12 | 41 | 37 | 24 | 61 |
| 9:00 | 21 | 13 | 34 | 21 | 15 | 36 | 42 | 28 | 70 |
| 10:00 | 14 | 21 | 35 | 15 | 8 | 23 | 29 | 29 | 58 |
| 11:00 | 19 | 21 | 40 | 16 | 15 | 31 | 35 | 36 | 71 |
| 12:00 | 14 | 9 | 23 | 32 | 29 | 61 | 46 | 38 | 84 |
| 13:00 | 14 | 14 | 28 | 19 | 13 | 32 | 33 | 27 | 60 |
| 14:00 | 11 | 11 | 22 | 27 | 19 | 46 | 38 | 30 | 68 |
| 15:00 | 18 | 14 | 32 | 13 | 42 | 55 | 31 | 56 | 87 |
| 16:00 | 13 | 11 | 24 | 11 | 36 | 47 | 24 | 47 | 71 |
| 17:00 | 6 | 8 | 14 | 17 | 35 | 52 | 23 | 43 | 66 |
| 18:00 | 2 | 2 | 4 | 7 | 25 | 32 | 9 | 27 | 36 |
| 19:00 | 1 | 1 | 2 | 4 | 6 | 10 | 5 | 7 | 12 |
| 10:00 | 3 | 2 | 5 | 1 | 2 | 3 | 4 | 4 | 8 |
| 21:00 | 1 | 2 | 3 | 2 | 16 | 18 | 3 | 18 | 21 |
| 22:00 | 0 | 0 | 0 | 6 | 2 | 8 | 6 | 2 | 8 |
| 23:00 | 1 | 0 | 1 | 2 | 6 | 8 | 3 | 6 | 9 |
| Total | 177 | 177 | 354 | 308 | 308 | 616 | 485 | 485 | 970 |
| Based on daily trips (Table 1) and ITE's Hourly Distribution of Entering and Exiting Truck Trips and Vehicle Trips tables. |  |  |  |  |  |  |  |  |  |

## 4. Projected Traffic Conditions

The total projected traffic volumes include the existing traffic volumes, increase in background traffic due to growth, and the traffic estimated to be generated by the proposed subject development.

## Development Traffic Assignment

The estimated weekday morning and weekday evening peak hour traffic volumes that will be generated by the proposed development were assigned to the street system in accordance with the previously described directional distribution (Figure 7). Figure 8 illustrates the traffic assignment of the new passenger vehicle trips for the development. Figure 9 illustrates the traffic assignment of the new truck trips for the development.

## Ambient Traffic Growth

To account for any additional increase in traffic due to other factors or developments not previously discussed, an ambient growth factor of 0.5 percent per year was also applied to the study area over a six-year period to represent Year 2027 no-build conditions. Furthermore, in order to account for the increase in population in the study area, bicycle and pedestrian volumes were increased by 10 percent at each intersection. Figure 10 illustrates the Year 2027 No Build Volumes.

## Total Projected Traffic Volumes

The Year 2021 base traffic volumes increased by the ambient growth in the area, were combined with the new peak hour traffic volumes generated by the subject development to determine the Year 2027 total traffic volumes, shown in Figure 11. It should be noted that the existing traffic turning to and from the Wheatland Tube Company access drive on $47^{\text {th }}$ Street was removed from the area roadway system, but no traffic was removed from $45^{\text {th }}$ Street or Oakley Avenue.





## 5. Traffic Analysis and Recommendations

The following provides an evaluation conducted for the weekday morning and weekday evening peak hours. The analysis includes conducting capacity analyses to determine how well the street system and access drives are projected to operate and whether any street improvements or modifications are required.

## Traffic Analyses

Intersection analyses were performed for the weekday morning and weekday evening peak hours for the Year 2021 base and Year 2027 total projected traffic volumes.

The traffic analyses were performed using the methodologies outlined in the Transportation Research Board's Highway Capacity Manual (HCM), $6^{\text {th }}$ Edition and analyzed using Synchro/SimTraffic 11 software. The analysis for the signalized intersections were conducted utilizing actual cycle lengths, phasings, and offsets.

The analyses for the unsignalized intersections determine the average control delay to vehicles at an intersection. Control delay is the elapsed time from a vehicle joining the queue at a stop sign (includes the time required to decelerate to a stop) until its departure from the stop sign and resumption of free flow speed. The methodology analyzes each intersection approach controlled by a stop sign and considers traffic volumes on all approaches and lane characteristics.

The ability of an intersection to accommodate traffic flow is expressed in terms of level of service, which is assigned a letter from A to F based on the average control delay experienced by vehicles passing through the intersection. The Highway Capacity Manual definitions for levels of service and the corresponding control delay for signalized intersections and unsignalized intersections are included in the Appendix of this report.

Summaries of the traffic analysis results showing the level of service and overall intersection delay (measured in seconds) for the Year 2021 base and Year 2027 total projected conditions are presented in Tables 3 through 8. A discussion of the intersections follows. Summary sheets for the capacity analyses are included in the Appendix.

Table 3
CAPACITY ANALYSIS RESULTS - WESTERN AVENUE WITH $45^{\text {TH }}$ STREET


Table 4
CAPACITY ANALYSIS RESULTS - WESTERN BOULEVARD WITH $45^{\text {TH }}$ STREET


Table 5
CAPACITY ANALYSIS RESULTS - WESTERN AVENUE WITH $47{ }^{\text {TH }}$ STREET


Table 6
CAPACITY ANALYSIS RESULTS - WESTERN BOULEVARD WITH $47^{\text {TH }}$ STREET

|  | Peak <br> Hour | Eastbound |  | $\begin{gathered} \text { Westbound } \\ \hline \text { L/T/R } \end{gathered}$ | Northbound |  | Southbound |  | Overall |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | L | T/R |  | L | T/R | L | T/R |  |
|  | Weekday <br> Morning Peak Hour | $\begin{gathered} \hline \hline \text { B } \\ 18.8 \end{gathered}$ | $\begin{gathered} \hline \hline \text { C } \\ 24.8 \\ \hline \end{gathered}$ | $\begin{gathered} \text { C } \\ 34.9 \end{gathered}$ | $\begin{gathered} \hline \hline \text { B } \\ 14.6 \end{gathered}$ | $\begin{gathered} \hline \hline \mathrm{D} \\ 48.3 \end{gathered}$ | $\begin{gathered} \hline \mathrm{E} \\ 67.0 \end{gathered}$ | $\begin{gathered} \hline \hline \mathrm{D} \\ 42.9 \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ 41.5 \end{gathered}$ |
|  |  | C-23.8 |  |  | D-47.5 |  | D - 48.5 |  |  |
|  | Weekday Evening | $\begin{gathered} \hline \mathrm{B} \\ 17.7 \\ \hline \end{gathered}$ | $\begin{gathered} \text { B } \\ 19.8 \\ \hline \end{gathered}$ | $\begin{gathered} \text { D } \\ 38.8 \end{gathered}$ | $\begin{gathered} \text { C } \\ 24.3 \\ \hline \end{gathered}$ | $\begin{gathered} \text { C } \\ 34.8 \\ \hline \end{gathered}$ | $\begin{gathered} \text { C } \\ 27.1 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ 50.4 \\ \hline \end{gathered}$ | D |
|  | Peak <br> Hour | B-19.5 |  |  | C - 34.1 |  | D - 46.6 |  | 38.5 |
|  | Weekday Morning | $\begin{gathered} C \\ 20.1 \end{gathered}$ | $\begin{gathered} \text { C } \\ 28.9 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ 35.9 \end{gathered}$ | $\begin{gathered} \text { B } \\ 14.7 \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 55.3 \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 70.5 \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ 43.0 \\ \hline \end{gathered}$ | D |
|  | Peak <br> Hour | C - 27.4 |  |  | D - 54.3 |  | D - 49.4 |  | 45.3 |
|  | Weekday Evening | $\begin{gathered} \hline \text { B } \\ 18.4 \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 21.0 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ 43.6 \end{gathered}$ | $\begin{gathered} \text { C } \\ 24.9 \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 36.1 \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 27.7 \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 63.1 \end{gathered}$ | D |
|  | Peak <br> Hour | C - 20.6 |  |  | C - 35.3 |  | E-57.3 |  | 44.5 |
| Letter denotes Level of Service Delay is measured in seconds. |  |  |  | L - Left-Turns <br> T - Through |  |  | R - Right-Turns |  |  |

Table 7
CAPACITY ANALYSIS RESULTS - UNSIGNALIZED - BASE CONDITIONS

| Intersection | Weekday Morning Peak Hour |  | Weekday Evening Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |
| $43^{\text {rd }}$ Street with Oakley Avenue |  |  |  |  |
| - Eastbound Left Turn | A | 8.7 | A | 8.0 |
| - Northbound Approach | B | 13.9 | C | 15.2 |
| 47 ${ }^{\text {th }}$ Street with Oakley Avenue and the Site Access Drive |  |  |  |  |
| - Eastbound Left Turn | -- | -- | -- | -- |
| - Westbound Left Turn | A | 8.8 | A | 9.5 |
| - Northbound Approach | C | 19.5 | C | 22.3 |
| - Southbound Approach | E | 43.8 | D | 30.6 |
| LOS = Level of Service Delay is measured in seconds. |  |  |  |  |

Table 8
CAPACITY ANALYSIS RESULTS - UNSIGNALIZED - PROJECTED CONDITIONS

| Intersection | Weekday Morning Peak Hour |  | Weekday Evening Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |
| $43^{\text {rd }}$ Street with Oakley Avenue |  |  |  |  |
| - Eastbound Left Turn | A | 8.6 | A | 8.1 |
| - Northbound Approach | B | 13.4 | C | 15.9 |
| $47^{\text {th }}$ Street with Oakley Avenue and the Site Access Drive |  |  |  |  |
| - Eastbound Left Turn | A | 9.3 | B | 10.1 |
| - Westbound Left Turn | A | 8.9 | A | 9.6 |
| - Northbound Approach | C | 21.8 | C | 24.9 |
| - Southbound Approach | C | 23.7 | D | 34.1 |
| Western Boulevard the Site Access Drive |  |  |  |  |
| - Westbound Approach | -- | -- | D | 30.2 |
| - Southbound Left Turn | B | 12.7 | -- | -- |
| LOS = Level of Service <br> Delay is measured in seconds. |  |  |  |  |

## Discussion and Recommendations

The following summarizes how the intersections are projected to operate and identifies any street and traffic control improvements necessary to accommodate the development-generated traffic.

## Western Avenue with $45^{\text {th }}$ Street

The results of the capacity analysis indicate that overall, this intersection currently operates at Level of Service (LOS) B during the weekday morning and weekday evening peak hours. Furthermore, all movements operate at an acceptable LOS D or better during both peak hours and through movements on Western Avenue operate at LOS B or better.

Under Year 2027 total projected conditions, the intersection is projected to continue operating at LOS B during the weekday morning and weekday evening peak hours with increases in delay of less than one second. Furthermore, all movements are projected to continue to operate at an acceptable LOS D or better during both peak hours and through movements on Western Avenue are projected to continue to operate at LOS B or better. As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements or traffic signal modifications will be required.

## Western Avenue with $47^{\text {th }}$ Street

The results of the capacity analysis indicate that overall, this intersection currently operates at LOS A during the weekday morning peak hour and LOS B during the weekday evening peak hour. Furthermore, all movements operate at an acceptable LOS C or better during both peak hours and through movements on Western Avenue operate at LOS B or better.

Under Year 2027 total projected conditions, the overall intersection is projected to continue operating at the same LOS during the weekday morning and weekday evening peak hours with increases in delay of approximately one to two seconds. Furthermore, the westbound approach, which will accommodate outbound site traffic, is projected to operate at LOS C during both peak hours and through movements on Western Avenue are projected to continue to operate at LOS B or better during both peak hours. As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements or traffic signal modifications will be required.

## Western Avenue with $47^{\text {th }}$ Street

The results of the capacity analysis indicate that overall, this intersection currently operates at LOS D during the weekday morning peak hour and LOS C during the weekday evening peak hour. Furthermore, all the intersection movements operate at an acceptable LOS D or better during both peak hours.

Under Year 2027 total projected conditions, the overall intersection is projected to continue operating at the same LOS during the weekday morning and weekday evening peak hours with increases in delay of approximately 12 and three seconds, respectively. This increase in delay is primarily the result of the northbound right-turn movement which is projected to operate at LOS E due to the nature of Western Avenue/Western Boulevard wherein northbound right-turn vehicles may be unable to turn onto $47^{\text {th }}$ Street given the limited space. However, northbound through movements are able to bypass right-turning cars in the northbound through lane, this movement is projected to continue to operate with a volume to capacity ratio ( $\mathrm{v} / \mathrm{c}$ ) of less than one, and $95^{\text {th }}$ percentile queues for this movement are projected to increase by only one to two vehicles indicating that vehicles will still be able to turn a majority of the time. As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements or traffic signal modifications will be required.

## Western Avenue with $47^{\text {th }}$ Street

The results of the capacity analysis indicate that overall, this intersection currently operates at LOS D during the weekday morning and weekday evening peak hours. Furthermore, all the intersection movements operate at LOS E or better during both peak hours.

Under Year 2027 total projected conditions, the overall intersection is projected to continue operating at the same LOS during the weekday morning and weekday evening peak hours with increases in delay of approximately four and six seconds, respectively. Furthermore, all movements are projected to continue to operate at LOS E or better. It should be noted that westbound queues at this intersection are projected to extend up to 270 feet and will not block the location of the proposed access drive. As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements or traffic signal modifications will be required.

## 43 ${ }^{\text {rd }}$ Street with Oakley Avenue

The results of the capacity analysis indicate that the northbound movement at this intersection currently operates LOS B during the weekday morning peak hour and LOS C during the weekday evening peak hour. Furthermore, westbound left turns operate at LOS A during both peak hours.

Under Year 2027 total projected conditions, the northbound movement at this intersection, which will include outbound site traffic, is projected to continue to operate at LOS B during the weekday morning peak hour and LOS C during the weekday evening peak hour. Furthermore, westbound left turns are projected to continue to operate at LOS A during both peak hours. As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements or traffic signal modifications will be required.

## 47th Street with Oakley Avenue and the Site Access Drive

The results of the capacity analysis indicate that northbound (Oakley Avenue) movements at this intersection currently operate at LOS C during the weekday morning and weekday evening peak hours and southbound (Wheatland Tube Company) movements operate at LOS E during the weekday morning peak hour and LOS D during the weekday evening peak hours. Furthermore, eastbound and westbound left turns operate at LOS A during both peak hours.

A proposed, the Wheatland Tube Company Access Drive will be replaced with a full movement access drive serving the site. This access drive will provide one inbound lane and one outbound lane wide enough to accommodate truck turning movements with outbound movements under stop sign control.

Under Year 2027 total projected conditions, the northbound (Oakley Avenue) movement at this intersection is projected to continue to operate at LOS C during the weekday morning peak hour and LOS C during the weekday evening peak hour and the southbound (Proposed Access Drive) access drive is projected to operate at LOS C during the weekday morning peak hour and LOS D during the weekday evening peak hours. Furthermore, eastbound and westbound left turns are projected to operate at LOS B or better during both peak hours with $95^{\text {th }}$ percentile queues of one two vehicles. As such, this access drive will be adequate in accommodating the traffic generated by the development and will have a limited impact on Oakley Avenue and $47^{\text {th }}$ Street traffic.

## Western Boulevard with the Proposed Site Access Drive

As proposed, a full movement access drive will be provided on the east side of Western Boulevard located approximately 300 feet north of $45^{\text {th }}$ Street. This access drive, which will primarily serve the approximate 63,320 square-foot building, will provide one inbound lane and one outbound lane with outbound movements under stop sign control.

The results of the capacity analysis indicate that outbound movements from the access drive on to Western Boulevard are projected to operate at LOS D during the weekday evening peak hour. Furthermore, the southbound left-turn movement from Western Boulevard on to the access drive is projected to operate at LOS B during the weekday morning peak hour. As such, this access drive will be adequate in accommodating the traffic generated by the development.

## 6. Conclusion

Based on the preceding analyses and recommendations, the following conclusions have been made:

- Access to the development is proposed to be provided as follows:

0 Via $45^{\text {th }}$ Street which is signalized with Western Avenue and Western Boulevard and Oakley Avenue which is unsignalized at its intersection with $43^{\text {rd }}$ Street.
o A full movement access drive on $47^{\text {th }}$ Street located approximately 500 feet east of Western Boulevard opposite Oakley Avenue. This access drive will provide one inbound lane and one outbound lane wide enough to accommodate truck turning movements with outbound movements under stop sign control. This access drive will replace an existing access drive at this location serving Wheatland Tube Company including its truck traffic.
o A full movement access drive on the east side of Western Boulevard located approximately 300 feet north of $45^{\text {th }}$ Street. This access drive, which will primarily serve the approximate 63,320 square-foot building, will provide one inbound lane and one outbound lane with outbound movements under stop sign control.

- Area intersections have sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no roadway improvements or traffic control modifications are required.
- The proposed access system will be adequate in accommodating the traffic estimated to be generated by the development.
- The proposed development will replace the Wheatland Tube Company which operates with a similar access system and generates truck traffic.


## Appendix

## Traffic Count Summary Sheets <br> Preliminary Site Plan <br> Level of Service Criteria Capacity Analysis Summary Sheets

## Traffic Count Summary Sheets

Rosemont, Illinois, United States 60018 (847)518-9990

Count Name: 43rd Street and Oakley Avenue Site Code:
Slart Date: 06/01/2021
Page No: 1

Turning Movement Data


| Buses | 0 | 28 | 0 | - | 28 | 0 | 0 | 30 | - | 30 | 0 | 0 | 0 | - | 0 | 58 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% Buses | 0.0 | 1.8 | 0.0 | - | 1.7 | 0.0 | 0.0 | 1.4 | - | 1.4 | - | 0.0 | 0.0 | - | 0.0 | 1.5 |
| Single-Unit Trucks | 0 | 48 | 4 | - | 52 | 0 | 3 | 65 | - | 68 | 0 | 2 | 4 | - | 6 | 126 |
| \% Single-Unit Trucks | 0.0 | 3.1 | 5.3 | - | 3.2 | 0.0 | 4.8 | 3.0 | - | 3.1 | - | 3.2 | 6.9 | - | 5.0 | 3.2 |
| Articulated Trucks | 0 | 37 | 3 | - | 40 | 0 | 18 | 41 | - | 59 | 0 | 3 | 8 | - | 11 | 110 |
| \% Articulated Trucks | 0.0 | 2.4 | 4.0 | - | 2.5 | 0.0 | 29.0 | 1.9 | - | 2.7 | - | 4.8 | 13.8 | - | 9.2 | 2.8 |
| Bicycles on Road | 0 | 3 | 0 | - | 3 | 0 | 0 | 4 | - | 4 | 0 | 0 | 0 | - | 0 | 7 |
| \% Bicycles on Road | 0.0 | 0.2 | 0.0 | - | 0.2 | 0.0 | 0.0 | 0.2 | $\checkmark$ | 0.2 | - | 0.0 | 0.0 | - | 0.0 | 0.2 |
| Pedestrians | - | - | - | 5 | - | - | - | - | 4 | - | - | - | - | 15 | - | - |
| \% Pedestrians | - | - | - | 100.0 | - | - | - | - | 100.0 | - | - | - | - | 100.0 | - | - |

Kenig Lindgren O'Hara Aboona, Inc. 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018
Count Name: 43rd Street and Oakley Avenue Site Code:
Start Date:
Start Dae: 06/01/2021
(847)518-9990

Page No: 3

Turning Movement Peak Hour Data (4:30 PM)


Kenig Lindgren O'Hara Aboona, Inc 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018
(847)518-9990

Count Name: 43rd Street and Oakley Avenue Site Code:
Start Date: 06/01/2021
Page No: 4

Turning Movement Peak Hour Data (7:30 AM)


Turning Movement Data

| Start Time | 45th Street Eastbound |  |  |  |  | 45th Street <br> Westbound |  |  |  |  |  | Western Avenue Northbound |  |  |  |  |  | Western Avenue Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | App. Total | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. Total |  |
| 3:00 PM | 0 | 5 | 21 | 7 | 33 | 0 | 12 | 0 | 7 | 0 | 19 | 0 | 0 | 206 | 3 | 0 | 209 | 0 | 6 | 250 | 0 | 2 | 256 | 517 |
| 3:15 PM | 0 | 9 | 15 | 12 | 36 | 0 | 12 | 0 | 3 | 0 | 15 | 0 | 0 | 154 | 11 | 0 | 165 | 0 | 5 | 255 | 0 | 1 | 260 | 476 |
| 3:30 PM | 0 | 5 | 28 | 7 | 40 | 0 | 12 | 0 | 10 | 0 | 22 | 0 | 0 | 142 | 18 | 1 | 160 | 0 | 6 | 239 | 0 | 3 | 245 | 467 |
| 3:45 PM | 0 | 8 | 19 | 7 | 34 | 0 | 14 | 0 | 6 | 0 | 20 | 0 | 0 | 146 | 4 | 0 | 150 | 0 | 13 | 270 | 0 | 5 | 283 | 487 |
| Hourly Total | 0 | 27 | 83 | 33 | 143 | 0 | 50 | 0 | 26 | 0 | 76 | 0 | 0 | 648 | 36 | 1 | 684 | 0 | 30 | 1014 | 0 | 11 | 1044 | 1947 |
| 4:00 PM | 0 | 2 | 11 | 8 | 21 | 0 | 17 | 0 | 3 | 0 | 20 | 0 | 0 | 182 | 8 | 0 | 190 | 0 | 4 | 287 | 0 | 1 | 291 | 522 |
| 4:15 PM | 0 | 2 | 26 | 7 | 35 | 0 | 11 | 0 | 3 | 0 | 14 | 0 | 0 | 158 | 9 | 1 | 167 | 1 | 8 | 272 | 0 | 1 | 281 | 497 |
| 4:30 PM | 0 | 6 | 24 | 6 | 36 | 0 | 18 | 1 | 4 | 0 | 23 | 0 | 0 | 171 | 4 | 1 | 175 | 0 | 2 | 268 | 0 | 0 | 270 | 504 |
| 4:45 PM | 0 | 3 | 18 | 13 | 34 | 0 | 8 | 0 | 9 | 1 | 17 | 0 | 0 | 155 | 9 | 0 | 164 | 0 | 6 | 251 | 0 | 4 | 257 | 472 |
| Hourly Total | 0 | 13 | 79 | 34 | 126 | 0 | 54 | 1 | 19 | 1 | 74 | 0 | 0 | 666 | 30 | 2 | 696 | 1 | 20 | 1078 | 0 | 6 | 1099 | 1995 |
| 5:00 PM | 0 | 6 | 16 | 14 | 36 | 0 | 15 | 0 | 12 | 0 | 27 | 0 | 0 | 154 | 7 | 0 | 161 | 0 | 12 | 269 | 0 | 1 | 281 | 505 |
| 5:15 PM | 0 | 4 | 18 | 5 | 27 | 0 | 18 | 0 | 7 | 0 | 25 | 0 | 0 | 174 | 1 | 0 | 175 | 0 | 6 | 276 | 0 | 1 | 282 | 509 |
| 5:30 PM | 0 | 10 | 15 | 5 | 30 | 0 | 15 | 0 | 6 | 1 | 21 | 0 | 0 | 171 | 2 | 1 | 173 | 0 | 5 | 290 | 0 | 0 | 295 | 519 |
| 5:45 PM | 0 | 4 | 22 | 6 | 32 | 0 | 6 | 0 | 6 | 0 | 12 | 0 | 0 | 158 | 5 | 0 | 163 | 0 | 6 | 259 | 0 | 1 | 265 | 472 |
| Hourly Total | 0 | 24 | 71 | 30 | 125 | 0 | 54 | 0 | 31 | 1 | 85 | 0 | 0 | 657 | 15 | 1 | 672 | 0 | 29 | 1094 | 0 | 3 | 1123 | 2005 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 6:00 AM | 0 | 14 | 20 | 3 | 37 | 0 | 13 | 0 | 7 | 1 | 20 | 0 | 0 | 218 | 5 | 0 | 223 | 0 | 3 | 77 | 0 | 1 | 80 | 360 |
| 6:15 AM | 0 | 5 | 18 | 5 | 28 | 0 | 2 | 0 | 2 | 0 | 4 | 0 | 0 | 213 | 2 | 1 | 215 | 0 | 5 | 78 | 0 | 1 | 83 | 330 |
| 6:30 AM | 0 | 5 | 25 | 8 | 38 | 0 | 2 | 0 | 2 | 0 | 4 | 0 | 0 | 273 | 5 | 0 | 278 | 0 | 4 | 102 | 0 | 0 | 106 | 426 |
| 6:45 AM | 0 | 4 | 14 | 2 | 20 | 0 | 2 | 0 | 5 | 0 | 7 | 0 | 0 | 234 | 5 | 0 | 239 | 0 | 1 | 66 | 0 | 0 | 67 | 333 |
| Hourly Total | 0 | 28 | 77 | 18 | 123 | 0 | 19 | 0 | 16 | 1 | 35 | 0 | 0 | 938 | 17 | 1 | 955 | 0 | 13 | 323 | 0 | 2 | 336 | 1449 |
| 7:00 AM | 0 | 13 | 15 | 2 | 30 | 0 | 2 | 0 | 5 | 0 | 7 | 0 | 0 | 242 | 14 | 0 | 256 | 0 | 7 | 92 | 0 | 0 | 99 | 392 |
| 7:15 AM | 0 | 12 | 25 | 5 | 42 | 0 | 4 | 0 | 3 | 0 | 7 | 0 | 0 | 242 | 7 | 0 | 249 | 0 | 5 | 95 | 0 | 0 | 100 | 398 |
| 7:30 AM | 0 | 8 | 14 | 4 | 26 | 0 | 5 | 0 | 7 | 0 | 12 | 0 | 0 | 232 | 9 | 0 | 241 | 0 | 5 | 115 | 0 | 1 | 120 | 399 |
| 7:45 AM | 0 | 8 | 19 | 7 | 34 | 0 | 2 | 0 | 5 | 2 | 7 | 0 | 0 | 226 | 8 | 0 | 234 | 0 | 3 | 119 | 0 | 1 | 122 | 397 |
| Hourly Total | 0 | 41 | 73 | 18 | 132 | 0 | 13 | 0 | 20 | 2 | 33 | 0 | 0 | 942 | 38 | 0 | 980 | 0 | 20 | 421 | 0 | 2 | 441 | 1586 |
| 8:00 AM | 0 | 9 | 17 | 8 | 34 | 0 | 2 | 0 | 1 | 0 | 3 | 0 | 0 | 203 | 4 | 1 | 207 | 0 | 6 | 121 | 0 | 0 | 127 | 371 |
| 8:15 AM | 0 | 10 | 18 | 6 | 34 | 0 | 7 | 0 | 5 | 1 | 12 | 0 | 0 | 248 | 9 | 0 | 257 | 0 | 8 | 107 | 1 | 2 | 116 | 419 |
| 8:30 AM | 0 | 12 | 17 | 6 | 35 | 0 | 6 | 0 | 0 | 1 | 6 | 0 | 0 | 204 | 10 | 1 | 214 | 0 | 3 | 112 | 1 | 2 | 116 | 371 |
| 8:45 AM | 0 | 7 | 23 | 9 | 39 | 0 | 5 | 0 | 5 | 0 | 10 | 0 | 0 | 171 | 6 | 1 | 177 | 0 | 5 | 140 | 0 | 0 | 145 | 371 |
| Hourly Total | 0 | 38 | 75 | 29 | 142 | 0 | 20 | 0 | 11 | 2 | 31 | 0 | 0 | 826 | 29 | 3 | 855 | 0 | 22 | 480 | 2 | 4 | 504 | 1532 |
| Grand Total | 0 | 171 | 458 | 162 | 791 | 0 | 210 | 1 | 123 | 7 | 334 | 0 | 0 | 4677 | 165 | 8 | 4842 | 1 | 134 | 4410 | 2 | 28 | 4547 | 10514 |
| Approach \% | 0.0 | 21.6 | 57.9 | 20.5 | - | 0.0 | 62.9 | 0.3 | 36.8 | - | - | 0.0 | 0.0 | 96.6 | 3.4 | - | - | 0.0 | 2.9 | 97.0 | 0.0 | - | - | - |
| Total \% | 0.0 | 1.6 | 4.4 | 1.5 | 7.5 | 0.0 | 2.0 | 0.0 | 1.2 | - | 3.2 | 0.0 | 0.0 | 44.5 | 1.6 | - | 46.1 | 0.0 | 1.3 | 41.9 | 0.0 | - | 43.2 | - |
| Lights | 0 | 168 | 454 | 160 | 782 | 0 | 202 | 0 | 115 | - | 317 | 0 | 0 | 4275 | 155 | - | 4430 | 1 | 121 | 4047 | 1 | - | 4170 | 9699 |


| \% Lights | - | 98.2 | 99.1 | 98.8 | 98.9 | - | 96.2 | 0.0 | 93.5 | - | 94.9 | - | - | 91.4 | 93.9 | - | 91.5 | 100.0 | 90.3 | 91.8 | 50.0 | - | 91.7 | 92.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Buses | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 92 | 0 | - | 92 | 0 | 2 | 89 | 0 | - | 91 | 184 |
| \% Buses | - | 0.6 | 0.0 | 0.0 | 0.1 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | - | 2.0 | 0.0 | $-$ | 1.9 | 0.0 | 1.5 | 2.0 | 0.0 | - | 2.0 | 1.8 |
| Single-Unit Trucks | 0 | 0 | 2 | 1 | 3 | 0 | 2 | 0 | 1 | - | 3 | 0 | 0 | 135 | 1 | - | 136 | 0 | 4 | 141 | 0 | - | 145 | 287 |
| $\begin{gathered} \hline \text { \% Single-Unit } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 0.0 | 0.4 | 0.6 | 0.4 | - | 1.0 | 0.0 | 0.8 | - | 0.9 | - | - | 2.9 | 0.6 | - | 2.8 | 0.0 | 3.0 | 3.2 | 0.0 | - | 3.2 | 2.7 |
| Articulated Trucks | 0 | 0 | 1 | 0 | 1 | 0 | 6 | 0 | 7 | - | 13 | 0 | 0 | 173 | 8 | - | 181 | 0 | 7 | 131 | 0 | - | 138 | 333 |
| \% Articulated Trucks | - | 0.0 | 0.2 | 0.0 | 0.1 | - | 2.9 | 0.0 | 5.7 | - | 3.9 | - | - | 3.7 | 4.8 | - | 3.7 | 0.0 | 5.2 | 3.0 | 0.0 | - | 3.0 | 3.2 |
| Bicycles on Road | 0 | 2 | 1 | 1 | 4 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 2 | 1 | - | 3 | 0 | 0 | 2 | 1 | - | 3 | 11 |
| \% Bicycles on Road | - | 1.2 | 0.2 | 0.6 | 0.5 | - | 0.0 | 100.0 | 0.0 | - | 0.3 | - | - | 0.0 | 0.6 | - | 0.1 | 0.0 | 0.0 | 0.0 | 50.0 | - | 0.1 | 0.1 |
| Pedestrians | - | - | - | - | - | - | - | - | - | 7 | - | - | - | - | - | 8 | - | - | - | - | - | 28 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | 100.0 | - | - | - | - | $-$ | 100.0 | - | - | - | - | - | 100.0 | - | - |

Rosemont, Illinois, United States 60018 (847)518-9990

Count Name: 45th Street with Western Avenue Site Code:
Start Date: 06/01/2021
Page No: 3

Turning Movement Peak Hour Data (4:30 PM)

| Start Time | 45th Street Eastbound |  |  |  |  | 45th Street Westbound |  |  |  |  |  | Western Avenue Northbound |  |  |  |  |  | Western Avenue Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | App. Total | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. Total |  |
| 4:30 PM | 0 | 6 | 24 | 6 | 36 | 0 | 18 | 1 | 4 | 0 | 23 | 0 | 0 | 171 | 4 | 1 | 175 | 0 | 2 | 268 | 0 | 0 | 270 | 504 |
| 4:45 PM | 0 | 3 | 18 | 13 | 34 | 0 | 8 | 0 | 9 | 1 | 17 | 0 | 0 | 155 | 9 | 0 | 164 | 0 | 6 | 251 | 0 | 4 | 257 | 472 |
| 5:00 PM | 0 | 6 | 16 | 14 | 36 | 0 | 15 | 0 | 12 | 0 | 27 | 0 | 0 | 154 | 7 | 0 | 161 | 0 | 12 | 269 | 0 | 1 | 281 | 505 |
| 5:15 PM | 0 | 4 | 18 | 5 | 27 | 0 | 18 | 0 | 7 | 0 | 25 | 0 | 0 | 174 | 1 | 0 | 175 | 0 | 6 | 276 | 0 | 1 | 282 | 509 |
| Total | 0 | 19 | 76 | 38 | 133 | 0 | 59 | 1 | 32 | 1 | 92 | 0 | 0 | 654 | 21 | 1 | 675 | 0 | 26 | 1064 | 0 | 6 | 1090 | 1990 |
| Approach \% | 0.0 | 14.3 | 57.1 | 28.6 | - | 0.0 | 64.1 | 1.1 | 34.8 | - | - | 0.0 | 0.0 | 96.9 | 3.1 | - | - | 0.0 | 2.4 | 97.6 | 0.0 | - | - | - |
| Total \% | 0.0 | 1.0 | 3.8 | 1.9 | 6.7 | 0.0 | 3.0 | 0.1 | 1.6 | - | 4.6 | 0.0 | 0.0 | 32.9 | 1.1 | - | 33.9 | 0.0 | 1.3 | 53.5 | 0.0 | - | 54.8 | - |
| PHF | 0.000 | 0.792 | 0.792 | 0.679 | 0.924 | 0.000 | 0.819 | 0.250 | 0.667 | - | 0.852 | 0.000 | 0.000 | 0.940 | 0.583 | - | 0.964 | 0.000 | 0.542 | 0.964 | 0.000 | - | 0.966 | 0.977 |
| Lights | 0 | 19 | 75 | 38 | 132 | 0 | 58 | 0 | 32 | - | 90 | 0 | 0 | 592 | 21 | - | 613 | 0 | 24 | 1025 | 0 | - | 1049 | 1884 |
| \% Lights | - | 100.0 | 98.7 | 100.0 | 99.2 | - | 98.3 | 0.0 | 100.0 | - | 97.8 | - | - | 90.5 | 100.0 | - | 90.8 | - | 92.3 | 96.3 | - | - | 96.2 | 94.7 |
| Buses | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 17 | 0 | - | 17 | 0 | 0 | 13 | 0 | - | 13 | 30 |
| \% Buses | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | - | 2.6 | 0.0 | - | 2.5 | - | 0.0 | 1.2 | - | - | 1.2 | 1.5 |
| Single-Unit Trucks | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 13 | 0 | - | 13 | 0 | 0 | 13 | 0 | - | 13 | 27 |
| $\begin{gathered} \hline \text { \% Single-Unit } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 0.0 | 1.3 | 0.0 | 0.8 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | - | 2.0 | 0.0 | - | 1.9 | - | 0.0 | 1.2 | - | - | 1.2 | 1.4 |
| Articulated Trucks | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | - | 1 | 0 | 0 | 32 | 0 | - | 32 | 0 | 2 | 13 | 0 | - | 15 | 48 |
| \% Articulated Trucks | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 1.7 | 0.0 | 0.0 | - | 1.1 | - | - | 4.9 | 0.0 | - | 4.7 | - | 7.7 | 1.2 | - | - | 1.4 | 2.4 |
| Bicycles on Road | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 1 |
| \% Bicycles on Road | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 100.0 | 0.0 | - | 1.1 | - | - | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | - | - | 0.0 | 0.1 |
| Pedestrians | - | - | - | - | - | - | - | - | - | 1 | - | - | - | - | - | 1 | - | - | - | - | - | 6 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |

Rosemont, Illinois, United States 60018 (847)518-9990

Count Name: 45th Street with Western Avenue Site Code:
Start Date: 06/01/2021
Page No: 4

Turning Movement Peak Hour Data (7:30 AM)

| Start Time | 45th Street Eastbound |  |  |  |  | 45th Street <br> Westbound |  |  |  |  |  | Western Avenue Northbound |  |  |  |  |  | Western Avenue Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | App. <br> Total | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \\ & \hline \end{aligned}$ | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Tota |  |
| 7:30 AM | 0 | 8 | 14 | 4 | 26 | 0 | 5 | 0 | 7 | 0 | 12 | 0 | 0 | 232 | 9 | 0 | 241 | 0 | 5 | 115 | 0 | 1 | 120 | 399 |
| 7:45 AM | 0 | 8 | 19 | 7 | 34 | 0 | 2 | 0 | 5 | 2 | 7 | 0 | 0 | 226 | 8 | 0 | 234 | 0 | 3 | 119 | 0 | 1 | 122 | 397 |
| 8:00 AM | 0 | 9 | 17 | 8 | 34 | 0 | 2 | 0 | 1 | 0 | 3 | 0 | 0 | 203 | 4 | 1 | 207 | 0 | 6 | 121 | 0 | 0 | 127 | 371 |
| 8:15 AM | 0 | 10 | 18 | 6 | 34 | 0 | 7 | 0 | 5 | 1 | 12 | 0 | 0 | 248 | 9 | 0 | 257 | 0 | 8 | 107 | 1 | 2 | 116 | 419 |
| Total | 0 | 35 | 68 | 25 | 128 | 0 | 16 | 0 | 18 | 3 | 34 | 0 | 0 | 909 | 30 | 1 | 939 | 0 | 22 | 462 | 1 | 4 | 485 | 1586 |
| Approach \% | 0.0 | 27.3 | 53.1 | 19.5 | - | 0.0 | 47.1 | 0.0 | 52.9 | - | - | 0.0 | 0.0 | 96.8 | 3.2 | - | - | 0.0 | 4.5 | 95.3 | 0.2 | - | - | - |
| Total \% | 0.0 | 2.2 | 4.3 | 1.6 | 8.1 | 0.0 | 1.0 | 0.0 | 1.1 | - | 2.1 | 0.0 | 0.0 | 57.3 | 1.9 | - | 59.2 | 0.0 | 1.4 | 29.1 | 0.1 | - | 30.6 | - |
| PHF | 0.000 | 0.875 | 0.895 | 0.781 | 0.941 | 0.000 | 0.571 | 0.000 | 0.643 | - | 0.708 | 0.000 | 0.000 | 0.916 | 0.833 | - | 0.913 | 0.000 | 0.688 | 0.955 | 0.250 | - | 0.955 | 0.946 |
| Lights | 0 | 34 | 68 | 25 | 127 | 0 | 16 | 0 | 15 | - | 31 | 0 | 0 | 837 | 28 | - | 865 | 0 | 18 | 396 | 1 | $\checkmark$ | 415 | 1438 |
| \% Lights | - | 97.1 | 100.0 | 100.0 | 99.2 | - | 100.0 | - | 83.3 | - | 91.2 | - | - | 92.1 | 93.3 | - | 92.1 | - | 81.8 | 85.7 | 100.0 | - | 85.6 | 90.7 |
| Buses | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 14 | 0 | - | 14 | 0 | 2 | 18 | 0 | - | 20 | 34 |
| \% Buses | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | - | 0.0 | - | - | 1.5 | 0.0 | - | 1.5 | - | 9.1 | 3.9 | 0.0 | $\cdots$ | 4.1 | 2.1 |
| Single-Unit Trucks | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 30 | 0 | - | 30 | 0 | 1 | 23 | 0 | - | 24 | 54 |
| $\begin{aligned} & \text { \% Single-Unit } \\ & \text { Trucks } \end{aligned}$ | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | - | 0.0 | - | - | 3.3 | 0.0 | - | 3.2 | - | 4.5 | 5.0 | 0.0 | - | 4.9 | 3.4 |
| Articulated Trucks | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | - | 3 | 0 | 0 | 27 | 2 | - | 29 | 0 | 1 | 24 | 0 | $\checkmark$ | 25 | 57 |
| \% Articulated Trucks | - | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 16.7 | - | 8.8 | - | - | 3.0 | 6.7 | - | 3.1 | - | 4.5 | 5.2 | 0.0 | - | 5.2 | 3.6 |
| Bicycles on Road | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 1 | 0 | - | 1 | 3 |
| \% Bicycles on Road | - | 2.9 | 0.0 | 0.0 | 0.8 | - | 0.0 | - | 0.0 | - | 0.0 | - | - | 0.1 | 0.0 | - | 0.1 | - | 0.0 | 0.2 | 0.0 | - | 0.2 | 0.2 |
| Pedestrians | - | - | - | - | - | - | - | - | - | 3 | - | - | - | - | - | 1 | - | - | - | - | - | 4 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |

Count Name: 45th Street with Western Boulevard
Rosemont, Illinois, United States 60018 (847)518-9990

Start Date: 06/01/2021
Sart Date:

Turning Movement Data

| Start Time | 45th Street <br> Eastbound |  |  |  |  |  | 45th Street Westbound |  |  |  |  |  | Western Boulevard Northbound |  |  |  |  |  | Western Boulevard Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. |  |
| 3:00 PM | 0 | 18 | 0 | 20 | 0 | 38 | 0 | 3 | 4 | 1 | 3 | 8 | 0 | 10 | 164 | 2 | 0 | 176 | 0 | 0 | 307 | 8 | 0 | 315 | 537 |
| 3:15 PM | 0 | 12 | 0 | 11 | 0 | 23 | 0 | 1 | 0 | 1 | 3 | 2 | 0 | 7 | 201 | 1 | 0 | 209 | 0 | 0 | 367 | 6 | 0 | 373 | 607 |
| 3:30 PM | 0 | 35 | 1 | 17 | 0 | 53 | 0 | 1 | 3 | 0 | 3 | 4 | 0 | 13 | 226 | 2 | 1 | 241 | 0 | 1 | 330 | 8 | 3 | 339 | 637 |
| 3:45 PM | 0 | 20 | 0 | 12 | 2 | 32 | 0 | 0 | 2 | 0 | 4 | 2 | 0 | 12 | 216 | 0 | 2 | 228 | 0 | 0 | 389 | 8 | 2 | 397 | 659 |
| Hourly Total | 0 | 85 | 1 | 60 | 2 | 146 | 0 | 5 | 9 | 2 | 13 | 16 | 0 | 42 | 807 | 5 | 3 | 854 | 0 | 1 | 1393 | 30 | 5 | 1424 | 2440 |
| 4:00 PM | 0 | 18 | 2 | 14 | 1 | 34 | 0 | 10 | 8 | 6 | 1 | 24 | 0 | 4 | 207 | 0 | 1 | 211 | 0 | 2 | 293 | 7 | 0 | 302 | 571 |
| 4:15 PM | 0 | 25 | 0 | 15 | 0 | 40 | 0 | 3 | 2 | 4 | 0 | 9 | 0 | 9 | 185 | 2 | 0 | 196 | 0 | 2 | 366 | 5 | 0 | 373 | 618 |
| 4:30 PM | 0 | 15 | 0 | 14 | 0 | 29 | 0 | 0 | 2 | 3 | 1 | 5 | 0 | 8 | 182 | 1 | 1 | 191 | 0 | 0 | 357 | 10 | 0 | 367 | 592 |
| 4:45 PM | 0 | 18 | 1 | 12 | 0 | 31 | 0 | 1 | 2 | 3 | 1 | 6 | 0 | 10 | 190 | 6 | 0 | 206 | 0 | 0 | 345 | 8 | 0 | 353 | 596 |
| Hourly Total | 0 | 76 | 3 | 55 | 1 | 134 | 0 | 14 | 14 | 16 | 3 | 44 | 0 | 31 | 764 | 9 | 2 | 804 | 0 | 4 | 1361 | 30 | 0 | 1395 | 2377 |
| 5:00 PM | 0 | 17 | 1 | 17 | 0 | 35 | 0 | 2 | 4 | 2 | 4 | 8 | 0 | 10 | 191 | 2 | 0 | 203 | 0 | 0 | 370 | 9 | 0 | 379 | 625 |
| 5:15 PM | 0 | 13 | 0 | 12 | 0 | 25 | 0 | 2 | 1 | 7 | 1 | 10 | 0 | 14 | 189 | 2 | 0 | 205 | 0 | 0 | 336 | 14 | 1 | 350 | 590 |
| 5:30 PM | 0 | 13 | 3 | 13 | 0 | 29 | 0 | 0 | 1 | 2 | 0 | 3 | 1 | 11 | 150 | 5 | 0 | 167 | 0 | 2 | 344 | 11 | 0 | 357 | 556 |
| 5:45 PM | 0 | 11 | 2 | 15 | 0 | 28 | 0 | 2 | 1 | 3 | 0 | 6 | 0 | 5 | 170 | 3 | 0 | 178 | 0 | 1 | 334 | 5 | 1 | 340 | 552 |
| Hourly Total | 0 | 54 | 6 | 57 | 0 | 117 | 0 | 6 | 7 | 14 | 5 | 27 | 1 | 40 | 700 | 12 | 0 | 753 | 0 | 3 | 1384 | 39 | 2 | 1426 | 2323 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 6:00 AM | 0 | 15 | 7 | 6 | 1 | 28 | 0 | 14 | 15 | 5 | 1 | 34 | 0 | 2 | 181 | 2 | 1 | 185 | 0 | 5 | 54 | 2 | 0 | 61 | 308 |
| 6:15 AM | 0 | 18 | 1 | 7 | 0 | 26 | 0 | 5 | 1 | 0 | 2 | 6 | 0 | 3 | 236 | 6 | 1 | 245 | 0 | 3 | 61 | 1 | 0 | 65 | 342 |
| 6:30 AM | 0 | 17 | 2 | 8 | 0 | 27 | 0 | 0 | 1 | 0 | 2 | 1 | 0 | 1 | 270 | 0 | 0 | 271 | 0 | 1 | 65 | 3 | 0 | 69 | 368 |
| 6:45 AM | 0 | 23 | 2 | 5 | 0 | 30 | 0 | 0 | 1 | 0 | 2 | 1 | 0 | 3 | 256 | 3 | 0 | 262 | 0 | 0 | 73 | 0 | 0 | 73 | 366 |
| Hourly Total | 0 | 73 | 12 | 26 | 1 | 111 | 0 | 19 | 18 | 5 | 7 | 42 | 0 | 9 | 943 | 11 | 2 | 963 | 0 | 9 | 253 | 6 | 0 | 268 | 1384 |
| 7:00 AM | 0 | 20 | 2 | 7 | 0 | 29 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 4 | 231 | 3 | 0 | 238 | 0 | 2 | 72 | 3 | 0 | 77 | 345 |
| 7:15 AM | 0 | 25 | 1 | 11 | 0 | 37 | 0 | 2 | 1 | 1 | 0 | 4 | 0 | 3 | 249 | 5 | 0 | 257 | 0 | 1 | 102 | 0 | 0 | 103 | 401 |
| 7:30 AM | 0 | 19 | 2 | 8 | 0 | 29 | 0 | 0 | 1 | 0 | 4 | 1 | 0 | 5 | 277 | 2 | 0 | 284 | 0 | 1 | 116 | 4 | 1 | 121 | 435 |
| 7:45 AM | 0 | 21 | 0 | 8 | 0 | 29 | 0 | 0 | 2 | 3 | 1 | 5 | 0 | 8 | 265 | 2 | 0 | 275 | 0 | 3 | 105 | 3 | 0 | 111 | 420 |
| Hourly Total | 0 | 85 | 5 | 34 | 0 | 124 | 0 | 2 | 5 | 4 | 5 | 11 | 0 | 20 | 1022 | 12 | 0 | 1054 | 0 | 7 | 395 | 10 | 1 | 412 | 1601 |
| 8:00 AM | 0 | 14 | 4 | 7 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 231 | 0 | 1 | 231 | 0 | 3 | 103 | 1 | 0 | 107 | 363 |
| 8:15 AM | 0 | 28 | 2 | 12 | 0 | 42 | 0 | 0 | 1 | 0 | 2 | 1 | 0 | 6 | 201 | 0 | 1 | 207 | 0 | 0 | 109 | 4 | 0 | 113 | 363 |
| 8:30 AM | 0 | 19 | 2 | 5 | 0 | 26 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 5 | 218 | 3 | 1 | 226 | 0 | 2 | 112 | 4 | 0 | 118 | 371 |
| 8:45 AM | 0 | 19 | 0 | 10 | 0 | 29 | 0 | 1 | 1 | 0 | 2 | 2 | 0 | 8 | 221 | 0 | 1 | 229 | 0 | 0 | 112 | 2 | 0 | 114 | 374 |
| Hourly Total | 0 | 80 | 8 | 34 | 0 | 122 | 0 | 2 | 2 | 0 | 4 | 4 | 0 | 19 | 871 | 3 | 4 | 893 | 0 | 5 | 436 | 11 | 0 | 452 | 1471 |
| Grand Total | 0 | 453 | 35 | 266 | 4 | 754 | 0 | 48 | 55 | 41 | 37 | 144 | 1 | 161 | 5107 | 52 | 11 | 5321 | 0 | 29 | 5222 | 126 | 8 | 5377 | 11596 |
| Approach \% | 0.0 | 60.1 | 4.6 | 35.3 | - | - | 0.0 | 33.3 | 38.2 | 28.5 | - | - | 0.0 | 3.0 | 96.0 | 1.0 | - | - | 0.0 | 0.5 | 97.1 | 2.3 | - | - | - |
| Total \% | 0.0 | 3.9 | 0.3 | 2.3 | - | 6.5 | 0.0 | 0.4 | 0.5 | 0.4 | - | 1.2 | 0.0 | 1.4 | 44.0 | 0.4 | - | 45.9 | 0.0 | 0.3 | 45.0 | 1.1 | - | 46.4 | - |
| Lights | 0 | 448 | 20 | 259 | - | 727 | 0 | 45 | 44 | 40 | - | 129 | 1 | 158 | 5023 | 43 | - | 5225 | 0 | 27 | 5142 | 122 | - | 5291 | 11372 |


| \% Lights | - | 98.9 | 57.1 | 97.4 | - | 96.4 | - | 93.8 | 80.0 | 97.6 | - | 89.6 | 100.0 | 98.1 | 98.4 | 82.7 | - | 98.2 | - | 93.1 | 98.5 | 96.8 | - | 98.4 | 98.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Buses | 0 | 1 | 0 | 2 | - | 3 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 26 | 0 | - | 26 | 0 | 0 | 23 | 0 | - | 23 | 52 |
| \% Buses | - | 0.2 | 0.0 | 0.8 | - | 0.4 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | - | 0.5 | - | 0.0 | 0.4 | 0.0 | - | 0.4 | 0.4 |
| Single-Unit Trucks | 0 | 3 | 2 | 2 | - | 7 | 0 | 1 | 1 | 1 | - | 3 | 0 | 1 | 45 | 1 | - | 47 | 0 | 1 | 42 | 2 | - | 45 | 102 |
| $\begin{gathered} \text { \% Single-Unit } \\ \text { Trucks } \end{gathered}$ | - | 0.7 | 5.7 | 0.8 | - | 0.9 | - | 2.1 | 1.8 | 2.4 | - | 2.1 | 0.0 | 0.6 | 0.9 | 1.9 | - | 0.9 | - | 3.4 | 0.8 | 1.6 | - | 0.8 | 0.9 |
| Articulated Trucks | 0 | 1 | 12 | 2 | - | 15 | 0 | 2 | 9 | 0 | - | 11 | 0 | 2 | 8 | 8 | - | 18 | 0 | 1 | 14 | 2 | - | 17 | 61 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 0.2 | 34.3 | 0.8 | - | 2.0 | - | 4.2 | 16.4 | 0.0 | - | 7.6 | 0.0 | 1.2 | 0.2 | 15.4 | - | 0.3 | - | 3.4 | 0.3 | 1.6 | - | 0.3 | 0.5 |
| Bicycles on Road | 0 | 0 | 1 | 1 | - | 2 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 5 | 0 | - | 5 | 0 | 0 | 1 | 0 | - | 1 | 9 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \end{gathered}$ | - | 0.0 | 2.9 | 0.4 | - | 0.3 | - | 0.0 | 1.8 | 0.0 | - | 0.7 | 0.0 | 0.0 | 0.1 | 0.0 | - | 0.1 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.1 |
| Pedestrians | - | - | - | - | 4 | - | - | - | - | - | 37 | - | - | - | - | - | 11 | - | - | - | - | - | 8 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | 9575 W. Higgins Rd., Suite 400

Count Name: 45th Street with Western Boulevard
Rosemont, Illinois, United States 60018
Site Code:
Start Date: 06/01/2021
Part No: 3

Turning Movement Peak Hour Data (4:30 PM)

| Start Time | 45th Street <br> Eastbound |  |  |  |  |  | 45th Street <br> Westbound |  |  |  |  |  | Western Boulevard Northbound |  |  |  |  |  | Western Boulevard Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. Total |  |
| 4:30 PM | 0 | 15 | 0 | 14 | 0 | 29 | 0 | 0 | 2 | 3 | 1 | 5 | 0 | 8 | 182 | 1 | 1 | 191 | 0 | 0 | 357 | 10 | 0 | 367 | 592 |
| 4:45 PM | 0 | 18 | 1 | 12 | 0 | 31 | 0 | 1 | 2 | 3 | 1 | 6 | 0 | 10 | 190 | 6 | 0 | 206 | 0 | 0 | 345 | 8 | 0 | 353 | 596 |
| 5:00 PM | 0 | 17 | 1 | 17 | 0 | 35 | 0 | 2 | 4 | 2 | 4 | 8 | 0 | 10 | 191 | 2 | 0 | 203 | 0 | 0 | 370 | 9 | 0 | 379 | 625 |
| 5:15 PM | 0 | 13 | 0 | 12 | 0 | 25 | 0 | 2 | 1 | 7 | 1 | 10 | 0 | 14 | 189 | 2 | 0 | 205 | 0 | 0 | 336 | 14 | 1 | 350 | 590 |
| Total | 0 | 63 | 2 | 55 | 0 | 120 | 0 | 5 | 9 | 15 | 7 | 29 | 0 | 42 | 752 | 11 | 1 | 805 | 0 | 0 | 1408 | 41 | 1 | 1449 | 2403 |
| Approach \% | 0.0 | 52.5 | 1.7 | 45.8 | - | - | 0.0 | 17.2 | 31.0 | 51.7 | - | - | 0.0 | 5.2 | 93.4 | 1.4 | - | - | 0.0 | 0.0 | 97.2 | 2.8 | - | - | - |
| Total \% | 0.0 | 2.6 | 0.1 | 2.3 | - | 5.0 | 0.0 | 0.2 | 0.4 | 0.6 | $\checkmark$ | 1.2 | 0.0 | 1.7 | 31.3 | 0.5 | - | 33.5 | 0.0 | 0.0 | 58.6 | 1.7 | - | 60.3 | - |
| PHF | 0.000 | 0.875 | 0.500 | 0.809 | - | 0.857 | 0.000 | 0.625 | 0.563 | 0.536 | - | 0.725 | 0.000 | 0.750 | 0.984 | 0.458 | - | 0.977 | 0.000 | 0.000 | 0.951 | 0.732 | - | 0.956 | 0.961 |
| Lights | 0 | 62 | 1 | 55 | - | 118 | 0 | 5 | 8 | 15 | - | 28 | 0 | 42 | 740 | 9 | $\checkmark$ | 791 | 0 | 0 | 1397 | 41 | - | 1438 | 2375 |
| \% Lights | - | 98.4 | 50.0 | 100.0 | - | 98.3 | - | 100.0 | 88.9 | 100.0 | - | 96.6 | - | 100.0 | 98.4 | 81.8 | - | 98.3 | - | - | 99.2 | 100.0 | - | 99.2 | 98.8 |
| Buses | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 4 | 0 | - | 4 | 0 | 0 | 3 | 0 | - | 3 | 7 |
| \% Buses | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.5 | 0.0 | - | 0.5 | - | - | 0.2 | 0.0 | $\checkmark$ | 0.2 | 0.3 |
| Single-Unit Trucks | 0 | 1 | 0 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 7 | 0 | - | 7 | 0 | 0 | 6 | 0 | - | 6 | 14 |
| $\begin{gathered} \% \text { Single-Unit } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 1.6 | 0.0 | 0.0 | - | 0.8 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.9 | 0.0 | - | 0.9 | - | - | 0.4 | 0.0 | - | 0.4 | 0.6 |
| Articulated Trucks | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | 2 | - | 3 | 0 | 0 | 2 | 0 | - | 2 | 6 |
| \% Articulated Trucks | - | 0.0 | 50.0 | 0.0 | - | 0.8 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | . | 0.0 | 0.1 | 18.2 | - | 0.4 | . | - | 0.1 | 0.0 | - | 0.1 | 0.2 |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 1 |
| \% Bicycles on Road | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 11.1 | 0.0 | - | 3.4 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | . | . | 0.0 | 0.0 | - | 0.0 | 0.0 |
| Pedestrians | - | - | - | - | 0 | - | - | - | - | - | 7 | - | - | - | - | - | 1 | - | - | - | - | - | 1 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | 9575 W. Higgins Rd., Suite 400

Count Name: 45th Street with Western Boulevard
Rosemont, Illinois, United States 60018 (847)518-9990

Turning Movement Peak Hour Data (7:30 AM)

| Start Time | 45th Street <br> Eastbound |  |  |  |  |  | 45th Street <br> Westbound |  |  |  |  |  | Western Boulevard Northbound |  |  |  |  |  | Western Boulevard Southbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. Total | Int. Total |
| 7:30 AM | 0 | 19 | 2 | 8 | 0 | 29 | 0 | 0 | 1 | 0 | 4 | 1 | 0 | 5 | 277 | 2 | 0 | 284 | 0 | 1 | 116 | 4 | 1 | 121 | 435 |
| 7:45 AM | 0 | 21 | 0 | 8 | 0 | 29 | 0 | 0 | 2 | 3 | 1 | 5 | 0 | 8 | 265 | 2 | 0 | 275 | 0 | 3 | 105 | 3 | 0 | 111 | 420 |
| 8:00 AM | 0 | 14 | 4 | 7 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 231 | 0 | 1 | 231 | 0 | 3 | 103 | 1 | 0 | 107 | 363 |
| 8:15 AM | 0 | 28 | 2 | 12 | 0 | 42 | 0 | 0 | 1 | 0 | 2 | 1 | 0 | 6 | 201 | 0 | 1 | 207 | 0 | 0 | 109 | 4 | 0 | 113 | 363 |
| Total | 0 | 82 | 8 | 35 | 0 | 125 | 0 | 0 | 4 | 3 | 7 | 7 | 0 | 19 | 974 | 4 | 2 | 997 | 0 | 7 | 433 | 12 | 1 | 452 | 1581 |
| Approach \% | 0.0 | 65.6 | 6.4 | 28.0 | - | - | 0.0 | 0.0 | 57.1 | 42.9 | - | - | 0.0 | 1.9 | 97.7 | 0.4 | - | - | 0.0 | 1.5 | 95.8 | 2.7 | - | - | - |
| Total \% | 0.0 | 5.2 | 0.5 | 2.2 | - | 7.9 | 0.0 | 0.0 | 0.3 | 0.2 | - | 0.4 | 0.0 | 1.2 | 61.6 | 0.3 | - | 63.1 | 0.0 | 0.4 | 27.4 | 0.8 | - | 28.6 | - |
| PHF | 0.000 | 0.732 | 0.500 | 0.729 | - | 0.744 | 0.000 | 0.000 | 0.500 | 0.250 | - | 0.350 | 0.000 | 0.594 | 0.879 | 0.500 | - | 0.878 | 0.000 | 0.583 | 0.933 | 0.750 | - | 0.934 | 0.909 |
| Lights | 0 | 81 | 5 | 33 | - | 119 | 0 | 0 | 1 | 3 | - | 4 | 0 | 19 | 953 | 3 | $\checkmark$ | 975 | 0 | 7 | 417 | 12 | - | 436 | 1534 |
| \% Lights | - | 98.8 | 62.5 | 94.3 | - | 95.2 | - | - | 25.0 | 100.0 | - | 57.1 | - | 100.0 | 97.8 | 75.0 | - | 97.8 | - | 100.0 | 96.3 | 100.0 | - | 96.5 | 97.0 |
| Buses | 0 | 1 | 0 | 1 | - | 2 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 5 | 0 | - | 5 | 0 | 0 | 5 | 0 | - | 5 | 12 |
| \% Buses | - | 1.2 | 0.0 | 2.9 | - | 1.6 | - | - | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.5 | 0.0 | - | 0.5 | - | 0.0 | 1.2 | 0.0 | - | 1.1 | 0.8 |
| Single-Unit Trucks | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 13 | 0 | - | 13 | 0 | 0 | 10 | 0 | $\checkmark$ | 10 | 24 |
| $\begin{gathered} \% \text { Single-Unit } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 0.0 | 12.5 | 0.0 | - | 0.8 | - | - | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 1.3 | 0.0 | - | 1.3 | - | 0.0 | 2.3 | 0.0 | - | 2.2 | 1.5 |
| Articulated Trucks | 0 | 0 | 2 | 1 | - | 3 | 0 | 0 | 3 | 0 | - | 3 | 0 | 0 | 3 | 1 | - | 4 | 0 | 0 | 1 | 0 | - | 1 | 11 |
| \% Articulated Trucks | . | 0.0 | 25.0 | 2.9 | - | 2.4 | - | - | 75.0 | 0.0 | - | 42.9 | . | 0.0 | 0.3 | 25.0 | - | 0.4 | . | 0.0 | 0.2 | 0.0 | - | 0.2 | 0.7 |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 |
| \% Bicycles on Road | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | . | 0.0 | 0.0 | - | 0.0 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 |
| Pedestrians | - | - | - | - | 0 | - | - | - | - | - | 7 | - | - | - | - | - | 2 | - | - | - | - | - | 1 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |


| Start Time | 47th Street <br> Eastbound |  |  |  |  |  | 47th Street <br> Westbound |  |  |  |  |  | Western Avenue Northbound |  |  |  |  |  | Western Avenue Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { Tpp. } \\ & \text { Tot } \end{aligned}$ | U-Turn | Left | Thru | Right | Peds | App. <br> Total |  |
| 3:00 PM | 0 | 8 | 61 | 14 | 17 | 83 | 0 | 13 | 85 | 22 | 2 | 120 | 0 | 14 | 164 | 6 | 5 | 184 | 0 | 25 | 192 | 28 | 11 | 245 | 632 |
| 3:15 PM | 0 | 7 | 61 | 11 | 17 | 79 | 0 | 13 | 92 | 3 | 0 | 108 | 0 | 21 | 176 | 14 | 9 | 211 | 0 | 22 | 215 | 24 | 7 | 261 | 659 |
| 3:30 PM | 0 | 7 | 67 | 11 | 24 | 85 | 0 | 15 | 96 | 21 | 1 | 132 | 0 | 16 | 152 | 18 | 12 | 186 | 0 | 24 | 193 | 22 | 11 | 239 | 642 |
| 3:45 PM | 0 | 9 | 78 | 11 | 14 | 98 | 0 | 22 | 98 | 19 | 0 | 139 | 0 | 22 | 119 | 5 | 9 | 146 | 0 | 20 | 220 | 28 | 2 | 268 | 651 |
| Hourly Total | 0 | 31 | 267 | 47 | 72 | 345 | 0 | 63 | 371 | 65 | 3 | 499 | 0 | 73 | 611 | 43 | 35 | 727 | 0 | 91 | 820 | 102 | 31 | 1013 | 2584 |
| 4:00 PM | 0 | 13 | 76 | 12 | 18 | 101 | 0 | 23 | 80 | 22 | 2 | 125 | 0 | 27 | 148 | 9 | 9 | 184 | 0 | 19 | 225 | 22 | 6 | 266 | 676 |
| 4:15 PM | 0 | 7 | 75 | 8 | 15 | 90 | 0 | 25 | 84 | 11 | 4 | 120 | 0 | 32 | 155 | 20 | 10 | 207 | 0 | 21 | 207 | 26 | 13 | 254 | 671 |
| 4:30 PM | 0 | 5 | 74 | 14 | 17 | 93 | 0 | 24 | 109 | 16 | 4 | 149 | 0 | 31 | 154 | 9 | 4 | 194 | 0 | 30 | 203 | 27 | 8 | 260 | 696 |
| 4:45 PM | 0 | 8 | 84 | 8 | 30 | 100 | 0 | 22 | 103 | 11 | 3 | 136 | 0 | 21 | 153 | 11 | 6 | 185 | 0 | 22 | 224 | 26 | 5 | 272 | 693 |
| Hourly Total | 0 | 33 | 309 | 42 | 80 | 384 | 0 | 94 | 376 | 60 | 13 | 530 | 0 | 111 | 610 | 49 | 29 | 770 | 0 | 92 | 859 | 101 | 32 | 1052 | 2736 |
| 5:00 PM | 0 | 9 | 78 | 6 | 24 | 93 | 0 | 19 | 93 | 15 | 3 | 127 | 0 | 18 | 142 | 11 | 7 | 171 | 0 | 25 | 239 | 21 | 9 | 285 | 676 |
| 5:15 PM | 0 | 9 | 82 | 14 | 16 | 105 | 0 | 24 | 103 | 21 | 0 | 148 | 0 | 28 | 142 | 16 | 10 | 186 | 0 | 20 | 240 | 27 | 14 | 287 | 726 |
| 5:30 PM | 0 | 11 | 76 | 14 | 20 | 101 | 0 | 26 | 100 | 13 | 3 | 139 | 0 | 18 | 150 | 9 | 8 | 177 | 0 | 16 | 258 | 22 | 15 | 296 | 713 |
| 5:45 PM | 0 | 11 | 62 | 8 | 8 | 81 | 0 | 20 | 77 | 13 | 1 | 110 | 0 | 27 | 132 | 13 | 6 | 172 | 0 | 21 | 211 | 33 | 10 | 265 | 628 |
| Hourly Total | 0 | 40 | 298 | 42 | 68 | 380 | 0 | 89 | 373 | 62 | 7 | 524 | 0 | 91 | 566 | 49 | 31 | 706 | 0 | 82 | 948 | 103 | 48 | 1133 | 2743 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 6:00 AM | 0 | 12 | 43 | 14 | 3 | 69 | 0 | 6 | 41 | 19 | 0 | 66 | 0 | 12 | 198 | 4 | 0 | 214 | 0 | 10 | 69 | 14 | 1 | 93 | 442 |
| 6:15 AM | 0 | 10 | 58 | 10 | 6 | 78 | 0 | 14 | 56 | 17 | 2 | 87 | 0 | 10 | 190 | 6 | 6 | 206 | 0 | 8 | 57 | 3 | 5 | 68 | 439 |
| 6:30 AM | 0 | 16 | 52 | 9 | 7 | 77 | 0 | 6 | 36 | 14 | 3 | 56 | 0 | 10 | 232 | 7 | 5 | 249 | 0 | 14 | 73 | 13 | 12 | 100 | 482 |
| 6:45 AM | 0 | 10 | 64 | 12 | 3 | 86 | 0 | 8 | 52 | 18 | 1 | 78 | 0 | 19 | 200 | 5 | 9 | 224 | 0 | 8 | 68 | 6 | 5 | 82 | 470 |
| Hourly Total | 0 | 48 | 217 | 45 | 19 | 310 | 0 | 34 | 185 | 68 | 6 | 287 | 0 | 51 | 820 | 22 | 20 | 893 | 0 | 40 | 267 | 36 | 23 | 343 | 1833 |
| 7:00 AM | 0 | 9 | 48 | 14 | 15 | 71 | 0 | 8 | 35 | 20 | 0 | 63 | 0 | 13 | 221 | 10 | 4 | 244 | 0 | 10 | 73 | 4 | 2 | 87 | 465 |
| 7:15 AM | 0 | 4 | 51 | 7 | 6 | 62 | 0 | 12 | 45 | 14 | 0 | 71 | 0 | 15 | 228 | 7 | 5 | 250 | 0 | 18 | 78 | 7 | 4 | 103 | 486 |
| 7:30 AM | 0 | 13 | 66 | 11 | 5 | 90 | 0 | 12 | 50 | 14 | 2 | 76 | 0 | 14 | 220 | 12 | 2 | 246 | 0 | 11 | 102 | 14 | 8 | 127 | 539 |
| 7:45 AM | 0 | 5 | 54 | 19 | 0 | 78 | 0 | 13 | 51 | 14 | 0 | 78 | 0 | 17 | 214 | 7 | 2 | 238 | 0 | 12 | 103 | 11 | 5 | 126 | 520 |
| Hourly Total | 0 | 31 | 219 | 51 | 26 | 301 | 0 | 45 | 181 | 62 | 2 | 288 | 0 | 59 | 883 | 36 | 13 | 978 | 0 | 51 | 356 | 36 | 19 | 443 | 2010 |
| 8:00 AM | 0 | 9 | 68 | 10 | 3 | 87 | 0 | 8 | 66 | 20 | 1 | 94 | 0 | 16 | 182 | 13 | 3 | 211 | 0 | 19 | 86 | 13 | 2 | 118 | 510 |
| 8:15 AM | 0 | 11 | 53 | 8 | 6 | 72 | 0 | 18 | 65 | 24 | 1 | 107 | 0 | 10 | 221 | 16 | 6 | 247 | 0 | 6 | 87 | 18 | 3 | 111 | 537 |
| 8:30 AM | 0 | 6 | 59 | 8 | 10 | 73 | 0 | 14 | 57 | 18 | 2 | 89 | 0 | 12 | 198 | 11 | 11 | 221 | 0 | 14 | 90 | 14 | 7 | 118 | 501 |
| 8:45 AM | 0 | 16 | 68 | 7 | 11 | 91 | 0 | 7 | 43 | 18 | 1 | 68 | 0 | 17 | 165 | 6 | 0 | 188 | 0 | 10 | 132 | 16 | 7 | 158 | 505 |
| Hourly Total | 0 | 42 | 248 | 33 | 30 | 323 | 0 | 47 | 231 | 80 | 5 | 358 | 0 | 55 | 766 | 46 | 20 | 867 | 0 | 49 | 395 | 61 | 19 | 505 | 2053 |
| Grand Total | 0 | 225 | 1558 | 260 | 295 | 2043 | 0 | 372 | 1717 | 397 | 36 | 2486 | 0 | 440 | 4256 | 245 | 148 | 4941 | 0 | 405 | 3645 | 439 | 172 | 4489 | 13959 |
| Approach \% | 0.0 | 11.0 | 76.3 | 12.7 | - | - | 0.0 | 15.0 | 69.1 | 16.0 | - | - | 0.0 | 8.9 | 86.1 | 5.0 | - | - | 0.0 | 9.0 | 81.2 | 9.8 | - | - | - |
| Total \% | 0.0 | 1.6 | 11.2 | 1.9 | - | 14.6 | 0.0 | 2.7 | 12.3 | 2.8 | - | 17.8 | 0.0 | 3.2 | 30.5 | 1.8 | - | 35.4 | 0.0 | 2.9 | 26.1 | 3.1 | - | 32.2 | - |
| Lights | 0 | 198 | 1420 | 152 | - | 1770 | 0 | 329 | 1545 | 356 | - | 2230 | 0 | 338 | 3892 | 197 | - | 4427 | 0 | 388 | 3319 | 414 | - | 4121 | 12548 |


| \% Lights | - | 88.0 | 91.1 | 58.5 | - | 86.6 | - | 88.4 | 90.0 | 89.7 | - | 89.7 | - | 76.8 | 91.4 | 80.4 | - | 89.6 | - | 95.8 | 91.1 | 94.3 | - | 91.8 | 89.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Buses | 0 | 0 | 28 | 30 | - | 58 | 0 | 18 | 33 | 4 | - | 55 | 0 | 27 | 88 | 19 | - | 134 | 0 | 1 | 82 | 2 | - | 85 | 332 |
| \% Buses | - | 0.0 | 1.8 | 11.5 | - | 2.8 | - | 4.8 | 1.9 | 1.0 | - | 2.2 | - | 6.1 | 2.1 | 7.8 | - | 2.7 | - | 0.2 | 2.2 | 0.5 | - | 1.9 | 2.4 |
| Single-Unit Trucks | 0 | 19 | 70 | 38 | - | 127 | 0 | 9 | 81 | 11 | - | 101 | 0 | 21 | 118 | 17 | - | 156 | 0 | 12 | 112 | 14 | - | 138 | 522 |
| $\begin{gathered} \text { \% Single-Unit } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 8.4 | 4.5 | 14.6 | - | 6.2 | - | 2.4 | 4.7 | 2.8 | - | 4.1 | - | 4.8 | 2.8 | 6.9 | - | 3.2 | - | 3.0 | 3.1 | 3.2 | - | 3.1 | 3.7 |
| Articulated Trucks | 0 | 8 | 38 | 40 | - | 86 | 0 | 15 | 53 | 25 | - | 93 | 0 | 54 | 153 | 11 | - | 218 | 0 | 4 | 131 | 9 | - | 144 | 541 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 3.6 | 2.4 | 15.4 | - | 4.2 | - | 4.0 | 3.1 | 6.3 | - | 3.7 | - | 12.3 | 3.6 | 4.5 | - | 4.4 | - | 1.0 | 3.6 | 2.1 | - | 3.2 | 3.9 |
| Bicycles on Road | 0 | 0 | 2 | 0 | - | 2 | 0 | 1 | 5 | 1 | - | 7 | 0 | 0 | 5 | 1 | - | 6 | 0 | 0 | 1 | 0 | - | 1 | 16 |
| \% Bicycles on Road | - | 0.0 | 0.1 | 0.0 | - | 0.1 | - | 0.3 | 0.3 | 0.3 | - | 0.3 | - | 0.0 | 0.1 | 0.4 | - | 0.1 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.1 |
| Pedestrians | - | - | - | - | 295 | - | - | - | - | - | 36 | - | - | - | - | - | 148 | - | - | - | - | - | 172 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018
Count Name: 47th Street with Western Avenue Site Code:
e: 06/01/2021
(847)518-9990

Page No: 3

Turning Movement Peak Hour Data (4:30 PM)

| Start Time | 47th Street Eastbound |  |  |  |  |  | 47th Street Westbound |  |  |  |  |  | Western Avenue Northbound |  |  |  |  |  | Western Avenue Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \end{aligned}$ | U-Turn | Left | Thru | Right | Peds | App. |  |
| 4:30 PM | 0 | 5 | 74 | 14 | 17 | 93 | 0 | 24 | 109 | 16 | 4 | 149 | 0 | 31 | 154 | 9 | 4 | 194 | 0 | 30 | 203 | 27 | 8 | 260 | 696 |
| 4:45 PM | 0 | 8 | 84 | 8 | 30 | 100 | 0 | 22 | 103 | 11 | 3 | 136 | 0 | 21 | 153 | 11 | 6 | 185 | 0 | 22 | 224 | 26 | 5 | 272 | 693 |
| 5:00 PM | 0 | 9 | 78 | 6 | 24 | 93 | 0 | 19 | 93 | 15 | 3 | 127 | 0 | 18 | 142 | 11 | 7 | 171 | 0 | 25 | 239 | 21 | 9 | 285 | 676 |
| 5:15 PM | 0 | 9 | 82 | 14 | 16 | 105 | 0 | 24 | 103 | 21 | 0 | 148 | 0 | 28 | 142 | 16 | 10 | 186 | 0 | 20 | 240 | 27 | 14 | 287 | 726 |
| Total | 0 | 31 | 318 | 42 | 87 | 391 | 0 | 89 | 408 | 63 | 10 | 560 | 0 | 98 | 591 | 47 | 27 | 736 | 0 | 97 | 906 | 101 | 36 | 1104 | 2791 |
| Approach \% | 0.0 | 7.9 | 81.3 | 10.7 | - | - | 0.0 | 15.9 | 72.9 | 11.3 | - | - | 0.0 | 13.3 | 80.3 | 6.4 | - | - | 0.0 | 8.8 | 82.1 | 9.1 | - | - | - |
| Total \% | 0.0 | 1.1 | 11.4 | 1.5 | - | 14.0 | 0.0 | 3.2 | 14.6 | 2.3 | - | 20.1 | 0.0 | 3.5 | 21.2 | 1.7 | - | 26.4 | 0.0 | 3.5 | 32.5 | 3.6 | - | 39.6 | - |
| PHF | 0.000 | 0.861 | 0.946 | 0.750 | - | 0.931 | 0.000 | 0.927 | 0.936 | 0.750 | - | 0.940 | 0.000 | 0.790 | 0.959 | 0.734 | - | 0.948 | 0.000 | 0.808 | 0.944 | 0.935 | - | 0.962 | 0.961 |
| Lights | 0 | 30 | 303 | 31 | - | 364 | 0 | 84 | 377 | 61 | - | 522 | 0 | 76 | 526 | 41 | - | 643 | 0 | 95 | 870 | 100 | - | 1065 | 2594 |
| \% Lights | - | 96.8 | 95.3 | 73.8 | - | 93.1 | - | 94.4 | 92.4 | 96.8 | - | 93.2 | - | 77.6 | 89.0 | 87.2 | - | 87.4 | - | 97.9 | 96.0 | 99.0 | - | 96.5 | 92.9 |
| Buses | 0 | 0 | 4 | 4 | - | 8 | 0 | 3 | 4 | 0 | - | 7 | 0 | 5 | 18 | 3 | - | 26 | 0 | 0 | 13 | 0 | - | 13 | 54 |
| \% Buses | - | 0.0 | 1.3 | 9.5 | - | 2.0 | - | 3.4 | 1.0 | 0.0 | - | 1.3 | - | 5.1 | 3.0 | 6.4 | - | 3.5 | - | 0.0 | 1.4 | 0.0 | - | 1.2 | 1.9 |
| Single-Unit Trucks | 0 | 1 | 6 | 3 | - | 10 | 0 | 0 | 21 | 0 | - | 21 | 0 | 5 | 16 | 1 | - | 22 | 0 | 2 | 8 | 0 | - | 10 | 63 |
| $\begin{gathered} \text { \% Single-Unit } \\ \text { Trucks } \end{gathered}$ | - | 3.2 | 1.9 | 7.1 | - | 2.6 | - | 0.0 | 5.1 | 0.0 | - | 3.8 | - | 5.1 | 2.7 | 2.1 | - | 3.0 | - | 2.1 | 0.9 | 0.0 | - | 0.9 | 2.3 |
| Articulated Trucks | 0 | 0 | 4 | 4 | - | 8 | 0 | 2 | 5 | 2 | - | 9 | 0 | 12 | 31 | 2 | - | 45 | 0 | 0 | 15 | 1 | - | 16 | 78 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 0.0 | 1.3 | 9.5 | - | 2.0 | - | 2.2 | 1.2 | 3.2 | - | 1.6 | - | 12.2 | 5.2 | 4.3 | - | 6.1 | - | 0.0 | 1.7 | 1.0 | - | 1.4 | 2.8 |
| Bicycles on Road | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 2 |
| \% Bicycles on Road | - | 0.0 | 0.3 | 0.0 | - | 0.3 | . | 0.0 | 0.2 | 0.0 | - | 0.2 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.1 |
| Pedestrians | - | - | - | - | 87 | - | - | - | - | - | 10 | - | - | - | - | - | 27 | - | - | - | - | - | 36 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018 (847)518-9990

Count Name: 47th Street with Western Avenue Site Code:
Pla De: 06/01/2021
Page No: 4

Turning Movement Peak Hour Data (7:30 AM)

| Start Time | 47th Street Eastbound |  |  |  |  |  | 47th Street Westbound |  |  |  |  |  | Western Avenue Northbound |  |  |  |  |  | Western Avenue Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \end{aligned}$ | U-Turn | Left | Thru | Right | Peds | App. |  |
| 7:30 AM | 0 | 13 | 66 | 11 | 5 | 90 | 0 | 12 | 50 | 14 | 2 | 76 | 0 | 14 | 220 | 12 | 2 | 246 | 0 | 11 | 102 | 14 | 8 | 127 | 539 |
| 7:45 AM | 0 | 5 | 54 | 19 | 0 | 78 | 0 | 13 | 51 | 14 | 0 | 78 | 0 | 17 | 214 | 7 | 2 | 238 | 0 | 12 | 103 | 11 | 5 | 126 | 520 |
| 8:00 AM | 0 | 9 | 68 | 10 | 3 | 87 | 0 | 8 | 66 | 20 | 1 | 94 | 0 | 16 | 182 | 13 | 3 | 211 | 0 | 19 | 86 | 13 | 2 | 118 | 510 |
| 8:15 AM | 0 | 11 | 53 | 8 | 6 | 72 | 0 | 18 | 65 | 24 | 1 | 107 | 0 | 10 | 221 | 16 | 6 | 247 | 0 | 6 | 87 | 18 | 3 | 111 | 537 |
| Total | 0 | 38 | 241 | 48 | 14 | 327 | 0 | 51 | 232 | 72 | 4 | 355 | 0 | 57 | 837 | 48 | 13 | 942 | 0 | 48 | 378 | 56 | 18 | 482 | 2106 |
| Approach \% | 0.0 | 11.6 | 73.7 | 14.7 | - | - | 0.0 | 14.4 | 65.4 | 20.3 | - | - | 0.0 | 6.1 | 88.9 | 5.1 | - | - | 0.0 | 10.0 | 78.4 | 11.6 | - | - | - |
| Total \% | 0.0 | 1.8 | 11.4 | 2.3 | - | 15.5 | 0.0 | 2.4 | 11.0 | 3.4 | - | 16.9 | 0.0 | 2.7 | 39.7 | 2.3 | - | 44.7 | 0.0 | 2.3 | 17.9 | 2.7 | $\checkmark$ | 22.9 | - |
| PHF | 0.000 | 0.731 | 0.886 | 0.632 | - | 0.908 | 0.000 | 0.708 | 0.879 | 0.750 | - | 0.829 | 0.000 | 0.838 | 0.947 | 0.750 | - | 0.953 | 0.000 | 0.632 | 0.917 | 0.778 | - | 0.949 | 0.977 |
| Lights | 0 | 31 | 207 | 21 | - | 259 | 0 | 39 | 205 | 61 | - | 305 | 0 | 44 | 769 | 36 | - | 849 | 0 | 45 | 318 | 47 | - | 410 | 1823 |
| \% Lights | - | 81.6 | 85.9 | 43.8 | - | 79.2 | - | 76.5 | 88.4 | 84.7 | - | 85.9 | - | 77.2 | 91.9 | 75.0 | - | 90.1 | - | 93.8 | 84.1 | 83.9 | - | 85.1 | 86.6 |
| Buses | 0 | 0 | 6 | 7 | - | 13 | 0 | 4 | 6 | 3 | - | 13 | 0 | 4 | 12 | 3 | - | 19 | 0 | 1 | 15 | 1 | - | 17 | 62 |
| \% Buses | - | 0.0 | 2.5 | 14.6 | - | 4.0 | - | 7.8 | 2.6 | 4.2 | - | 3.7 | - | 7.0 | 1.4 | 6.3 | - | 2.0 | - | 2.1 | 4.0 | 1.8 | - | 3.5 | 2.9 |
| Single-Unit Trucks | 0 | 7 | 19 | 10 | - | 36 | 0 | 3 | 12 | 3 | - | 18 | 0 | 0 | 31 | 8 | - | 39 | 0 | 1 | 21 | 7 | - | 29 | 122 |
| $\begin{gathered} \text { \% Single-Unit } \\ \text { Trucks } \end{gathered}$ | - | 18.4 | 7.9 | 20.8 | - | 11.0 | - | 5.9 | 5.2 | 4.2 | - | 5.1 | - | 0.0 | 3.7 | 16.7 | - | 4.1 | - | 2.1 | 5.6 | 12.5 | - | 6.0 | 5.8 |
| Articulated Trucks | 0 | 0 | 9 | 10 | - | 19 | 0 | 5 | 7 | 5 | - | 17 | 0 | 9 | 24 | 1 | - | 34 | 0 | 1 | 24 | 1 | - | 26 | 96 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 0.0 | 3.7 | 20.8 | - | 5.8 | - | 9.8 | 3.0 | 6.9 | - | 4.8 | - | 15.8 | 2.9 | 2.1 | - | 3.6 | - | 2.1 | 6.3 | 1.8 | - | 5.4 | 4.6 |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 2 | 0 | - | 2 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 3 |
| \% Bicycles on Road | - | 0.0 | 0.0 | 0.0 | - | 0.0 | . | 0.0 | 0.9 | 0.0 | - | 0.6 | . | 0.0 | 0.1 | 0.0 | - | 0.1 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.1 |
| Pedestrians | - | - | - | - | 14 | - | - | - | - | - | 4 | - | - | - | - | - | 13 | - | - | - | - | - | 18 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |

Count Name: 47th Street with Western Boulevard
Rosemont, Illinois, United States 60018
Start Date: 06/01/2021
Part No: 1

Turning Movement Data

| Start Time | 47th Street Eastbound |  |  |  |  |  | 47th Street <br> Westbound |  |  |  |  |  | Western Boulevard Northbound |  |  |  |  |  | Western Boulevard Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \end{aligned}$ |  |
| 3:00 PM | 0 | 16 | 73 | 4 | 0 | 93 | 0 | 13 | 87 | 18 | 2 | 118 | 0 | 17 | 156 | 14 | 8 | 187 | 0 | 54 | 269 | 13 | 3 | 336 | 734 |
| 3:15 PM | 0 | 19 | 83 | 4 | 0 | 106 | 0 | 14 | 88 | 24 | 1 | 126 | 0 | 13 | 138 | 15 | 8 | 166 | 0 | 50 | 272 | 9 | 13 | 331 | 729 |
| 3:30 PM | 0 | 17 | 86 | 4 | 1 | 107 | 0 | 15 | 115 | 14 | 5 | 144 | 0 | 6 | 168 | 14 | 11 | 188 | 0 | 68 | 286 | 14 | 5 | 368 | 807 |
| 3:45 PM | 0 | 6 | 94 | 3 | 0 | 103 | 0 | 12 | 109 | 21 | 8 | 142 | 0 | 10 | 171 | 28 | 6 | 209 | 0 | 57 | 303 | 13 | 3 | 373 | 827 |
| Hourly Total | 0 | 58 | 336 | 15 | 1 | 409 | 0 | 54 | 399 | 77 | 16 | 530 | 0 | 46 | 633 | 71 | 33 | 750 | 0 | 229 | 1130 | 49 | 24 | 1408 | 3097 |
| 4:00 PM | 0 | 10 | 80 | 6 | 0 | 96 | 0 | 7 | 105 | 28 | 2 | 140 | 0 | 10 | 161 | 17 | 5 | 188 | 0 | 47 | 270 | 10 | 5 | 327 | 751 |
| 4:15 PM | 0 | 18 | 101 | 4 | 1 | 123 | 0 | 7 | 96 | 22 | 1 | 125 | 0 | 11 | 122 | 18 | 7 | 151 | 0 | 56 | 290 | 12 | 8 | 358 | 757 |
| 4:30 PM | 0 | 17 | 91 | 4 | 0 | 112 | 0 | 10 | 121 | 10 | 2 | 141 | 0 | 15 | 160 | 12 | 4 | 187 | 0 | 64 | 282 | 11 | 5 | 357 | 797 |
| 4:45 PM | 0 | 26 | 92 | 0 | 1 | 118 | 0 | 8 | 111 | 16 | 5 | 135 | 0 | 13 | 134 | 20 | 4 | 167 | 0 | 62 | 270 | 17 | 2 | 349 | 769 |
| Hourly Total | 0 | 71 | 364 | 14 | 2 | 449 | 0 | 32 | 433 | 76 | 10 | 541 | 0 | 49 | 577 | 67 | 20 | 693 | 0 | 229 | 1112 | 50 | 20 | 1391 | 3074 |
| 5:00 PM | 0 | 14 | 106 | 1 | 1 | 121 | 0 | 13 | 91 | 19 | 5 | 123 | 0 | 12 | 147 | 14 | 2 | 173 | 0 | 66 | 281 | 19 | 12 | 366 | 783 |
| 5:15 PM | 0 | 13 | 92 | 6 | 0 | 111 | 0 | 10 | 109 | 20 | 2 | 139 | 0 | 13 | 146 | 20 | 1 | 179 | 0 | 46 | 287 | 17 | 11 | 350 | 779 |
| 5:30 PM | 0 | 7 | 87 | 6 | 1 | 100 | 0 | 11 | 109 | 16 | 2 | 136 | 0 | 15 | 129 | 20 | 4 | 164 | 0 | 55 | 273 | 7 | 10 | 335 | 735 |
| 5:45 PM | 0 | 16 | 77 | 5 | 0 | 98 | 0 | 12 | 86 | 24 | 0 | 122 | 0 | 8 | 139 | 22 | 6 | 169 | 0 | 64 | 263 | 16 | 10 | 343 | 732 |
| Hourly Total | 0 | 50 | 362 | 18 | 2 | 430 | 0 | 46 | 395 | 79 | 9 | 520 | 0 | 48 | 561 | 76 | 13 | 685 | 0 | 231 | 1104 | 59 | 43 | 1394 | 3029 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 6:00 AM | 0 | 11 | 42 | 3 | 0 | 56 | 0 | 0 | 63 | 25 | 7 | 88 | 0 | 1 | 139 | 6 | 5 | 146 | 0 | 24 | 45 | 4 | 2 | 73 | 363 |
| 6:15 AM | 0 | 10 | 59 | 0 | 2 | 69 | 0 | 4 | 69 | 28 | 3 | 101 | 0 | 7 | 184 | 6 | 8 | 197 | 0 | 15 | 44 | 1 | 5 | 60 | 427 |
| 6:30 AM |  | 12 | 58 | 3 | 1 | 73 | 0 | 1 | 59 | 31 | 1 | 91 | 0 | 1 | 243 | 26 | 8 | 270 | 0 | 17 | 55 | 0 | 4 | 72 | 506 |
| 6:45 AM | 0 | 25 | 44 | 3 | 0 | 72 | 0 | 4 | 63 | 19 | 4 | 86 | 0 | 4 | 230 | 6 | 5 | 240 | 0 | 13 | 48 | 2 | 6 | 63 | 461 |
| Hourly Total | 0 | 58 | 203 | 9 | 3 | 270 | 0 | 9 | 254 | 103 | 15 | 366 | 0 | 13 | 796 | 44 | 26 | 853 | 0 | 69 | 192 | 7 | 17 | 268 | 1757 |
| 7:00 AM | 0 | 20 | 44 | 3 | 0 | 67 | 0 | 2 | 64 | 31 | 1 | 97 | 0 | 4 | 187 | 13 | 6 | 204 | 0 | 25 | 47 | 2 | 3 | 74 | 442 |
| 7:15 AM | 0 | 15 | 62 | 6 | 0 | 83 | 0 | 1 | 58 | 28 | 0 | 87 | 0 | 3 | 215 | 7 | 3 | 225 | 0 | 27 | 86 |  | 5 | 116 | 511 |
| 7:30 AM | 0 | 20 | 68 | 3 | 1 | 91 | 0 | 7 | 69 | 32 | 4 | 108 | 0 | 5 | 216 | 15 | 1 | 236 | 0 | 26 | 79 | 5 | 6 | 110 | 545 |
| 7:45 AM | 0 | 9 | 58 | 0 | 0 | 67 | 0 | 4 | 74 | 26 | 3 | 104 | 0 | 5 | 220 | 12 | 2 | 237 | 0 | 26 | 69 | 9 | 5 | 104 | 512 |
| Hourly Total | 0 | 64 | 232 | 12 | 1 | 308 | 0 | 14 | 265 | 117 | 8 | 396 | 0 | 17 | 838 | 47 | 12 | 902 | 0 | 104 | 281 | 19 | 19 | 404 | 2010 |
| 8:00 AM | 0 | 15 | 79 | 2 | 0 | 96 | 0 | 3 | 72 | 21 | 3 | 96 | 0 | 7 | 197 | 17 | 4 | 221 | 0 | 27 | 88 | 6 | 7 | 121 | 534 |
| 8:15 AM | 0 | 13 | 63 | 1 | 1 | 77 | 0 | 2 | 85 | 21 | 5 | 108 | 0 | 6 | 178 | 15 | 4 | 199 | 0 | 29 | 79 | 3 | 7 | 111 | 495 |
| 8:30 AM | 0 | 9 | 75 | 5 | 0 | 89 | 0 | 7 | 69 | 17 | 0 | 93 | 0 | 8 | 175 | 16 | 2 | 199 | 0 | 21 | 71 | 6 | 7 | 98 | 479 |
| 8:45 AM | 0 | 17 | 73 | 2 | 0 | 92 | 0 | 1 | 62 | 25 | 2 | 88 | 0 | 6 | 150 | 17 | 1 | 173 | 0 | 32 | 77 | 3 | 8 | 112 | 465 |
| Hourly Total | 0 | 54 | 290 | 10 | 1 | 354 | 0 | 13 | 288 | 84 | 10 | 385 | 0 | 27 | 700 | 65 | 11 | 792 | 0 | 109 | 315 | 18 | 29 | 442 | 1973 |
| Grand Total | 0 | 355 | 1787 | 78 | 10 | 2220 | 0 | 168 | 2034 | 536 | 68 | 2738 | 0 | 200 | 4105 | 370 | 115 | 4675 | 0 | 971 | 4134 | 202 | 152 | 5307 | 14940 |
| Approach \% | 0.0 | 16.0 | 80.5 | 3.5 | - | - | 0.0 | 6.1 | 74.3 | 19.6 | - | - | 0.0 | 4.3 | 87.8 | 7.9 | - | - | 0.0 | 18.3 | 77.9 | 3.8 | - | - | - |
| Total \% | 0.0 | 2.4 | 12.0 | 0.5 | - | 14.9 | 0.0 | 1.1 | 13.6 | 3.6 | - | 18.3 | 0.0 | 1.3 | 27.5 | 2.5 | - | 31.3 | 0.0 | 6.5 | 27.7 | 1.4 | - | 35.5 | - |
| Lights | 0 | 338 | 1604 | 78 | - | 2020 | 0 | 163 | 1785 | 514 | - | 2462 | 0 | 197 | 4053 | 358 | - | 4608 | 0 | 955 | 4069 | 196 | - | 5220 | 14310 |


| \% Lights | - | 95.2 | 89.8 | 100.0 | - | 91.0 | - | 97.0 | 87.8 | 95.9 | - | 89.9 | - | 98.5 | 98.7 | 96.8 | - | 98.6 | - | 98.4 | 98.4 | 97.0 | - | 98.4 | 95.8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Buses | 0 | 1 | 47 | 0 | - | 48 | 0 | 4 | 52 | 5 | - | 61 | 0 | 0 | 19 | 1 | - | 20 | 0 | 3 | 22 | 0 | - | 25 | 154 |
| \% Buses | - | 0.3 | 2.6 | 0.0 | - | 2.2 | - | 2.4 | 2.6 | 0.9 | - | 2.2 | - | 0.0 | 0.5 | 0.3 | - | 0.4 | - | 0.3 | 0.5 | 0.0 | - | 0.5 | 1.0 |
| Single-Unit Trucks | 0 | 7 | 89 | 0 | - | 96 | 0 | 0 | 105 | 8 | - | 113 | 0 | 3 | 28 | 8 | - | 39 | 0 | 6 | 33 | 2 | - | 41 | 289 |
| $\begin{gathered} \text { \% Single-Unit } \\ \text { Trucks } \end{gathered}$ | - | 2.0 | 5.0 | 0.0 | - | 4.3 | - | 0.0 | 5.2 | 1.5 | - | 4.1 | - | 1.5 | 0.7 | 2.2 | - | 0.8 | - | 0.6 | 0.8 | 1.0 | - | 0.8 | 1.9 |
| Articulated Trucks | 0 | 9 | 43 | 0 | - | 52 | 0 | 1 | 90 | 7 | - | 98 | 0 | 0 | 4 | 3 | - | 7 | 0 | 7 | 9 | 4 | - | 20 | 177 |
| \% Articulated Trucks | - | 2.5 | 2.4 | 0.0 | - | 2.3 | - | 0.6 | 4.4 | 1.3 | - | 3.6 | - | 0.0 | 0.1 | 0.8 | - | 0.1 | - | 0.7 | 0.2 | 2.0 | - | 0.4 | 1.2 |
| Bicycles on Road | 0 | 0 | 4 | 0 | - | 4 | 0 | 0 | 2 | 2 | - | 4 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 1 | 0 | - | 1 | 10 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \end{gathered}$ | - | 0.0 | 0.2 | 0.0 | - | 0.2 | - | 0.0 | 0.1 | 0.4 | - | 0.1 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.1 |
| Pedestrians | - | - | - | - | 10 | - | - | - | - | - | 68 | - | - | - | - | - | 115 | - | - | - | - | - | 152 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | 9575 W. Higgins Rd., Suite 400

Count Name: 47th Street with Western Boulevard
Rosemont, Illinois, United States 60018
Site Code:
Start Date: 06/01/2021
Page No: 3

Turning Movement Peak Hour Data (4:30 PM)

| Start Time | 47th Street Eastbound |  |  |  |  |  | 47th Street <br> Westbound |  |  |  |  |  | Western Boulevard Northbound |  |  |  |  |  | Western Boulevard Southbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | Int. Total |
| 4:30 PM | 0 | 17 | 91 | 4 | 0 | 112 | 0 | 10 | 121 | 10 | 2 | 141 | 0 | 15 | 160 | 12 | 4 | 187 | 0 | 64 | 282 | 11 | 5 | 357 | 797 |
| 4:45 PM | 0 | 26 | 92 | 0 | 1 | 118 | 0 | 8 | 111 | 16 | 5 | 135 | 0 | 13 | 134 | 20 | 4 | 167 | 0 | 62 | 270 | 17 | 2 | 349 | 769 |
| 5:00 PM | 0 | 14 | 106 | 1 | 1 | 121 | 0 | 13 | 91 | 19 | 5 | 123 | 0 | 12 | 147 | 14 | 2 | 173 | 0 | 66 | 281 | 19 | 12 | 366 | 783 |
| 5:15 PM | 0 | 13 | 92 | 6 | 0 | 111 | 0 | 10 | 109 | 20 | 2 | 139 | 0 | 13 | 146 | 20 | 1 | 179 | 0 | 46 | 287 | 17 | 11 | 350 | 779 |
| Total | 0 | 70 | 381 | 11 | 2 | 462 | 0 | 41 | 432 | 65 | 14 | 538 | 0 | 53 | 587 | 66 | 11 | 706 | 0 | 238 | 1120 | 64 | 30 | 1422 | 3128 |
| Approach \% | 0.0 | 15.2 | 82.5 | 2.4 | - | - | 0.0 | 7.6 | 80.3 | 12.1 | - | - | 0.0 | 7.5 | 83.1 | 9.3 | - | - | 0.0 | 16.7 | 78.8 | 4.5 | - | - | - |
| Total \% | 0.0 | 2.2 | 12.2 | 0.4 | - | 14.8 | 0.0 | 1.3 | 13.8 | 2.1 | - | 17.2 | 0.0 | 1.7 | 18.8 | 2.1 | - | 22.6 | 0.0 | 7.6 | 35.8 | 2.0 | - | 45.5 | - |
| PHF | 0.000 | 0.673 | 0.899 | 0.458 | - | 0.955 | 0.000 | 0.788 | 0.893 | 0.813 | - | 0.954 | 0.000 | 0.883 | 0.917 | 0.825 | - | 0.944 | 0.000 | 0.902 | 0.976 | 0.842 | - | 0.971 | 0.981 |
| Lights | 0 | 66 | 362 | 11 | - | 439 | 0 | 40 | 395 | 65 | - | 500 | 0 | 53 | 576 | 65 | - | 694 | 0 | 237 | 1109 | 63 | - | 1409 | 3042 |
| \% Lights | - | 94.3 | 95.0 | 100.0 | - | 95.0 | - | 97.6 | 91.4 | 100.0 | - | 92.9 | - | 100.0 | 98.1 | 98.5 | - | 98.3 | - | 99.6 | 99.0 | 98.4 | - | 99.1 | 97.3 |
| Buses | 0 | 0 | 6 | 0 | - | 6 | 0 | 1 | 7 | 0 | - | 8 | 0 | 0 | 4 | 0 | - | 4 | 0 | 0 | 3 | 0 | - | 3 | 21 |
| \% Buses | - | 0.0 | 1.6 | 0.0 | - | 1.3 | - | 2.4 | 1.6 | 0.0 | - | 1.5 | - | 0.0 | 0.7 | 0.0 | - | 0.6 | - | 0.0 | 0.3 | 0.0 | - | 0.2 | 0.7 |
| Single-Unit Trucks | 0 | 1 | 8 | 0 | - | 9 | 0 | 0 | 20 | 0 | - | 20 | 0 | 0 | 7 | 1 | - | 8 | 0 | 1 | 5 | 1 | - | 7 | 44 |
| \% Single-Unit Trucks | - | 1.4 | 2.1 | 0.0 | - | 1.9 | - | 0.0 | 4.6 | 0.0 | - | 3.7 | - | 0.0 | 1.2 | 1.5 | - | 1.1 | - | 0.4 | 0.4 | 1.6 | - | 0.5 | 1.4 |
| Articulated Trucks | 0 | 3 | 3 | 0 | - | 6 | 0 | 0 | 10 | 0 | $\checkmark$ | 10 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 3 | 0 | - | 3 | 19 |
| \% Articulated Trucks | - | 4.3 | 0.8 | 0.0 | - | 1.3 | - | 0.0 | 2.3 | 0.0 | - | 1.9 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.3 | 0.0 | - | 0.2 | 0.6 |
| Bicycles on Road | 0 | 0 | 2 | 0 | $\cdots$ | 2 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 2 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \\ \hline \end{gathered}$ | - | 0.0 | 0.5 | 0.0 | - | 0.4 | - | 0.0 | 0.0 | 0.0 | . | 0.0 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.1 |
| Pedestrians | - | - | - | - | 2 | - | - | - | - | - | 14 | - | - | - | - | - | 11 | - | - | - | - | - | 30 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | $\cdot$ | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | 9575 W. Higgins Rd., Suite 400

Count Name: 47th Street with Western Boulevard
Rosemont, Illinois, United States 60018 (847)518-9990

Start Date: 06/01/2021
Page No: 4

Turning Movement Peak Hour Data (7:30 AM)

| Start Time | 47th Street Eastbound |  |  |  |  |  | 47th Street Westbound |  |  |  |  |  | Western Boulevard Northbound |  |  |  |  |  | Western Boulevard Southbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | Int. Total |
| 7:30 AM | 0 | 20 | 68 | 3 | 1 | 91 | 0 | 7 | 69 | 32 | 4 | 108 | 0 | 5 | 216 | 15 | 1 | 236 | 0 | 26 | 79 | 5 | 6 | 110 | 545 |
| 7:45 AM | 0 | 9 | 58 | 0 | 0 | 67 | 0 | 4 | 74 | 26 | 3 | 104 | 0 | 5 | 220 | 12 | 2 | 237 | 0 | 26 | 69 | 9 | 5 | 104 | 512 |
| 8:00 AM | 0 | 15 | 79 | 2 | 0 | 96 | 0 | 3 | 72 | 21 | 3 | 96 | 0 | 7 | 197 | 17 | 4 | 221 | 0 | 27 | 88 | 6 | 7 | 121 | 534 |
| 8:15 AM | 0 | 13 | 63 | 1 | 1 | 77 | 0 | 2 | 85 | 21 | 5 | 108 | 0 | 6 | 178 | 15 | 4 | 199 | 0 | 29 | 79 | 3 | 7 | 111 | 495 |
| Total | 0 | 57 | 268 | 6 | 2 | 331 | 0 | 16 | 300 | 100 | 15 | 416 | 0 | 23 | 811 | 59 | 11 | 893 | 0 | 108 | 315 | 23 | 25 | 446 | 2086 |
| Approach \% | 0.0 | 17.2 | 81.0 | 1.8 | - | - | 0.0 | 3.8 | 72.1 | 24.0 | - | - | 0.0 | 2.6 | 90.8 | 6.6 | - | - | 0.0 | 24.2 | 70.6 | 5.2 | - | - | - |
| Total \% | 0.0 | 2.7 | 12.8 | 0.3 | - | 15.9 | 0.0 | 0.8 | 14.4 | 4.8 | - | 19.9 | 0.0 | 1.1 | 38.9 | 2.8 | - | 42.8 | 0.0 | 5.2 | 15.1 | 1.1 | - | 21.4 | - |
| PHF | 0.000 | 0.713 | 0.848 | 0.500 | - | 0.862 | 0.000 | 0.571 | 0.882 | 0.781 | - | 0.963 | 0.000 | 0.821 | 0.922 | 0.868 | - | 0.942 | 0.000 | 0.931 | 0.895 | 0.639 | - | 0.921 | 0.957 |
| Lights | 0 | 55 | 224 | 6 | - | 285 | 0 | 16 | 253 | 89 | - | 358 | 0 | 22 | 802 | 56 | - | 880 | 0 | 105 | 304 | 22 | - | 431 | 1954 |
| \% Lights | - | 96.5 | 83.6 | 100.0 | - | 86.1 | - | 100.0 | 84.3 | 89.0 | - | 86.1 | - | 95.7 | 98.9 | 94.9 | - | 98.5 | - | 97.2 | 96.5 | 95.7 | - | 96.6 | 93.7 |
| Buses | 0 | 0 | 10 | 0 | - | 10 | 0 | 0 | 11 | 2 | - | 13 | 0 | 0 | 1 | 0 | - | 1 | 0 | 2 | 4 | 0 | - | 6 | 30 |
| \% Buses | - | 0.0 | 3.7 | 0.0 | - | 3.0 | - | 0.0 | 3.7 | 2.0 | - | 3.1 | - | 0.0 | 0.1 | 0.0 | - | 0.1 | - | 1.9 | 1.3 | 0.0 | - | 1.3 | 1.4 |
| Single-Unit Trucks | 0 | 1 | 25 | 0 | - | 26 | 0 | 0 | 20 | 4 | - | 24 | 0 | 1 | 6 | 3 | - | 10 | 0 | 1 | 7 | 0 | - | 8 | 68 |
| \% $\underset{\substack{\text { Single-Unit } \\ \text { Trucks }}}{\text { Stat }}$ | . | 1.8 | 9.3 | 0.0 | - | 7.9 | - | 0.0 | 6.7 | 4.0 | - | 5.8 | . | 4.3 | 0.7 | 5.1 | - | 1.1 | - | 0.9 | 2.2 | 0.0 | - | 1.8 | 3.3 |
| Articulated Trucks | 0 | 1 | 9 | 0 | - | 10 | 0 | 0 | 15 | 3 | - | 18 | 0 | 0 | 2 | 0 | - | 2 | 0 | 0 | 0 | 1 | - | 1 | 31 |
| \% Articulated Trucks | - | 1.8 | 3.4 | 0.0 | - | 3.0 | - | 0.0 | 5.0 | 3.0 | - | 4.3 | - | 0.0 | 0.2 | 0.0 | - | 0.2 | . | 0.0 | 0.0 | 4.3 | - | 0.2 | 1.5 |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | 2 | - | 3 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 3 |
| $\begin{gathered} \% \text { Bicycles on } \\ \text { Road } \end{gathered}$ | . | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.3 | 2.0 | - | 0.7 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.1 |
| Pedestrians | - | - | - | - | 2 | - | - | - | - | - | 15 | - | - | - | - | - | 11 | - | - | - | - | - | 25 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |

## Preliminary Site Plan



## Level of Service Criteria

Level of Service

A Favorable progression. Most vehicles arrive during the green indication and travel through the intersection without stopping.

B Good progression, with more vehicles stopping than for
Level of Service A.
C Individual cycle failures (i.e., one or more queued vehicles are not able to depart as a result of insufficient capacity during the cycle) may begin to appear. Number of vehicles stopping is significant, although many vehicles still pass through the intersection without
stopping.
D The volume-to-capacity ratio is high and either >35-55 progression is ineffective or the cycle length is too long. Many vehicles stop and individual cycle failures are noticeable.

E Progression is unfavorable. The volume-to-capacity ratio >55-80 is high and the cycle length is long. Individual cycle failures are frequent.

F The volume-to-capacity ratio is very high, progression is >80.0 very poor, and the cycle length is long. Most cycles fail to clear the queue.

|  | Unsignalized Intersections |
| ---: | ---: | ---: |
| Level of Service | Average Total Delay (SEC/VEH) |
| A | $0-10$ |
| B | $>10-15$ |
| C | $>15-25$ |
| D | $>25-35$ |
| E | $>35-50$ |
| F | $>50$ |

## Capacity Analysis Summary Sheets 2021 Base Weekday Morning Peak Hour Conditions

|  | 4 |  |  | 7 |  |  | $4$ | 9 | $p$ |  |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\leqslant$ |  |  | 中 ${ }^{\text {W }}$ |  |  | * $\uparrow$ ¢ |  |
| Traffic Volume (vph) | 43 | 91 | 31 | 20 | 0 | 24 | 0 | 1145 | 38 | 28 | 577 | 0 |
| Future Volume (vph) | 43 | 91 | 31 | 20 | 0 | 24 | 0 | 1145 | 38 | 28 | 577 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 10 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  | 0.99 |  |  | 1.00 |  |  |  |  |
| Frt |  | 0.974 |  |  | 0.927 |  |  | 0.995 |  |  |  |  |
| Flt Protected |  | 0.987 |  |  | 0.978 |  |  |  |  |  | 0.998 |  |
| Satd. Flow (prot) | 0 | 1639 | 0 | 0 | 1405 | 0 | 0 | 3323 | 0 | 0 | 2829 | 0 |
| Flt Permitted |  | 0.921 |  |  | 0.892 |  |  |  |  |  | 0.852 |  |
| Satd. Flow (perm) | 0 | 1528 | 0 | 0 | 1281 | 0 | 0 | 3323 | 0 | 0 | 2415 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 10 |  |  | 25 |  |  | 5 |  |  |  |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 966 |  |  | 172 |  |  | 1339 |  |  | 1013 |  |
| Travel Time (s) |  | 22.0 |  |  | 3.9 |  |  | 30.4 |  |  | 23.0 |  |
| Confl. Peds. (\#/hr) | 4 |  | 1 | 1 |  | 4 |  |  | 3 | 3 |  |  |
| Confl. Bikes (\#/hr) |  |  | 1 |  |  |  |  |  | 1 |  |  | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 0\% | 0\% | 17\% | 0\% | 8\% | 8\% | 11\% | 13\% | 0\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  | 0 | 0 |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 174 | 0 | 0 | 46 | 0 | 0 | 1245 | 0 | 0 | 636 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA |  |  | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  |  |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 |  |  | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 20.0 | 20.0 |  | 8.0 | 20.0 |  |  | 20.0 |  | 20.0 | 20.0 |  |
| Minimum Split (s) | 28.0 | 28.0 |  | 12.0 | 40.0 |  |  | 70.0 |  | 70.0 | 70.0 |  |
| Total Split (s) | 28.0 | 28.0 |  | 12.0 | 40.0 |  |  | 70.0 |  | 70.0 | 70.0 |  |
| Total Split (\%) | 25.5\% | 25.5\% |  | 10.9\% | 36.4\% |  |  | 63.6\% |  | 63.6\% | 63.6\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 0.0 | 0.0 |  | 1.0 | 1.0 |  |  | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) |  | 3.0 |  |  | 4.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lead/Lag | Lead | Lead |  | Lag |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  |  | C-Max |  | C-Max | C-Max |  |
| Act Effct Green (s) |  | 25.0 |  |  | 36.0 |  |  | 66.0 |  |  | 66.0 |  |
| Actuated g/C Ratio |  | 0.23 |  |  | 0.33 |  |  | 0.60 |  |  | 0.60 |  |


| $\stackrel{ }{*}$ |  |  |  |  |  |  | $\dagger$ |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.49 |  |  | 0.10 |  |  | 0.62 |  |  | 0.44 |  |
| Control Delay | 40.2 |  |  | 27.0 |  |  | 4.4 |  |  | 13.1 |  |
| Queue Delay | 0.1 |  |  | 2.6 |  |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 40.4 |  |  | 29.7 |  |  | 4.5 |  |  | 13.2 |  |
| LOS | D |  |  | C |  |  | A |  |  | B |  |
| Approach Delay | 40.4 |  |  | 29.7 |  |  | 4.5 |  |  | 13.2 |  |
| Approach LOS | D |  |  | C |  |  | A |  |  | B |  |
| Queue Length 50th (t) | 101 |  |  | 20 |  |  | 50 |  |  | 120 |  |
| Queue Length 95th (t) | 171 |  |  | m43 |  |  | 59 |  |  | 162 |  |
| Internal Link Dist (t) | 886 |  |  | 92 |  |  | 1259 |  |  | 933 |  |
| Turn Bay Length (tt) |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 355 |  |  | 445 |  |  | 1995 |  |  | 1449 |  |
| Starvation Cap Reductn | 0 |  |  | 325 |  |  | 0 |  |  | 0 |  |
| Spillback Cap Reductn | 11 |  |  | 0 |  |  | 49 |  |  | 35 |  |
| Storage Cap Reductn | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 0.51 |  |  | 0.38 |  |  | 0.64 |  |  | 0.45 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other <br> Cycle Length: 110  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 29 (26\%), Referenced to phase 2:NBT and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.62 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 10.6 |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 61.6\% |  |  | ICU Level of Service B |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Western Avenue \& 45th Street


|  | 4 | $\rightarrow$ | V | $\bigcirc$ |  |  | $4$ | $\dagger$ | 7 | ( | $\frac{1}{\dagger}$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | \& |  |  | * $\uparrow$ |  |  | * $\uparrow$ |  |
| Traffic Volume (vph) | 103 | 10 | 44 | 0 | 5 | 4 | 24 | 1218 | 5 | 9 | 541 | 15 |
| Future Volume (vph) | 103 | 10 | 44 | 0 | 5 | 4 | 24 | 1218 | 5 | 9 | 541 | 15 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 16 | 12 | 12 | 10 | 12 | 12 | 10 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Ped Bike Factor |  | 0.99 |  |  | 0.99 |  |  | 1.00 |  |  |  |  |
| Frt |  | 0.962 |  |  | 0.940 |  |  | 0.999 |  |  | 0.996 |  |
| Flt Protected |  | 0.968 |  |  |  |  |  | 0.999 |  |  | 0.999 |  |
| Satd. Flow (prot) | 0 | 1698 | 0 | 0 | 1393 | 0 | 0 | 3298 | 0 | 0 | 3259 | 0 |
| Flt Permitted |  | 0.804 |  |  |  |  |  | 0.934 |  |  | 0.927 |  |
| Satd. Flow (perm) | 0 | 1408 | 0 | 0 | 1393 | 0 | 0 | 3083 | 0 | 0 | 3024 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 18 |  |  | 4 |  |  | 1 |  |  | 5 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 172 |  |  | 1568 |  |  | 1346 |  |  | 1025 |  |
| Travel Time (s) |  | 3.9 |  |  | 35.6 |  |  | 30.6 |  |  | 23.3 |  |
| Confl. Peds. (\#/hr) | 1 |  | 2 | 2 |  | 1 |  |  | 7 | 7 |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 1\% | 40\% | 2\% | 0\% | 80\% | 0\% | 0\% | 2\% | 0\% | 0\% | 3\% | 0\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 172 | 0 | 0 | 9 | 0 | 0 | 1369 | 0 | 0 | 621 | 0 |
| Turn Type | pm+pt | NA |  |  | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 17.0 |  | 17.0 | 17.0 |  | 17.0 | 17.0 |  | 17.0 | 17.0 |  |
| Minimum Split (s) | 9.0 | 37.0 |  | 28.0 | 28.0 |  | 73.0 | 73.0 |  | 73.0 | 73.0 |  |
| Total Split (s) | 9.0 | 37.0 |  | 28.0 | 28.0 |  | 73.0 | 73.0 |  | 73.0 | 73.0 |  |
| Total Split (\%) | 8.2\% | 33.6\% |  | 25.5\% | 25.5\% |  | 66.4\% | 66.4\% |  | 66.4\% | 66.4\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 0.0 | 0.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) |  | 4.0 |  |  | 3.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lead/Lag | Lag |  |  | Lead | Lead |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | C-Max | C-Max |  | C-Max | C-Max |  |
| Act Effct Green (s) |  | 33.0 |  |  | 25.0 |  |  | 69.0 |  |  | 69.0 |  |
| Actuated g/C Ratio |  | 0.30 |  |  | 0.23 |  |  | 0.63 |  |  | 0.63 |  |


| $\stackrel{ }{*}$ | $\rightarrow$ |  | $\dagger$ |  |  | 4 | $\dagger$ | 7 |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.38 |  |  | 0.03 |  |  | 0.71 |  |  | 0.33 |  |
| Control Delay | 20.0 |  |  | 26.6 |  |  | 5.7 |  |  | 10.1 |  |
| Queue Delay | 2.9 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 23.0 |  |  | 26.6 |  |  | 5.7 |  |  | 10.1 |  |
| LOS | C |  |  | C |  |  | A |  |  | B |  |
| Approach Delay | 23.0 |  |  | 26.6 |  |  | 5.7 |  |  | 10.1 |  |
| Approach LOS | C |  |  | C |  |  | A |  |  | B |  |
| Queue Length 50th (ft) | 50 |  |  | 3 |  |  | 68 |  |  | 99 |  |
| Queue Length 95th (tt) | 81 |  |  | 16 |  |  | m82 |  |  | 131 |  |
| Internal Link Dist (tt) | 92 |  |  | 1488 |  |  | 1266 |  |  | 945 |  |
| Turn Bay Length (t) |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 448 |  |  | 319 |  |  | 1934 |  |  | 1898 |  |
| Starvation Cap Reductn | 183 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 0.65 |  |  | 0.03 |  |  | 0.71 |  |  | 0.33 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 27 (25\%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.71 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 8.4 |  |  | Intersection LOS: A |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 73.4\% |  |  | ICU Level of Service D |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |

$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 2: Western Boulevard \& 45th Street/Site Access


|  | 4 |  | $\checkmark$ | $\checkmark$ |  |  | $4$ | $\dagger$ | $p$ | V |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ $\uparrow$ |  | ${ }^{1}$ | $\uparrow$ |  | ${ }^{7}$ | 中\% |  | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume (vph) | 48 | 301 | 60 | 64 | 288 | 90 | 71 | 1045 | 60 | 60 | 498 | 70 |
| Future Volume (vph) | 48 | 301 | 60 | 64 | 288 | 90 | 71 | 1045 | 60 | 60 | 498 | 70 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 10 | 12 | 10 | 12 | 12 | 10 | 11 | 12 | 10 | 11 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 160 | 0 |  | 0 | 100 |  | 0 | 100 |  | 0 |
| Storage Lanes | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 95 |  |  | 95 |  |  |
| Lane Util. Factor | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor |  | 0.99 |  | 0.99 | 0.99 |  | 0.98 | 1.00 |  |  | 0.99 |  |
| Frt |  | 0.978 |  |  | 0.964 |  |  | 0.992 |  |  | 0.981 |  |
| Flt Protected |  | 0.994 |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 2491 | 0 | 1381 | 1635 | 0 | 1327 | 3171 | 0 | 1604 | 3019 | 0 |
| Flt Permitted |  | 0.797 |  | 0.404 |  |  | 0.359 |  |  | 0.113 |  |  |
| Satd. Flow (perm) | 0 | 1995 | 0 | 582 | 1635 | 0 | 494 | 3171 | 0 | 191 | 3019 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 18 |  |  | 18 |  |  | 7 |  |  | 18 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 2698 |  |  | 179 |  |  | 1284 |  |  | 1339 |  |
| Travel Time (s) |  | 61.3 |  |  | 4.1 |  |  | 29.2 |  |  | 30.4 |  |
| Confl. Peds. (\#/hr) | 18 |  | 13 | 13 |  | 18 | 14 |  | 4 | 4 |  | 14 |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 2 |  |  | 1 |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.99 | 0.98 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 19\% | 16\% | 52\% | 22\% | 11\% | 11\% | 27\% | 7\% | 25\% | 5\% | 11\% | 14\% |
| Bus Blockages (\#/hr) | 0 | 11 | 11 | 0 | 0 | 0 | 0 | 5 | 5 | 0 | 5 | 5 |
| Parking (\#/hr) | 0 | 0 | 0 |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 417 | 0 | 65 | 386 | 0 | 72 | 1127 | 0 | 61 | 574 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 21.0 | 21.0 |  | 10.0 | 21.0 |  | 5.0 | 17.0 |  | 5.0 | 17.0 |  |
| Minimum Split (s) | 37.0 | 37.0 |  | 14.0 | 51.0 |  | 8.0 | 51.0 |  | 8.0 | 51.0 |  |
| Total Split (s) | 37.0 | 37.0 |  | 14.0 | 51.0 |  | 8.0 | 51.0 |  | 8.0 | 51.0 |  |
| Total Split (\%) | 33.6\% | 33.6\% |  | 12.7\% | 46.4\% |  | 7.3\% | 46.4\% |  | 7.3\% | 46.4\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 0.0 | 0.0 |  | 1.0 | 1.0 |  | 0.0 | 1.0 |  | 0.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 3.0 |  | 4.0 | 4.0 |  | 3.0 | 4.0 |  | 3.0 | 4.0 |  |
| Lead/Lag | Lead | Lead |  | Lag |  |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | None | C-Max |  | None | C-Max |  |
| Act Effct Green (s) |  | 34.0 |  | 47.0 | 47.0 |  | 53.6 | 48.6 |  | 53.6 | 48.6 |  |
| Actuated g/C Ratio |  | 0.31 |  | 0.43 | 0.43 |  | 0.49 | 0.44 |  | 0.49 | 0.44 |  |



Splits and Phases: 3: Western Avenue \& 47th Street


|  | 4 |  |  | 7 |  |  | $4$ |  | $p$ | ( |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | $\hat{*}$ |  |  | * $\uparrow$ |  | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  | * | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume (vph) | 71 | 342 | 8 | 20 | 384 | 123 | 29 | 1053 | 74 | 135 | 421 | 29 |
| Future Volume (vph) | 71 | 342 | 8 | 20 | 384 | 123 | 29 | 1053 | 74 | 135 | 421 | 29 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 11 | 12 | 12 | 10 | 12 | 9 | 9 | 12 | 9 | 9 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 320 | 50 |  | 0 | 70 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 20 |  |  | 25 |  |  | 145 |  |  | 160 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | 0.99 | 1.00 |  |  | 0.99 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.997 |  |  | 0.965 |  |  | 0.990 |  |  | 0.990 |  |
| Flt Protected | 0.950 |  |  |  | 0.998 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1620 | 1500 | 0 | 0 | 2666 | 0 | 1577 | 3163 | 0 | 1608 | 3120 | 0 |
| Flt Permitted | 0.313 |  |  |  | 0.933 |  | 0.456 |  |  | 0.087 |  |  |
| Satd. Flow (perm) | 526 | 1500 | 0 | 0 | 2491 | 0 | 756 | 3163 | 0 | 147 | 3120 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 1 |  |  | 38 |  |  | 8 |  |  | 7 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 179 |  |  | 500 |  |  | 1309 |  |  | 1346 |  |
| Travel Time (s) |  | 4.1 |  |  | 11.4 |  |  | 29.8 |  |  | 30.6 |  |
| Confl. Peds. (\#/hr) | 25 |  | 11 | 11 |  | 25 | 2 |  | 15 | 15 |  | 2 |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 3 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 4\% | 18\% | 0\% | 0\% | 14\% | 7\% | 3\% | 1\% | 5\% | 1\% | 3\% | 3\% |
| Bus Blockages (\#/hr) | 0 | 9 | 9 | 0 | 10 | 10 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  | 0 | 0 | 0 |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 74 | 364 | 0 | 0 | 549 | 0 | 30 | 1174 | 0 | 141 | 469 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 17.0 |  | 17.0 | 17.0 |  | 5.0 | 19.0 |  | 5.0 | 19.0 |  |
| Minimum Split (s) | 14.0 | 52.0 |  | 38.0 | 38.0 |  | 8.0 | 47.0 |  | 8.0 | 47.0 |  |
| Total Split (s) | 14.0 | 52.0 |  | 38.0 | 38.0 |  | 11.0 | 47.0 |  | 11.0 | 47.0 |  |
| Total Split (\%) | 12.7\% | 47.3\% |  | 34.5\% | 34.5\% |  | 10.0\% | 42.7\% |  | 10.0\% | 42.7\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 0.0 | 0.0 |  | 0.0 | 1.0 |  | 0.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 4.0 | 4.0 |  |  | 3.0 |  | 3.0 | 4.0 |  | 3.0 | 4.0 |  |
| Lead/Lag | Lag |  |  | Lead | Lead |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | None | C-Max |  | None | C-Max |  |
| Act Effct Green (s) | 48.0 | 48.0 |  |  | 35.0 |  | 50.6 | 43.0 |  | 53.7 | 47.9 |  |
| Actuated g/C Ratio | 0.44 | 0.44 |  |  | 0.32 |  | 0.46 | 0.39 |  | 0.49 | 0.44 |  |


|  | $\rangle$ |  |  |  |  |  | $\checkmark$ | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.23 | 0.56 |  |  | 0.67 |  | 0.08 | 0.95 |  | 0.80 | 0.34 |  |
| Control Delay | 14.9 | 19.2 |  |  | 34.9 |  | 14.6 | 48.3 |  | 67.0 | 42.9 |  |
| Queue Delay | 4.0 | 5.6 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 18.8 | 24.8 |  |  | 34.9 |  | 14.6 | 48.3 |  | 67.0 | 42.9 |  |
| LOS | B | C |  |  | C |  | B | D |  | E | D |  |
| Approach Delay |  | 23.8 |  |  | 34.9 |  |  | 47.5 |  |  | 48.5 |  |
| Approach LOS |  | C |  |  | C |  |  | D |  |  | D |  |
| Queue Length 50th ( t ) | 17 | 93 |  |  | 164 |  | 10 | 413 |  | 88 | 173 |  |
| Queue Length 95th (t) | m26 | m226 |  |  | 227 |  | 26 | \#562 |  | \#163 | 230 |  |
| Internal Link Dist (t) |  | 99 |  |  | 420 |  |  | 1229 |  |  | 1266 |  |
| Turn Bay Length (tt) |  |  |  |  |  |  | 50 |  |  | 70 |  |  |
| Base Capacity (vph) | 328 | 655 |  |  | 818 |  | 417 | 1241 |  | 177 | 1362 |  |
| Starvation Cap Reductn | 190 | 228 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.54 | 0.85 |  |  | 0.67 |  | 0.07 | 0.95 |  | 0.80 | 0.34 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 13 (12\%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.95 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 41.5 |  |  |  | Intersection LOS: D |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 86.7\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 4: Western Boulevard \& 47th Street


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |
| Traffic Vol, veh/h | 0 | 540 | 11 | 14 | 522 | 0 | 5 | 0 | 11 | 3 | 0 | 0 |  |
| Future Vol, veh/h | 0 | 540 | 11 | 14 | 522 | 0 | 5 | 0 | 11 | 3 | 0 | 0 |  |
| Conflicting Peds, \#/hr | 13 | 0 | 16 | 16 | 0 | 13 | 0 | 0 | 3 | 3 | 0 | 0 |  |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - |  | None |  |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade,\% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 0 | 12 | 36 | 0 | 2 | 0 | 20 | 0 | 36 | 100 | 0 | 0 |  |
| Mvmt Flow | 0 | 587 | 12 | 15 | 567 | 0 | 5 | 0 | 12 | 3 | 0 | 0 |  |





## Capacity Analysis Summary Sheets <br> 2021 Base Weekday Evening Peak Hour Conditions

|  | 4 | $\rightarrow$ |  | 7 |  |  | $4$ | $\dagger$ |  |  |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | $\$$ |  |  | 中 ${ }^{\text {a }}$ |  |  | $\uparrow \uparrow$ |  |
| Traffic Volume (vph) | 19 | 76 | 38 | 59 | 0 | 32 | 0 | 664 | 21 | 26 | 1064 | 0 |
| Future Volume (vph) | 19 | 76 | 38 | 59 | 0 | 32 | 0 | 664 | 21 | 26 | 1064 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 10 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  | 0.99 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.961 |  |  | 0.952 |  |  | 0.995 |  |  |  |  |
| Flt Protected |  | 0.993 |  |  | 0.969 |  |  |  |  |  | 0.999 |  |
| Satd. Flow (prot) | 0 | 1616 | 0 | 0 | 1545 | 0 | 0 | 3331 | 0 | 0 | 3101 | 0 |
| Flt Permitted |  | 0.961 |  |  | 0.807 |  |  |  |  |  | 0.924 |  |
| Satd. Flow (perm) | 0 | 1563 | 0 | 0 | 1286 | 0 | 0 | 3331 | 0 | 0 | 2868 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 17 |  |  | 27 |  |  | 5 |  |  |  |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 966 |  |  | 172 |  |  | 1339 |  |  | 1013 |  |
| Travel Time (s) |  | 22.0 |  |  | 3.9 |  |  | 30.4 |  |  | 23.0 |  |
| Confl. Peds. (\#/hr) | 6 |  | 1 | 1 |  | 6 |  |  | 1 | 1 |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 0\% | 1\% | 0\% | 2\% | 0\% | 0\% | 0\% | 8\% | 0\% | 8\% | 3\% | 0\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  | 0 | 0 |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 136 | 0 | 0 | 93 | 0 | 0 | 699 | 0 | 0 | 1113 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA |  |  | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  |  |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 |  |  | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 20.0 | 20.0 |  | 8.0 | 20.0 |  |  | 20.0 |  | 20.0 | 20.0 |  |
| Minimum Split (s) | 28.0 | 28.0 |  | 12.0 | 40.0 |  |  | 70.0 |  | 70.0 | 70.0 |  |
| Total Split (s) | 28.0 | 28.0 |  | 12.0 | 40.0 |  |  | 70.0 |  | 70.0 | 70.0 |  |
| Total Split (\%) | 25.5\% | 25.5\% |  | 10.9\% | 36.4\% |  |  | 63.6\% |  | 63.6\% | 63.6\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 0.0 | 0.0 |  | 1.0 | 1.0 |  |  | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) |  | 3.0 |  |  | 4.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lead/Lag | Lead | Lead |  | Lag |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  |  | C-Max |  | C-Max | C-Max |  |
| Act Effct Green (s) |  | 25.0 |  |  | 36.0 |  |  | 66.0 |  |  | 66.0 |  |
| Actuated g/C Ratio |  | 0.23 |  |  | 0.33 |  |  | 0.60 |  |  | 0.60 |  |


|  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

Splits and Phases: 1: Western Avenue \& 45th Street


|  | 4 |  | 7 | 4 |  |  |  | $\dagger$ | 7 | $\downarrow$ |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | 4 |  |  | *T |  |  | $\uparrow \uparrow$ |  |
| Traffic Volume (vph) | 66 | 2 | 55 | 5 | 8 | 15 | 42 | 752 | 11 | 0 | 1408 | 41 |
| Future Volume (vph) | 66 | 2 | 55 | 5 | 8 | 15 | 42 | 752 | 11 | 0 | 1408 | 41 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 16 | 12 | 12 | 10 | 12 | 12 | 10 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Ped Bike Factor |  | 0.99 |  |  | 0.99 |  |  | 1.00 |  |  |  |  |
| Frt |  | 0.940 |  |  | 0.926 |  |  | 0.998 |  |  | 0.996 |  |
| Flt Protected |  | 0.974 |  |  | 0.991 |  |  | 0.997 |  |  |  |  |
| Satd. Flow (prot) | 0 | 1688 | 0 | 0 | 1962 | 0 | 0 | 3312 | 0 | 0 | 3322 | 0 |
| Flt Permitted |  | 0.844 |  |  | 0.968 |  |  | 0.744 |  |  |  |  |
| Satd. Flow (perm) | 0 | 1463 | 0 | 0 | 1916 | 0 | 0 | 2471 | 0 | 0 | 3322 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 38 |  |  | 16 |  |  | 2 |  |  | 5 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 172 |  |  | 1568 |  |  | 1346 |  |  | 1025 |  |
| Travel Time (s) |  | 3.9 |  |  | 35.6 |  |  | 30.6 |  |  | 23.3 |  |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  | 7 | 7 |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 3\% | 50\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 18\% | 0\% | 1\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 128 | 0 | 0 | 29 | 0 | 0 | 838 | 0 | 0 | 1510 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA |  | Perm | NA |  |  | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 17.0 |  | 17.0 | 17.0 |  | 17.0 | 17.0 |  | 17.0 | 17.0 |  |
| Minimum Split (s) | 9.0 | 37.0 |  | 28.0 | 28.0 |  | 73.0 | 73.0 |  | 73.0 | 73.0 |  |
| Total Split (s) | 9.0 | 37.0 |  | 28.0 | 28.0 |  | 73.0 | 73.0 |  | 73.0 | 73.0 |  |
| Total Split (\%) | 8.2\% | 33.6\% |  | 25.5\% | 25.5\% |  | 66.4\% | 66.4\% |  | 66.4\% | 66.4\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 0.0 | 0.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) |  | 4.0 |  |  | 3.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lead/Lag | Lag |  |  | Lead | Lead |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | C-Max | C-Max |  | C-Max | C-Max |  |
| Act Effct Green (s) |  | 33.0 |  |  | 25.0 |  |  | 69.0 |  |  | 69.0 |  |
| Actuated g/C Ratio |  | 0.30 |  |  | 0.23 |  |  | 0.63 |  |  | 0.63 |  |


$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 2: Western Boulevard \& 45th Street/Site Access


|  | 4 | $\rightarrow$ | $\checkmark$ | $\checkmark$ |  | 4 | $4$ | 4 | \％ | $\checkmark$ |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ＊${ }^{\text {W }}$ |  | ${ }^{7}$ | 个 |  | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{4}$ | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume（vph） | 31 | 317 | 42 | 89 | 407 | 63 | 98 | 591 | 47 | 97 | 963 | 101 |
| Future Volume（vph） | 31 | 317 | 42 | 89 | 407 | 63 | 98 | 591 | 47 | 97 | 963 | 101 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（ft） | 12 | 10 | 12 | 10 | 12 | 12 | 10 | 11 | 12 | 10 | 11 | 12 |
| Grade（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Storage Length（ft） | 0 |  | 160 | 0 |  | 0 | 100 |  | 0 | 100 |  | 0 |
| Storage Lanes | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 95 |  |  | 95 |  |  |
| Lane Util．Factor | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor |  | 0.99 |  | 0.98 | 0.99 |  |  | 1.00 |  | 0.99 | 0.97 |  |
| Frt |  | 0.984 |  |  | 0.980 |  |  | 0.989 |  |  | 0.986 |  |
| Flt Protected |  | 0.996 |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 0 | 2781 | 0 | 1574 | 1693 | 0 | 1381 | 3144 | 0 | 1652 | 3249 | 0 |
| Flt Permitted |  | 0.753 |  | 0.398 |  |  | 0.119 |  |  | 0.308 |  |  |
| Satd．Flow（perm） | 0 | 2100 | 0 | 647 | 1693 | 0 | 173 | 3144 | 0 | 533 | 3249 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 12 |  |  | 9 |  |  | 9 |  |  | 13 |  |
| Link Speed（mph） |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance（ft） |  | 2698 |  |  | 179 |  |  | 1284 |  |  | 1339 |  |
| Travel Time（s） |  | 61.3 |  |  | 4.1 |  |  | 29.2 |  |  | 30.4 |  |
| Confl．Peds．（\＃／hr） | 36 |  | 27 | 27 |  | 36 | 87 |  | 10 | 10 |  | 87 |
| Confl．Bikes（\＃／hr） |  |  | 1 |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ |
| Heavy Vehicles（\％） | 3\％ | 7\％ | 33\％ | 7\％ | 10\％ | 3\％ | 22\％ | 8\％ | 15\％ | 2\％ | 2\％ | 1\％ |
| Bus Blockages（\＃／hr） | 0 | 12 | 12 | 0 | 0 | 0 | 0 | 5 | 5 | 0 | 5 | 5 |
| Parking（\＃／hr） | 0 | 0 | 0 |  |  |  |  |  |  |  |  |  |
| Mid－Block Traffic（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 0 | 406 | 0 | 93 | 490 | 0 | 102 | 665 | 0 | 101 | 1108 | 0 |
| Turn Type | Perm | NA |  | pm＋pt | NA |  | pm＋pt | NA |  | pm＋pt | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 21.0 | 21.0 |  | 11.0 | 21.0 |  | 6.0 | 17.0 |  | 6.0 | 17.0 |  |
| Minimum Split（s） | 34.0 | 34.0 |  | 15.0 | 49.0 |  | 9.0 | 52.0 |  | 9.0 | 52.0 |  |
| Total Split（s） | 34.0 | 34.0 |  | 15.0 | 49.0 |  | 9.0 | 52.0 |  | 9.0 | 52.0 |  |
| Total Split（\％） | 30．9\％ | 30．9\％ |  | 13．6\％ | 44．5\％ |  | 8．2\％ | 47．3\％ |  | 8．2\％ | 47．3\％ |  |
| Yellow Time（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All－Red Time（s） | 0.0 | 0.0 |  | 1.0 | 1.0 |  | 0.0 | 1.0 |  | 0.0 | 1.0 |  |
| Lost Time Adjust（s） |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） |  | 3.0 |  | 4.0 | 4.0 |  | 3.0 | 4.0 |  | 3.0 | 4.0 |  |
| Lead／Lag | Lead | Lead |  | Lag |  |  | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Optimize？ |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | None | C－Max |  | None | C－Max |  |
| Act Effct Green（s） |  | 31.0 |  | 45.0 | 45.0 |  | 55.0 | 48.0 |  | 55.0 | 48.0 |  |
| Actuated g／C Ratio |  | 0.28 |  | 0.41 | 0.41 |  | 0.50 | 0.44 |  | 0.50 | 0.44 |  |


| $\rangle$ |  |  | 7 |  |  | 4 | 4 |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.68 |  | 0.26 | 0.70 |  | 0.67 | 0.48 |  | 0.31 | 0.78 |  |
| Control Delay | 40.6 |  | 10.8 | 18.2 |  | 37.3 | 23.3 |  | 21.9 | 43.3 |  |
| Queue Delay | 0.0 |  | 4.6 | 8.1 |  | 0.0 | 1.8 |  | 1.0 | 0.0 |  |
| Total Delay | 40.6 |  | 15.4 | 26.2 |  | 37.3 | 25.1 |  | 22.9 | 43.3 |  |
| LOS | D |  | B | C |  | D | C |  | C | D |  |
| Approach Delay | 40.6 |  |  | 24.5 |  |  | 26.7 |  |  | 41.6 |  |
| Approach LOS | D |  |  | C |  |  | C |  |  | D |  |
| Queue Length 50th ( t ) | 130 |  | 16 | 335 |  | 35 | 170 |  | 54 | 440 |  |
| Queue Length 95th (t) | 187 |  | m23 | m461 |  | \#84 | 223 |  | m88 | 508 |  |
| Internal Link Dist (t) | 2618 |  |  | 99 |  |  | 1204 |  |  | 1259 |  |
| Turn Bay Length (t) |  |  |  |  |  | 100 |  |  | 100 |  |  |
| Base Capacity (vph) | 600 |  | 357 | 697 |  | 152 | 1377 |  | 327 | 1425 |  |
| Starvation Cap Reductn | 0 |  | 202 | 168 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 2 |  | 0 | 0 |  | 0 | 523 |  | 91 | 0 |  |
| Storage Cap Reductn | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.68 |  | 0.60 | 0.93 |  | 0.67 | 0.78 |  | 0.43 | 0.78 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 33 (30\%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.78 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 34.3 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 94.0\% |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 3: Western Avenue \& 47th Street


|  | 4 | $\rightarrow$ |  | $\bigcirc$ |  |  | 4 | $\dagger$ | 7 | , |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{\beta}$ |  |  | * $\uparrow$ |  | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 中t |  |
| Traffic Volume (vph) | 70 | 380 | 11 | 41 | 442 | 65 | 53 | 670 | 66 | 238 | 1166 | 64 |
| Future Volume (vph) | 70 | 380 | 11 | 41 | 442 | 65 | 53 | 670 | 66 | 238 | 1166 | 64 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 11 | 12 | 12 | 10 | 12 | 9 | 9 | 12 | 9 | 9 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 320 | 50 |  | 0 | 70 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 20 |  |  | 25 |  |  | 145 |  |  | 160 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | 0.98 | 1.00 |  |  | 0.99 |  |  | 0.99 |  |  | 1.00 |  |
| Frt |  | 0.996 |  |  | 0.982 |  |  | 0.987 |  |  | 0.992 |  |
| Flt Protected | 0.950 |  |  |  | 0.996 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1589 | 1650 | 0 | 0 | 2797 | 0 | 1624 | 3155 | 0 | 1624 | 3187 | 0 |
| Flt Permitted | 0.312 |  |  |  | 0.843 |  | 0.106 |  |  | 0.194 |  |  |
| Satd. Flow (perm) | 513 | 1650 | 0 | 0 | 2366 | 0 | 181 | 3155 | 0 | 332 | 3187 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 2 |  |  | 14 |  |  | 10 |  |  | 6 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 179 |  |  | 500 |  |  | 1309 |  |  | 1346 |  |
| Travel Time (s) |  | 4.1 |  |  | 11.4 |  |  | 29.8 |  |  | 30.6 |  |
| Confl. Peds. (\#/hr) | 30 |  | 11 | 11 |  | 30 | 2 |  | 14 | 14 |  | 2 |
| Confl. Bikes (\#/hr) |  |  | 2 |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 6\% | 7\% | 0\% | 0\% | 11\% | 0\% | 0\% | 1\% | 2\% | 0\% | 1\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 9 | 9 | 0 | 10 | 10 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  | 0 | 0 | 0 |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 71 | 399 | 0 | 0 | 559 | 0 | 54 | 751 | 0 | 243 | 1255 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 17.0 |  | 17.0 | 17.0 |  | 5.0 | 19.0 |  | 7.0 | 19.0 |  |
| Minimum Split (s) | 12.0 | 51.0 |  | 39.0 | 39.0 |  | 8.0 | 40.0 |  | 10.0 | 51.0 |  |
| Total Split (s) | 12.0 | 51.0 |  | 39.0 | 39.0 |  | 8.0 | 40.0 |  | 19.0 | 51.0 |  |
| Total Split (\%) | 10.9\% | 46.4\% |  | 35.5\% | 35.5\% |  | 7.3\% | 36.4\% |  | 17.3\% | 46.4\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 0.0 | 0.0 |  | 0.0 | 1.0 |  | 0.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 4.0 | 4.0 |  |  | 3.0 |  | 3.0 | 4.0 |  | 3.0 | 4.0 |  |
| Lead/Lag | Lag |  |  | Lead | Lead |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | None | C-Max |  | None | C-Max |  |
| Act Effct Green (s) | 47.0 | 47.0 |  |  | 36.0 |  | 43.9 | 37.9 |  | 56.0 | 48.6 |  |
| Actuated g/C Ratio | 0.43 | 0.43 |  |  | 0.33 |  | 0.40 | 0.34 |  | 0.51 | 0.44 |  |


|  | 4 |  |  | 7 |  |  | - | $\uparrow$ |  | , | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.24 | 0.57 |  |  | 0.71 |  | 0.39 | 0.69 |  | 0.73 | 0.89 |  |
| Control Delay | 14.9 | 16.7 |  |  | 37.7 |  | 23.8 | 34.8 |  | 27.1 | 40.6 |  |
| Queue Delay | 2.8 | 3.1 |  |  | 1.2 |  | 0.5 | 0.0 |  | 0.0 | 9.7 |  |
| Total Delay | 17.7 | 19.8 |  |  | 38.8 |  | 24.3 | 34.8 |  | 27.1 | 50.4 |  |
| LOS | B | B |  |  | D |  | C | C |  | C | D |  |
| Approach Delay |  | 19.5 |  |  | 38.8 |  |  | 34.1 |  |  | 46.6 |  |
| Approach LOS |  | B |  |  | D |  |  | C |  |  | D |  |
| Queue Length 50th (t) | 17 | 97 |  |  | 177 |  | 19 | 238 |  | 135 | 502 |  |
| Queue Length 95th (t) | m27 | 129 |  |  | 243 |  | 40 | 313 |  | m195 | \#598 |  |
| Internal Link Dist (t) |  | 99 |  |  | 420 |  |  | 1229 |  |  | 1266 |  |
| Turn Bay Length (t) |  |  |  |  |  |  | 50 |  |  | 70 |  |  |
| Base Capacity (vph) | 297 | 706 |  |  | 783 |  | 137 | 1094 |  | 356 | 1411 |  |
| Starvation Cap Reductn | 150 | 206 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 79 |  | 9 | 0 |  | 0 | 149 |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.48 | 0.80 |  |  | 0.79 |  | 0.42 | 0.69 |  | 0.68 | 0.99 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: $40(36 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.89 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 38.5 |  |  |  |  | Intersection LOS: D |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 88.3\% |  |  |  |  | ICU Level of Service E |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 4: Western Boulevard \& 47th Street






## Capacity Analysis Summary Sheets

 2027 Projected Weekday Morning Peak Hour Conditions|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| $\rangle$ |  |  |  |  |  |  | $\dagger$ | \% |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.51 |  |  | 0.13 |  |  | 0.64 |  |  | 0.50 |  |
| Control Delay | 40.8 |  |  | 22.0 |  |  | 4.5 |  |  | 14.2 |  |
| Queue Delay | 0.7 |  |  | 2.5 |  |  | 0.1 |  |  | 0.1 |  |
| Total Delay | 41.5 |  |  | 24.4 |  |  | 4.6 |  |  | 14.3 |  |
| LOS | D |  |  | C |  |  | A |  |  | B |  |
| Approach Delay | 41.5 |  |  | 24.4 |  |  | 4.6 |  |  | 14.3 |  |
| Approach LOS | D |  |  | C |  |  | A |  |  | B |  |
| Queue Length 50th (t) | 105 |  |  | 18 |  |  | 52 |  |  | 133 |  |
| Queue Length 95th (t) | 177 |  |  | m40 |  |  | 62 |  |  | 181 |  |
| Internal Link Dist (t) | 886 |  |  | 92 |  |  | 1259 |  |  | 933 |  |
| Turn Bay Length (t) |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 353 |  |  | 415 |  |  | 2014 |  |  | 1335 |  |
| Starvation Cap Reductn | 0 |  |  | 279 |  |  | 0 |  |  | 0 |  |
| Spillback Cap Reductn | 41 |  |  | 0 |  |  | 124 |  |  | 82 |  |
| Storage Cap Reductn | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 0.57 |  |  | 0.40 |  |  | 0.68 |  |  | 0.53 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 29 (26\%), Referenced to phase 2:NBT and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.64 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 11.1 |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 71.6\% |  |  | ICU Level of Service C |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Western Avenue \& 45th Street


|  | 4 | $\rightarrow$ |  |  |  |  | 4 | 4 |  |  |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | ¢ |  |  | * ${ }^{\text {F }}$ |  |  | * $\uparrow$ |  |
| Traffic Volume (vph) | 117 | 17 | 45 | 0 | 12 | 5 | 25 | 1258 | 12 | 14 | 559 | 15 |
| Future Volume (vph) | 117 | 17 | 45 | 0 | 12 | 5 | 25 | 1258 | 12 | 14 | 559 | 15 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 16 | 12 | 12 | 10 | 12 | 12 | 10 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Ped Bike Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Frt |  | 0.966 |  |  | 0.962 |  |  | 0.999 |  |  | 0.996 |  |
| Flt Protected |  | 0.968 |  |  |  |  |  | 0.999 |  |  | 0.999 |  |
| Satd. Flow (prot) | 0 | 1697 | 0 | 0 | 1339 | 0 | 0 | 3295 | 0 | 0 | 3259 | 0 |
| Flt Permitted |  | 0.794 |  |  |  |  |  | 0.933 |  |  | 0.905 |  |
| Satd. Flow (perm) | 0 | 1391 | 0 | 0 | 1339 | 0 | 0 | 3077 | 0 | 0 | 2953 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 15 |  |  | 5 |  |  | 2 |  |  | 4 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 172 |  |  | 1568 |  |  | 1346 |  |  | 309 |  |
| Travel Time (s) |  | 3.9 |  |  | 35.6 |  |  | 30.6 |  |  | 7.0 |  |
| Confl. Peds. (\#/hr) | 1 |  | 2 | 2 |  | 1 |  |  | 7 | 7 |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 4\% | 12\% | 2\% | 0\% | 75\% | 0\% | 0\% | 2\% | 8\% | 0\% | 3\% | 0\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 197 | 0 | 0 | 18 | 0 | 0 | 1422 | 0 | 0 | 645 | 0 |
| Turn Type | pm+pt | NA |  |  | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 17.0 |  | 17.0 | 17.0 |  | 17.0 | 17.0 |  | 17.0 | 17.0 |  |
| Minimum Split (s) | 9.0 | 37.0 |  | 28.0 | 28.0 |  | 73.0 | 73.0 |  | 73.0 | 73.0 |  |
| Total Split (s) | 9.0 | 37.0 |  | 28.0 | 28.0 |  | 73.0 | 73.0 |  | 73.0 | 73.0 |  |
| Total Split (\%) | 8.2\% | 33.6\% |  | 25.5\% | 25.5\% |  | 66.4\% | 66.4\% |  | 66.4\% | 66.4\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 0.0 | 0.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) |  | 4.0 |  |  | 3.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lead/Lag | Lag |  |  | Lead | Lead |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | C-Max | C-Max |  | C-Max | C-Max |  |
| Act Effct Green (s) |  | 33.0 |  |  | 25.0 |  |  | 69.0 |  |  | 69.0 |  |
| Actuated g/C Ratio |  | 0.30 |  |  | 0.23 |  |  | 0.63 |  |  | 0.63 |  |


| 4 | $\rightarrow$ |  | 7 |  |  | , | 4 | \% |  | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.45 |  |  | 0.06 |  |  | 0.74 |  |  | 0.35 |  |
| Control Delay | 24.6 |  |  | 27.5 |  |  | 6.2 |  |  | 10.3 |  |
| Queue Delay | 4.7 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 29.3 |  |  | 27.5 |  |  | 6.2 |  |  | 10.3 |  |
| LOS | C |  |  | C |  |  | A |  |  | B |  |
| Approach Delay | 29.3 |  |  | 27.5 |  |  | 6.2 |  |  | 10.3 |  |
| Approach LOS | C |  |  | C |  |  | A |  |  | B |  |
| Queue Length 50th (ft) | 68 |  |  | 7 |  |  | 74 |  |  | 104 |  |
| Queue Length 95th (ft) | 105 |  |  | 27 |  |  | m85 |  |  | 138 |  |
| Internal Link Dist (ft) | 92 |  |  | 1488 |  |  | 1266 |  |  | 229 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 441 |  |  | 308 |  |  | 1930 |  |  | 1853 |  |
| Starvation Cap Reductn | 177 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 0.75 |  |  | 0.06 |  |  | 0.74 |  |  | 0.35 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 27 (25\%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.74 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 9.5 |  |  |  | Intersection LOS: A |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 76.5\% <br> ICU Level of Service D <br> Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| m Volume for 95th percentile queue is |  | by up |  |  |  |  |  |  |  |  |  |

Splits and Phases: 2: Western Boulevard \& 45th Street/Site Access


|  | 4 | $\rightarrow$ | $\cdots$ | 7 |  | 4 | 4 | $\dagger$ | $p$ | ( | $\frac{1}{\dagger}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * $\uparrow$ |  | ${ }^{*}$ | $\hat{\beta}$ |  | ${ }^{*}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{*}$ | 中t |  |
| Traffic Volume (vph) | 50 | 317 | 62 | 67 | 301 | 95 | 73 | 1081 | 68 | 64 | 515 | 72 |
| Future Volume (vph) | 50 | 317 | 62 | 67 | 301 | 95 | 73 | 1081 | 68 | 64 | 515 | 72 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 10 | 12 | 10 | 12 | 12 | 10 | 11 | 12 | 10 | 11 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 160 | 0 |  | 0 | 100 |  | 0 | 100 |  | 0 |
| Storage Lanes | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 95 |  |  | 95 |  |  |
| Lane Util. Factor | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor |  | 0.99 |  | 0.99 | 0.99 |  | 0.99 | 1.00 |  |  | 0.99 |  |
| Frt |  | 0.978 |  |  | 0.964 |  |  | 0.991 |  |  | 0.982 |  |
| Flt Protected |  | 0.994 |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 2541 | 0 | 1452 | 1643 | 0 | 1465 | 3178 | 0 | 1589 | 3022 | 0 |
| Flt Permitted |  | 0.777 |  | 0.389 |  |  | 0.348 |  |  | 0.099 |  |  |
| Satd. Flow (perm) | 0 | 1984 | 0 | 590 | 1643 | 0 | 529 | 3178 | 0 | 166 | 3022 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 18 |  |  | 18 |  |  | 7 |  |  | 17 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 2698 |  |  | 179 |  |  | 1284 |  |  | 1339 |  |
| Travel Time (s) |  | 61.3 |  |  | 4.1 |  |  | 29.2 |  |  | 30.4 |  |
| Confl. Peds. (\#/hr) | 18 |  | 13 | 13 |  | 18 | 14 |  | 4 | 4 |  | 14 |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 2 |  |  | 1 |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.99 | 0.98 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 18\% | 15\% | 42\% | 16\% | 10\% | 12\% | 15\% | 7\% | 18\% | 6\% | 11\% | 14\% |
| Bus Blockages (\#/hr) | 0 | 11 | 11 | 0 | 0 | 0 | 0 | 5 | 5 | 0 | 5 | 5 |
| Parking (\#/hr) | 0 | 0 | 0 |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 437 | 0 | 68 | 404 | 0 | 74 | 1172 | 0 | 65 | 593 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 21.0 | 21.0 |  | 10.0 | 21.0 |  | 5.0 | 17.0 |  | 5.0 | 17.0 |  |
| Minimum Split (s) | 37.0 | 37.0 |  | 14.0 | 51.0 |  | 8.0 | 51.0 |  | 8.0 | 51.0 |  |
| Total Split (s) | 37.0 | 37.0 |  | 14.0 | 51.0 |  | 8.0 | 51.0 |  | 8.0 | 51.0 |  |
| Total Split (\%) | 33.6\% | 33.6\% |  | 12.7\% | 46.4\% |  | 7.3\% | 46.4\% |  | 7.3\% | 46.4\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 0.0 | 0.0 |  | 1.0 | 1.0 |  | 0.0 | 1.0 |  | 0.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 3.0 |  | 4.0 | 4.0 |  | 3.0 | 4.0 |  | 3.0 | 4.0 |  |
| Lead/Lag | Lead | Lead |  | Lag |  |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | None | C-Max |  | None | C-Max |  |
| Act Effct Green (s) |  | 34.0 |  | 47.0 | 47.0 |  | 53.6 | 48.6 |  | 53.6 | 48.6 |  |
| Actuated g/C Ratio |  | 0.31 |  | 0.43 | 0.43 |  | 0.49 | 0.44 |  | 0.49 | 0.44 |  |


|  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Splits and Phases: 3: Western Avenue \& 47th Street


|  | 4 |  |  | 7 |  |  | $4$ |  | $p$ | ( |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  |  | * $\uparrow$ |  | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume (vph) | 74 | 367 | 8 | 22 | 403 | 131 | 30 | 1090 | 81 | 140 | 434 | 30 |
| Future Volume (vph) | 74 | 367 | 8 | 22 | 403 | 131 | 30 | 1090 | 81 | 140 | 434 | 30 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 11 | 12 | 12 | 10 | 12 | 9 | 9 | 12 | 9 | 9 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 320 | 50 |  | 0 | 70 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 20 |  |  | 25 |  |  | 145 |  |  | 160 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | 0.99 | 1.00 |  |  | 0.99 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.997 |  |  | 0.965 |  |  | 0.990 |  |  | 0.990 |  |
| Flt Protected | 0.950 |  |  |  | 0.998 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1620 | 1525 | 0 | 0 | 2701 | 0 | 1577 | 3162 | 0 | 1608 | 3120 | 0 |
| Flt Permitted | 0.294 |  |  |  | 0.930 |  | 0.445 |  |  | 0.087 |  |  |
| Satd. Flow (perm) | 495 | 1525 | 0 | 0 | 2517 | 0 | 738 | 3162 | 0 | 147 | 3120 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 1 |  |  | 39 |  |  | 8 |  |  | 7 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 179 |  |  | 500 |  |  | 1309 |  |  | 1346 |  |
| Travel Time (s) |  | 4.1 |  |  | 11.4 |  |  | 29.8 |  |  | 30.6 |  |
| Confl. Peds. (\#/hr) | 25 |  | 11 | 11 |  | 25 | 2 |  | 15 | 15 |  | 2 |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 3 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 4\% | 16\% | 0\% | 0\% | 12\% | 7\% | 3\% | 1\% | 5\% | 1\% | 3\% | 3\% |
| Bus Blockages (\#/hr) | 0 | 9 | 9 | 0 | 10 | 10 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  | 0 | 0 | 0 |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 77 | 390 | 0 | 0 | 579 | 0 | 31 | 1219 | 0 | 146 | 483 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 17.0 |  | 17.0 | 17.0 |  | 5.0 | 19.0 |  | 5.0 | 19.0 |  |
| Minimum Split (s) | 14.0 | 52.0 |  | 38.0 | 38.0 |  | 8.0 | 47.0 |  | 8.0 | 47.0 |  |
| Total Split (s) | 14.0 | 52.0 |  | 38.0 | 38.0 |  | 11.0 | 47.0 |  | 11.0 | 47.0 |  |
| Total Split (\%) | 12.7\% | 47.3\% |  | 34.5\% | 34.5\% |  | 10.0\% | 42.7\% |  | 10.0\% | 42.7\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 0.0 | 0.0 |  | 0.0 | 1.0 |  | 0.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 4.0 | 4.0 |  |  | 3.0 |  | 3.0 | 4.0 |  | 3.0 | 4.0 |  |
| Lead/Lag | Lag |  |  | Lead | Lead |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | None | C-Max |  | None | C-Max |  |
| Act Effct Green (s) | 48.0 | 48.0 |  |  | 35.0 |  | 50.6 | 43.0 |  | 53.6 | 47.8 |  |
| Actuated g/C Ratio | 0.44 | 0.44 |  |  | 0.32 |  | 0.46 | 0.39 |  | 0.49 | 0.43 |  |


|  | $\rangle$ |  |  | 7 |  |  | 4 | $\uparrow$ | 7 | , | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.24 | 0.59 |  |  | 0.70 |  | 0.08 | 0.98 |  | 0.82 | 0.36 |  |
| Control Delay | 15.3 | 19.7 |  |  | 35.9 |  | 14.7 | 55.3 |  | 70.5 | 43.0 |  |
| Queue Delay | 4.8 | 9.2 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 20.1 | 28.9 |  |  | 35.9 |  | 14.7 | 55.3 |  | 70.5 | 43.0 |  |
| LOS | C | C |  |  | D |  | B | E |  | E | D |  |
| Approach Delay |  | 27.4 |  |  | 35.9 |  |  | 54.3 |  |  | 49.4 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | D |  |
| Queue Length 50th (ft) | 18 | 132 |  |  | 175 |  | 11 | 439 |  | 92 | 179 |  |
| Queue Length 95th (ft) | m26 | m254 |  |  | 242 |  | 27 | \#598 |  | \#172 | 235 |  |
| Internal Link Dist (ft) |  | 99 |  |  | 420 |  |  | 1229 |  |  | 1266 |  |
| Turn Bay Length (tt) |  |  |  |  |  |  | 50 |  |  | 70 |  |  |
| Base Capacity (vph) | 318 | 666 |  |  | 827 |  | 409 | 1240 |  | 177 | 1360 |  |
| Starvation Cap Reductn | 184 | 238 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.57 | 0.91 |  |  | 0.70 |  | 0.08 | 0.98 |  | 0.82 | 0.36 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: $13(12 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.98 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 45.3 |  |  |  | Intersection LOS: D |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 90.2\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 4: Western Boulevard \& 47th Street




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 0 |  |  |  |  |  |  |
| Movement V | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * |  | 中 ${ }^{\text {a }}$ |  |  | ¢4 |
| Traffic Vol, veh/h | 0 | 0 | 1378 | 2 | 2 | 588 |
| Future Vol, veh/h | 0 | 0 | 1378 | 2 | 2 | 588 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 0 | 2 | 0 | 0 | 2 |
| Mvmt Flow | 0 | 0 | 1451 | 2 | 2 | 619 |


| Major/Minor M | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1766 | 727 | 0 | 0 | 1453 | 0 |
| Stage 1 | 1452 | - | - | - | - | - |
| Stage 2 | 314 | - | - | - | - | - |
| Critical Hdwy | 6.8 | 6.9 | - | - | 4.1 | - |
| Critical Hdwy Stg 1 | 5.8 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.8 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | - | - | 2.2 | - |
| Pot Cap-1 Maneuver | 77 | 371 | - | - | 472 | - |
| Stage 1 | 185 | - | - | - | - | - |
| Stage 2 | 720 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 77 | 371 | - | - | 472 | - |
| Mov Cap-2 Maneuver | 77 | - | - | - | - | - |
| Stage 1 | 185 | - | - | - | - | - |
| Stage 2 | 716 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 0 |  | 0 |  | 0 |  |
| HCM LOS | A |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  |  | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | - | 472 | - |
| HCM Lane V/C Ratio |  | - | - | - | 0.004 | - |
| HCM Control Delay (s) |  | - | - | 0 | 12.7 | 0 |
| HCM Lane LOS |  | - | - | A | B | A |
| HCM 95th \%tile Q(veh) |  | - | - | - | 0 | - |

## Capacity Analysis Summary Sheets 2027 Projected Weekday Evening Peak Hour Conditions

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |



Splits and Phases: 1: Western Avenue \& 45th Street


|  | 4 | $\rightarrow$ |  | $\downarrow$ |  | 4 | 4 | 4 | $p$ | , | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | * |  |  | * $\uparrow$ |  |  | * $\uparrow$ |  |
| Traffic Volume (vph) | 70 | 8 | 57 | 11 | 26 | 20 | 43 | 775 | 13 | 1 | 1453 | 42 |
| Future Volume (vph) | 70 | 8 | 57 | 11 | 26 | 20 | 43 | 775 | 13 | 1 | 1453 | 42 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 16 | 12 | 12 | 10 | 12 | 12 | 10 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Ped Bike Factor |  | 0.99 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.943 |  |  | 0.952 |  |  | 0.998 |  |  | 0.996 |  |
| Flt Protected |  | 0.975 |  |  | 0.991 |  |  | 0.997 |  |  |  |  |
| Satd. Flow (prot) | 0 | 1643 | 0 | 0 | 1892 | 0 | 0 | 3311 | 0 | 0 | 3322 | 0 |
| Flt Permitted |  | 0.832 |  |  | 0.953 |  |  | 0.729 |  |  | 0.955 |  |
| Satd. Flow (perm) | 0 | 1402 | 0 | 0 | 1819 | 0 | 0 | 2421 | 0 | 0 | 3172 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 34 |  |  | 21 |  |  | 3 |  |  | 5 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 172 |  |  | 1568 |  |  | 1346 |  |  | 309 |  |
| Travel Time (s) |  | 3.9 |  |  | 35.6 |  |  | 30.6 |  |  | 7.0 |  |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  | 7 | 7 |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 4\% | 63\% | 0\% | 0\% | 15\% | 0\% | 0\% | 1\% | 15\% | 0\% | 1\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 140 | 0 | 0 | 59 | 0 | 0 | 866 | 0 | 0 | 1559 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 17.0 |  | 17.0 | 17.0 |  | 17.0 | 17.0 |  | 17.0 | 17.0 |  |
| Minimum Split (s) | 9.0 | 37.0 |  | 28.0 | 28.0 |  | 73.0 | 73.0 |  | 73.0 | 73.0 |  |
| Total Split (s) | 9.0 | 37.0 |  | 28.0 | 28.0 |  | 73.0 | 73.0 |  | 73.0 | 73.0 |  |
| Total Split (\%) | 8.2\% | 33.6\% |  | 25.5\% | 25.5\% |  | 66.4\% | 66.4\% |  | 66.4\% | 66.4\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 0.0 | 0.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) |  | 4.0 |  |  | 3.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lead/Lag | Lag |  |  | Lead | Lead |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | C-Max | C-Max |  | C-Max | C-Max |  |
| Act Effct Green (s) |  | 33.0 |  |  | 25.0 |  |  | 69.0 |  |  | 69.0 |  |
| Actuated g/C Ratio |  | 0.30 |  |  | 0.23 |  |  | 0.63 |  |  | 0.63 |  |


|  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |

$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 2: Western Boulevard \& 45th Street/Site Access


|  | 4 | $\rightarrow$ | $\cdots$ | 7 |  |  | 4 | $\dagger$ | $p$ | , |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * $\uparrow$ |  | ${ }^{*}$ | $\hat{\beta}$ |  | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{*}$ | 中t |  |
| Traffic Volume (vph) | 32 | 331 | 43 | 97 | 426 | 68 | 101 | 611 | 50 | 101 | 998 | 105 |
| Future Volume (vph) | 32 | 331 | 43 | 97 | 426 | 68 | 101 | 611 | 50 | 101 | 998 | 105 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 10 | 12 | 10 | 12 | 12 | 10 | 11 | 12 | 10 | 11 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 160 | 0 |  | 0 | 100 |  | 0 | 100 |  | 0 |
| Storage Lanes | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 95 |  |  | 95 |  |  |
| Lane Util. Factor | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor |  | 0.99 |  | 0.98 | 0.99 |  |  | 1.00 |  | 1.00 | 0.97 |  |
| Frt |  | 0.984 |  |  | 0.979 |  |  | 0.989 |  |  | 0.986 |  |
| Flt Protected |  | 0.996 |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 2851 | 0 | 1636 | 1702 | 0 | 1428 | 3159 | 0 | 1636 | 3220 | 0 |
| Flt Permitted |  | 0.725 |  | 0.384 |  |  | 0.106 |  |  | 0.296 |  |  |
| Satd. Flow (perm) | 0 | 2073 | 0 | 649 | 1702 | 0 | 159 | 3159 | 0 | 507 | 3220 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 12 |  |  | 9 |  |  | 10 |  |  | 13 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 2698 |  |  | 179 |  |  | 1284 |  |  | 1339 |  |
| Travel Time (s) |  | 61.3 |  |  | 4.1 |  |  | 29.2 |  |  | 30.4 |  |
| Confl. Peds. (\#/hr) | 36 |  | 27 | 27 |  | 36 | 87 |  | 10 | 10 |  | 87 |
| Confl. Bikes (\#/hr) |  |  | 1 |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 3\% | 6\% | 16\% | 3\% | 9\% | 4\% | 18\% | 8\% | 8\% | 3\% | 3\% | 1\% |
| Bus Blockages (\#/hr) | 0 | 12 | 12 | 0 | 0 | 0 | 0 | 5 | 5 | 0 | 5 | 5 |
| Parking (\#/hr) | 0 | 0 | 0 |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 423 | 0 | 101 | 515 | 0 | 105 | 688 | 0 | 105 | 1149 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 21.0 | 21.0 |  | 11.0 | 21.0 |  | 6.0 | 17.0 |  | 6.0 | 17.0 |  |
| Minimum Split (s) | 34.0 | 34.0 |  | 15.0 | 49.0 |  | 9.0 | 52.0 |  | 9.0 | 52.0 |  |
| Total Split (s) | 34.0 | 34.0 |  | 15.0 | 49.0 |  | 9.0 | 52.0 |  | 9.0 | 52.0 |  |
| Total Split (\%) | 30.9\% | 30.9\% |  | 13.6\% | 44.5\% |  | 8.2\% | 47.3\% |  | 8.2\% | 47.3\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 0.0 | 0.0 |  | 1.0 | 1.0 |  | 0.0 | 1.0 |  | 0.0 | 1.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 3.0 |  | 4.0 | 4.0 |  | 3.0 | 4.0 |  | 3.0 | 4.0 |  |
| Lead/Lag | Lead | Lead |  | Lag |  |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | None | C-Max |  | None | C-Max |  |
| Act Effct Green (s) |  | 31.0 |  | 45.0 | 45.0 |  | 55.0 | 48.0 |  | 55.0 | 48.0 |  |
| Actuated g/C Ratio |  | 0.28 |  | 0.41 | 0.41 |  | 0.50 | 0.44 |  | 0.50 | 0.44 |  |


| $\rangle$ |  |  | 7 |  |  | 4 | 4 |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.71 |  | 0.28 | 0.73 |  | 0.71 | 0.50 |  | 0.33 | 0.81 |  |
| Control Delay | 42.3 |  | 10.6 | 18.0 |  | 41.5 | 23.5 |  | 21.9 | 44.1 |  |
| Queue Delay | 0.0 |  | 5.7 | 20.6 |  | 0.0 | 2.3 |  | 1.2 | 0.0 |  |
| Total Delay | 42.3 |  | 16.3 | 38.6 |  | 41.5 | 25.8 |  | 23.1 | 44.1 |  |
| LOS | D |  | B | D |  | D | C |  | C | D |  |
| Approach Delay | 42.3 |  |  | 35.0 |  |  | 27.8 |  |  | 42.3 |  |
| Approach LOS | D |  |  | C |  |  | C |  |  | D |  |
| Queue Length 50th ( t ) | 137 |  | 17 | 346 |  | 36 | 177 |  | 56 | 455 |  |
| Queue Length 95th ( t ) | 197 |  | m22 | m488 |  | \#104 | 232 |  | m87 | 525 |  |
| Internal Link Dist (t) | 2618 |  |  | 99 |  |  | 1204 |  |  | 1259 |  |
| Turn Bay Length (t) |  |  |  |  |  | 100 |  |  | 100 |  |  |
| Base Capacity (vph) | 592 |  | 364 | 701 |  | 148 | 1384 |  | 315 | 1412 |  |
| Starvation Cap Reductn | 0 |  | 209 | 188 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 2 |  | 0 | 0 |  | 0 | 536 |  | 88 | 0 |  |
| Storage Cap Reductn | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.72 |  | 0.65 | 1.00 |  | 0.71 | 0.81 |  | 0.46 | 0.81 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Offset: $33(30 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.81 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 37.1 |  |  |  | Intersection LOS: D |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 96.5\% |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |

$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 3: Western Avenue \& 47th Street


|  | 4 | $\rightarrow$ |  | 7 |  |  | $4$ |  | $p$ | $v$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | $\hat{\dagger}$ |  |  | * $\uparrow$ |  | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume (vph) | 72 | 399 | 11 | 46 | 469 | 68 | 55 | 691 | 69 | 248 | 1206 | 67 |
| Future Volume (vph) | 72 | 399 | 11 | 46 | 469 | 68 | 55 | 691 | 69 | 248 | 1206 | 67 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 11 | 12 | 12 | 10 | 12 | 9 | 9 | 12 | 9 | 9 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 320 | 50 |  | 0 | 70 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 20 |  |  | 25 |  |  | 145 |  |  | 160 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | 0.98 | 1.00 |  |  | 0.99 |  |  | 0.99 |  |  | 1.00 |  |
| Frt |  | 0.996 |  |  | 0.983 |  |  | 0.986 |  |  | 0.992 |  |
| Flt Protected | 0.950 |  |  |  | 0.996 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1589 | 1665 | 0 | 0 | 2822 | 0 | 1624 | 3155 | 0 | 1624 | 3189 | 0 |
| Flt Permitted | 0.289 |  |  |  | 0.809 |  | 0.107 |  |  | 0.179 |  |  |
| Satd. Flow (perm) | 476 | 1665 | 0 | 0 | 2291 | 0 | 183 | 3155 | 0 | 306 | 3189 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 2 |  |  | 14 |  |  | 10 |  |  | 6 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 179 |  |  | 500 |  |  | 1309 |  |  | 1346 |  |
| Travel Time (s) |  | 4.1 |  |  | 11.4 |  |  | 29.8 |  |  | 30.6 |  |
| Confl. Peds. (\#/hr) | 30 |  | 11 | 11 |  | 30 | 2 |  | 14 | 14 |  | 2 |
| Confl. Bikes (\#/hr) |  |  | 2 |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 6\% | 6\% | 0\% | 0\% | 10\% | 0\% | 0\% | 1\% | 1\% | 0\% | 1\% | 1\% |
| Bus Blockages (\#/hr) | 0 | 9 | 9 | 0 | 10 | 10 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  | 0 | 0 | 0 |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 73 | 418 | 0 | 0 | 595 | 0 | 56 | 775 | 0 | 253 | 1299 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 7 | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 7 | 4 |  | 8 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 17.0 |  | 17.0 | 17.0 |  | 5.0 | 19.0 |  | 7.0 | 19.0 |  |
| Minimum Split (s) | 12.0 | 51.0 |  | 39.0 | 39.0 |  | 8.0 | 40.0 |  | 10.0 | 51.0 |  |
| Total Split (s) | 12.0 | 51.0 |  | 39.0 | 39.0 |  | 8.0 | 40.0 |  | 19.0 | 51.0 |  |
| Total Split (\%) | 10.9\% | 46.4\% |  | 35.5\% | 35.5\% |  | 7.3\% | 36.4\% |  | 17.3\% | 46.4\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 0.0 | 0.0 |  | 0.0 | 1.0 |  | 0.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 4.0 | 4.0 |  |  | 3.0 |  | 3.0 | 4.0 |  | 3.0 | 4.0 |  |
| Lead/Lag | Lag |  |  | Lead | Lead |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | None | C-Max |  | None | C-Max |  |
| Act Effct Green (s) | 47.0 | 47.0 |  |  | 36.0 |  | 43.5 | 37.5 |  | 56.0 | 48.6 |  |
| Actuated g/C Ratio | 0.43 | 0.43 |  |  | 0.33 |  | 0.40 | 0.34 |  | 0.51 | 0.44 |  |


|  | $\rangle$ | $\rightarrow$ |  |  |  |  | $\checkmark$ | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.26 | 0.59 |  |  | 0.78 |  | 0.41 | 0.72 |  | 0.77 | 0.92 |  |
| Control Delay | 15.1 | 16.8 |  |  | 41.3 |  | 24.3 | 36.1 |  | 27.7 | 41.5 |  |
| Queue Delay | 3.4 | 4.3 |  |  | 2.4 |  | 0.5 | 0.0 |  | 0.0 | 21.6 |  |
| Total Delay | 18.4 | 21.0 |  |  | 43.6 |  | 24.9 | 36.1 |  | 27.7 | 63.1 |  |
| LOS | B | C |  |  | D |  | C | D |  | C | E |  |
| Approach Delay |  | 20.6 |  |  | 43.6 |  |  | 35.3 |  |  | 57.3 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | E |  |
| Queue Length 50th (tt) | 17 | 102 |  |  | 194 |  | 19 | 251 |  | 141 | 520 |  |
| Queue Length 95th (t) | m27 | 134 |  |  | 267 |  | 41 | 325 |  | m166 | \#632 |  |
| Internal Link Dist (t) |  | 99 |  |  | 420 |  |  | 1229 |  |  | 1266 |  |
| Turn Bay Length (tt) |  |  |  |  |  |  | 50 |  |  | 70 |  |  |
| Base Capacity (vph) | 284 | 712 |  |  | 759 |  | 137 | 1081 |  | 347 | 1412 |  |
| Starvation Cap Reductn | 143 | 215 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 75 |  | 9 | 0 |  | 0 | 162 |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.52 | 0.84 |  |  | 0.87 |  | 0.44 | 0.72 |  | 0.73 | 1.04 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: $40(36 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.92 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 44.5 |  |  |  | Intersection LOS: D |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 91.5\% |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 4: Western Boulevard \& 47th Street




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | - | r |  |
| Traffic Vol, veh/h | 311 | 8 | 13 | 561 | 22 | 15 |
| Future Vol, veh/h | 311 | 8 | 13 | 561 | 22 | 15 |
| Conflicting Peds, \#/hr | 0 | 3 | 3 | 0 | 1 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, $\%$ | 9 | 0 | 8 | 2 | 5 | 0 |
| Mvmt Flow | 327 | 8 | 14 | 591 | 23 | 16 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * |  | 中\% |  |  | $\uparrow \uparrow$ |
| Traffic Vol, veh/h | 2 | 2 | 865 | 0 | 0 | 1494 |
| Future Vol, veh/h | 2 | 2 | 865 | 0 | 0 | 1494 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 0 | 1 | 0 | 0 | 1 |
| Mvmt Flow | 2 | 2 | 911 | 0 | 0 | 1573 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1698 | 456 | 0 | 0 | 911 | 0 |
| Stage 1 | 911 | - | - | - | - | - |
| Stage 2 | 787 | - | - | - | - | - |
| Critical Hdwy | 6.8 | 6.9 | - | - | 4.1 | - |
| Critical Hdwy Stg 1 | 5.8 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.8 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | - | - | 2.2 | - |
| Pot Cap-1 Maneuver | 85 | 557 | - | - | 756 | - |
| Stage 1 | 357 | - | - | - | - | - |
| Stage 2 | 414 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 85 | 557 | - | - | 756 | - |
| Mov Cap-2 Maneuver | 85 | - | - | - | - | - |
| Stage 1 | 357 | - | - | - | - | - |
| Stage 2 | 414 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 30.2 |  | 0 |  | 0 |  |
| HCM LOS | D |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 147 | 756 | - |
| HCM Lane V/C Ratio |  | - | - | 0.029 | - | - |
| HCM Control Delay (s) |  | - | - | 30.2 | 0 | - |
| HCM Lane LOS |  | - | - | D | A | - |
| HCM 95th \%tile Q(veh) |  | - | - | 0.1 | 0 | - |

## Appendix IV: Table 5-1: Link Emission Factor Calculations

Table 5.1: MOVES Links Worksheet

|  | ProjectName: 53:3398 Wheatland Tube Traffic Volumes |  |  |  |  |  | Approach Delay (s) |  | Link Length |  | MOVES Emissions Factors |  |  | Emissions (g/s) NO2 |  | Emissions (g/s) PM10 |  | Emissions (g/s) PM2.5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vtype | StreetName | Dir. | Type | SBIN | AM | PM | AM | PM | Length (m) ${ }^{\text {L }}$ | Length (mi) | NO2 | PM10 | PM2.5 | AM | PM | AM | PM | AM | PM |
| Car | 45ST | EB1 | ACC | 4 | 14 | 3 |  |  | 31.9 | 0.020 | 0.032582 | 0.002064 | 0.001825 | 0.00000251517 | 0.00000053897 | 0.00000015930 | 0.00000003414 | 0.00000014092 | 0.00000003020 |
| Car | 45ST | EB2 | DEC | 2 | 14 | 3 |  |  | 22.0 | 0.014 | 0.038301 | 0.003871 | 0.003425 | 0.00000203155 | 0.00000043533 | 0.00000020535 | 0.00000004400 | 0.00000018165 | 0.00000003893 |
| Car | 45ST | EB2 | QUE | 0 | 14 | 3 | 29.7 | 24.4 | 22.0 | 0.014 | 0.098636 | 0.016165 | 0.014300 | 0.00000316456 | 0.00000055711 | 0.00000051864 | 0.00000009131 | 0.00000045880 | 0.00000008077 |
| Car | 45ST | EB2 | ACC | 4 | 26 | 6 |  |  | 27.6 | 0.017 | 0.032582 | 0.002064 | 0.001825 | 0.00000403078 | 0.00000093018 | 0.00000025529 | 0.00000005891 | 0.00000022583 | 0.00000005212 |
| Car | 45ST | EB2 | FFD | 7 | 26 | 6 |  |  | 132.9 | 0.083 | 0.027878 | 0.001348 | 0.001193 | 0.00001662982 | 0.00000383765 | 0.00000080436 | 0.00000018562 | 0.00000071154 | 0.00000016420 |
| Car | 45ST | WB1 | FFA | 7 | 3 | 25 |  |  | 118.1 | 0.073 | 0.027878 | 0.001348 | 0.001193 | 0.00000170552 | 0.00001421266 | 0.00000008249 | 0.00000068744 | 0.00000007297 | 0.00000060812 |
| Car | 45ST | WB1 | DEC | 2 | 3 | 25 |  |  | 16.1 | 0.010 | 0.038301 | 0.003871 | 0.003425 | 0.00000031981 | 0.00000266506 | 0.00000003233 | 0.00000026938 | 0.00000002860 | 0.00000023830 |
| Car | 45ST | WB1 | QUE | 0 | 3 | 25 | 25.9 | 25.3 | 16.1 | 0.010 | 0.098636 | 0.016165 | 0.014300 | 0.00000059136 | 0.00000481381 | 0.00000009692 | 0.00000078894 | 0.00000008574 | 0.00000069791 |
| Car | 45ST | WB1 | ACC | 4 | 2 | 14 |  |  | 31.6 | 0.020 | 0.032582 | 0.002064 | 0.001825 | 0.00000035514 | 0.00000248601 | 0.00000002249 | 0.00000015745 | 0.00000001990 | 0.00000013928 |
| Car | 45ST | WB2 | DEC | 2 | 2 | 14 |  |  | 17.0 | 0.011 | 0.038301 | 0.003871 | 0.003425 | 0.00000022508 | 0.00000157559 | 0.00000002275 | 0.00000015926 | 0.00000002013 | 0.00000014088 |
| Car | 45ST | WB2 | QUE | 0 | 2 | 14 | 25.2 | 33.3 | 17.0 | 0.011 | 0.098636 | 0.016165 | 0.014300 | 0.00000038358 | 0.00000354814 | 0.00000006287 | 0.00000058151 | 0.00000005561 | 0.00000051441 |
| Car | 47ST | EB1 | FFA | 7 | 6 | 1 |  |  | 246.2 | 0.153 | 0.027878 | 0.001348 | 0.001193 | 0.00000710876 | 0.00000118479 | 0.00000034384 | 0.00000005731 | 0.00000030416 | 0.00000005069 |
| Car | 47ST | EB1 | DEC | 2 | 6 | 1 |  |  | 41.9 | 0.026 | 0.038301 | 0.003871 | 0.003425 | 0.00000166015 | 0.00000027669 | 0.00000016781 | 0.00000002797 | 0.00000014845 | 0.00000002474 |
| Car | 47ST | EB1 | QUE | 0 | 6 | 1 | 39.9 | 42.7 | 41.9 | 0.026 | 0.098636 | 0.016165 | 0.014300 | 0.00000182202 | 0.00000032498 | 0.00000029861 | 0.00000005326 | 0.00000026416 | 0.00000004712 |
| Car | 47ST | EB2 | DEC | 2 | 10 | 2 |  |  | 52.4 | 0.033 | 0.038301 | 0.003871 | 0.003425 | 0.00000346626 | 0.00000069325 | 0.00000035037 | 0.00000007007 | 0.00000030994 | 0.00000006199 |
| Car | 47ST | EB2 | QUE | 0 | 10 | 2 | 27.7 | 20.9 | 52.4 | 0.033 | 0.098636 | 0.016165 | 0.014300 | 0.00000210818 | 0.00000031813 | 0.00000034551 | 0.00000005214 | 0.00000030565 | 0.00000004612 |
| Car | 47ST | EB2 | ACC | 4 | 14 | 6 |  |  | 30.6 | 0.019 | 0.032582 | 0.002064 | 0.001825 | 0.00000240999 | 0.00000103285 | 0.00000015264 | 0.00000006542 | 0.00000013503 | 0.00000005787 |
| Car | 47ST | EB2 | FFD | 7 | 14 | 6 |  |  | 102.1 | 0.063 | 0.027878 | 0.001348 | 0.001193 | 0.00000687702 | 0.00000294730 | 0.00000033263 | 0.00000014256 | 0.00000029425 | 0.00000012611 |
| Car | 47ST | EB3 | FFA | 6 | 14 | 6 | 0 | 0 | 35.6 | 0.022 | 0.030816 | 0.001479 | 0.001308 | 0.00000265366 | 0.00000113728 | 0.00000012734 | 0.00000005458 | 0.00000011265 | 0.00000004828 |
| Car | 47ST | EB3 | FFD | 6 | 2 | 11 | 0 | 0 | 170.8 | 0.106 | 0.030816 | 0.001479 | 0.001308 | 0.00000181745 | 0.00000999598 | 0.00000008721 | 0.00000047968 | 0.00000007715 | 0.00000042433 |
| Car | 47ST | EBL2 | DEC | 2 | 1 | 0 |  |  | 52.2 | 0.032 | 0.038301 | 0.003871 | 0.003425 | 0.00000034517 | 0.00000000000 | 0.00000003489 | 0.00000000000 | 0.00000003086 | 0.00000000000 |
| Car | 47ST | EBL2 | QUE | 0 | 1 | 0 | 27.7 | 20.9 | 52.2 | 0.032 | 0.098636 | 0.016165 | 0.014300 | 0.00000021082 | 0.00000000000 | 0.00000003455 | 0.00000000000 | 0.00000003056 | 0.00000000000 |
| Car | 47ST | WB1 | FFA | 6 | 13 | 3 | 0 | 0 | 171.1 | 0.106 | 0.030816 | 0.001479 | 0.001308 | 0.00001183392 | 0.00000273090 | 0.00000056788 | 0.00000013105 | 0.00000050236 | 0.00000011593 |
| Car | 47ST | WB1 | FFD | 6 | 6 | 14 | 0 | 0 | 35.5 | 0.022 | 0.030816 | 0.001479 | 0.001308 | 0.00000113342 | 0.00000264464 | 0.00000005439 | 0.00000012691 | 0.00000004811 | 0.00000011227 |
| Car | 47ST | WB2 | FFA | 7 | 6 | 14 |  |  | 46.8 | 0.029 | 0.027878 | 0.001348 | 0.001193 | 0.00000135132 | 0.00000315308 | 0.00000006536 | 0.00000015251 | 0.00000005782 | 0.00000013491 |
| Car | 47ST | WB2 | DEC | 2 | 6 | 14 |  |  | 59.1 | 0.037 | 0.038301 | 0.003871 | 0.003425 | 0.00000234362 | 0.00000546846 | 0.00000023689 | 0.00000055275 | 0.00000020956 | 0.00000048897 |
| Car | 47ST | WB2 | QUE | 0 | 6 | 14 | 35.8 | 43.9 | 59.1 | 0.037 | 0.098636 | 0.016165 | 0.014300 | 0.00000163479 | 0.00000467758 | 0.00000026793 | 0.00000076661 | 0.00000023701 | 0.00000067816 |
| Car | 47ST | WB3 | DEC | 2 | 2 | 6 |  |  | 48.9 | 0.030 | 0.038301 | 0.003871 | 0.003425 | 0.00000064681 | 0.00000194044 | 0.00000006538 | 0.00000019614 | 0.00000005784 | 0.00000017351 |
| Car | 47ST | WB3 | QUE | 0 | 2 | 6 | 8.4 | 35.6 | 48.9 | 0.030 | 0.098636 | 0.016165 | 0.014300 | 0.00000012786 | 0.00000162566 | 0.00000002096 | 0.00000026643 | 0.00000001854 | 0.00000023569 |
| Car | 47ST | WB3 | ACC | 4 | 1 | 6 |  |  | 30.5 | 0.019 | 0.032582 | 0.002064 | 0.001825 | 0.00000017148 | 0.00000102891 | 0.00000001086 | 0.00000006517 | 0.00000000961 | 0.00000005765 |
| Car | 47ST | WB3 | FFD | 7 | 1 | 6 |  |  | 288.2 | 0.179 | 0.027878 | 0.001348 | 0.001193 | 0.00000138654 | 0.00000831926 | 0.00000006706 | 0.00000040239 | 0.00000005933 | 0.00000035596 |
| Car | 47ST | WBL3 | DEC | 2 | 0 | 4 |  |  | 48.8 | 0.030 | 0.038301 | 0.003871 | 0.003425 | 0.00000000000 | 0.00000129099 | 0.00000000000 | 0.00000013049 | 0.00000000000 | 0.00000011544 |
| Car | 47ST | WBL3 | QUE | 0 | 0 | 4 | 8.4 | 35.6 | 48.8 | 0.030 | 0.098636 | 0.016165 | 0.014300 | 0.00000000000 | 0.00000108377 | 0.00000000000 | 0.00000017762 | 0.00000000000 | 0.00000015713 |
| Car | OAKA | NB | ACC | 4 | 24 | 6 |  |  | 41.7 | 0.026 | 0.032582 | 0.002064 | 0.001825 | 0.00000562234 | 0.00000140559 | 0.00000035609 | 0.00000008902 | 0.00000031500 | 0.00000007875 |
| Car | OAKA | SB | DEC | 2 | 5 | 22 |  |  | 27.5 | 0.017 | 0.038301 | 0.003871 | 0.003425 | 0.00000091063 | 0.00000400679 | 0.00000009205 | 0.00000040500 | 0.00000008143 | 0.00000035827 |
| Car | OAKA | SB | QUE | 0 | 5 | 22 | 26.9 | 36.4 | 27.5 | 0.017 | 0.098636 | 0.016165 | 0.014300 | 0.00000102365 | 0.00000609470 | 0.00000016777 | 0.00000099887 | 0.00000014841 | 0.00000088362 |
| Car | WAVE | NB1 | FFA | 7 | 9 | 2 |  |  | 166.5 | 0.103 | 0.027878 | 0.001348 | 0.001193 | 0.00000721222 | 0.00000160272 | 0.00000034884 | 0.00000007752 | 0.00000030859 | 0.00000006858 |
| Car | WAVE | NB1 | DEC |  | 9 | 2 |  |  | 116.0 | 0.072 | 0.038301 | 0.003871 | 0.003425 | 0.00000690218 | 0.00000153382 | 0.00000069767 | 0.00000015504 | 0.00000061717 | 0.00000013715 |
| Car | WAVE | NB1 | QUE | 0 | 9 | 2 | 70.5 | 27.9 | 116.0 | 0.072 | 0.098636 | 0.016165 | 0.014300 | 0.00000482903 | 0.00000042468 | 0.00000079144 | 0.00000006960 | 0.00000070012 | 0.00000006157 |
| Car | WAVE | NB1 | ACC | 4 | 6 | 2 |  |  | 31.0 | 0.019 | 0.032582 | 0.002064 | 0.001825 | 0.00000104547 | 0.00000034849 | 0.00000006621 | 0.00000002207 | 0.00000005857 | 0.00000001952 |
| Car | WAVE | NB1 | FFD | 7 | 6 | 2 |  |  | 184.5 | 0.115 | 0.027878 | 0.001348 | 0.001193 | 0.00000532651 | 0.00000177550 | 0.00000025763 | 0.00000008588 | 0.00000022791 | 0.00000007597 |
| Car | WAVE | NB2 | FFA | 7 | 6 | 2 |  |  | 176.2 | 0.109 | 0.027878 | 0.001348 | 0.001193 | 0.00000508582 | 0.00000169527 | 0.00000024599 | 0.00000008200 | 0.00000021761 | 0.00000007254 |
| Car | WAVE | NB2 | DEC | 2 | 6 | 2 |  |  | 16.0 | 0.010 | 0.038301 | 0.003871 | 0.003425 | 0.00000063441 | 0.00000021147 | 0.00000006413 | 0.00000002138 | 0.00000005673 | 0.00000001891 |
| Car | wave | NB2 | QUE | 0 | 6 | 2 | 4.6 | 3.3 | 16.0 | 0.010 | 0.098636 | 0.016165 | 0.014300 | 0.00000021006 | 0.00000005023 | 0.00000003443 | 0.00000000823 | 0.00000003045 | 0.00000000728 |
| Car | WAVE | NB2 | ACC | 4 | 2 | 9 |  |  | 30.7 | 0.019 | 0.032582 | 0.002064 | 0.001825 | 0.00000034549 | 0.00000155470 | 0.00000002188 | 0.00000009847 | 0.00000001936 | 0.00000008711 |
| Car | WAVE | NB2 | FFD | 7 | 2 | 9 |  |  | 370.5 | 0.230 | 0.027878 | 0.001348 | 0.001193 | 0.00000356525 | 0.00001604363 | 0.00000017245 | 0.00000077600 | 0.00000015255 | 0.00000068646 |
| Car | WAVE | SB1 | FFA | 7 | 10 | 2 |  |  | 298.1 | 0.185 | 0.027878 | 0.001348 | 0.001193 | 0.00001434244 | 0.00000286849 | 0.00000069372 | 0.00000013874 | 0.00000061367 | 0.00000012273 |
| Car | WAVE | SB1 | DEC | 2 | 10 | 2 |  |  | 82.4 | 0.051 | 0.038301 | 0.003871 | 0.003425 | 0.00000544753 | 0.00000108951 | 0.00000055063 | 0.00000011013 | 0.00000048710 | 0.00000009742 |
| Car | WAVE | SB1 | QUE | 0 | 10 | 2 | 14.4 | 17.4 | 82.4 | 0.051 | 0.098636 | 0.016165 | 0.014300 | 0.00000109595 | 0.00000026485 | 0.00000017962 | 0.00000004341 | 0.00000015889 | 0.00000003840 |
| Car | WAVE | SB1 | ACC | 4 | 2 | 6 |  |  | 30.1 | 0.019 | 0.032582 | 0.002064 | 0.001825 | 0.00000033842 | 0.00000101525 | 0.00000002143 | 0.00000006430 | 0.00000001896 | 0.00000005688 |
| Car | WAVE | SB1 | FFD | 7 | 2 | 6 |  |  | 182.9 | 0.114 | 0.027878 | 0.001348 | 0.001193 | 0.00000175983 | 0.00000527950 | 0.00000008512 | 0.00000025536 | 0.00000007530 | 0.00000022590 |
| Car | WAVE | SB2 | FFA | 7 | 2 | 6 |  |  | 51.3 | 0.032 | 0.027878 | 0.001348 | 0.001193 | 0.00000049342 | 0.00000148025 | 0.00000002387 | 0.00000007160 | 0.00000002111 | 0.00000006334 |
| Car | WAVE | SB2 | DEC | 2 | 1 | 6 |  |  | 138.5 | 0.086 | 0.038301 | 0.003871 | 0.003425 | 0.00000091571 | 0.00000549424 | 0.00000009256 | 0.00000055535 | 0.00000008188 | 0.00000049128 |
| Car | wave | SB2 | QUE | 0 | 1 | 6 | 40.3 | 42.5 | 138.5 | 0.086 | 0.098636 | 0.016165 | 0.014300 | 0.00000030671 | 0.00000194074 | 0.00000005027 | 0.00000031807 | 0.00000004447 | 0.00000028137 |
| Car | wave | SB2 | ACC | 4 | 1 | 9 |  |  | 30.3 | 0.019 | 0.032582 | 0.002064 | 0.001825 | 0.00000017038 | 0.00000153346 | 0.00000001079 | 0.00000009712 | 0.00000000955 | 0.00000008592 |
| Car | WAVE | SB2 | FFD | 7 | 1 | 9 |  |  | 278.2 | 0.173 | 0.027878 | 0.001348 | 0.001193 | 0.00000133852 | 0.00001204672 | 0.00000006474 | 0.00000058268 | 0.00000005727 | 0.00000051545 |

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Table 5.1: MOVES Links Worksheet

|  | ProjectName: 53:3398 Wheatland Tube |  |  |  | Traffic Volumes |  | Approach Delay (s) |  | Link Length |  | MOVES Emissions Factors |  |  | Emissions (g/s) NO2 |  | Emissions (g/s) PM10 |  | Emissions (g/s) PM2.5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vtype | StreetName | Dir. | Type | SBIN | AM | PM | AM | PM | Length ( m ) | Length (mi) | NO2 | PM10 | PM2.5 | AM | PM | AM | PM | AM | PM |
| Car | WAVE | SBL2 | DEC | 2 | 1 | 0 |  |  | 31.8 | 0.020 | 0.038301 | 0.003871 | 0.003425 | 0.00000021005 | 0.00000000000 | 0.00000002123 | 0.00000000000 | 0.00000001878 | 0.00000000000 |
| Car | WAVE | SBL2 | QUE | 0 | 1 | 0 | 40.3 | 42.5 | 31.8 | 0.020 | 0.098636 | 0.016165 | 0.014300 | 0.00000030671 | 0.00000000000 | 0.00000005027 | 0.00000000000 | 0.00000004447 | 0.00000000000 |
| Car | WBLD | NB1 | FFA | 7 | 9 | 2 |  |  | 148.0 | 0.092 | 0.027878 | 0.001348 | 0.001193 | 0.00000640911 | 0.00000142425 | 0.00000031000 | 0.00000006889 | 0.00000027423 | 0.00000006094 |
| Car | WBLD | NB1 | DEC | 2 | 9 | 2 |  |  | 133.2 | 0.083 | 0.038301 | 0.003871 | 0.003425 | 0.00000792727 | 0.00000176162 | 0.00000080128 | 0.00000017806 | 0.00000070883 | 0.00000015752 |
| Car | WBLD | NB1 | QUE | 0 | 9 | 2 | 54.2 | 35.4 | 133.2 | 0.083 | 0.098636 | 0.016165 | 0.014300 | 0.00000371253 | 0.00000053884 | 0.00000060845 | 0.00000008831 | 0.00000053825 | 0.00000007812 |
| Car | WBLD | NB1 | ACC | 4 | 9 | 2 |  |  | 30.6 | 0.019 | 0.032582 | 0.002064 | 0.001825 | 0.00000154749 | 0.00000034389 | 0.00000009801 | 0.00000002178 | 0.00000008670 | 0.00000001927 |
| Car | WBLD | NB1 | FFD | 7 | 9 | 2 |  |  | 181.8 | 0.113 | 0.027878 | 0.001348 | 0.001193 | 0.00000787125 | 0.00000174917 | 0.00000038072 | 0.00000008460 | 0.00000033679 | 0.00000007484 |
| Car | WBLD | NB2 | FFA | 7 | 9 | 2 |  |  | 175.0 | 0.109 | 0.027878 | 0.001348 | 0.001193 | 0.00000757934 | 0.00000168430 | 0.00000036660 | 0.00000008147 | 0.00000032430 | 0.00000007207 |
| Car | WBLD | NB2 | DEC | 2 | 9 | 2 |  |  | 22.5 | 0.014 | 0.038301 | 0.003871 | 0.003425 | 0.00000133775 | 0.00000029728 | 0.00000013522 | 0.00000003005 | 0.00000011962 | 0.00000002658 |
| Car | WBLD | NB2 | QUE | 0 | 9 | 2 | 6.1 | 4.8 | 22.5 | 0.014 | 0.098636 | 0.016165 | 0.014300 | 0.00000041783 | 0.00000007306 | 0.00000006848 | 0.00000001197 | 0.00000006058 | 0.00000001059 |
| Car | WBLD | NB2 | ACC | 4 | 3 | 5 |  |  | 30.2 | 0.019 | 0.032582 | 0.002064 | 0.001825 | 0.00000050977 | 0.00000084961 | 0.00000003229 | 0.00000005381 | 0.00000002856 | 0.00000004760 |
| Car | WBLD | NB2 | FFD | 7 | 3 | 5 |  |  | 369.8 | 0.230 | 0.027878 | 0.001348 | 0.001193 | 0.00000533764 | 0.00000889606 | 0.00000025817 | 0.00000043029 | 0.00000022838 | 0.00000038064 |
| Car | WBLD | SB1 | FFA | 7 | 7 | 2 |  |  | 350.7 | 0.218 | 0.027878 | 0.001348 | 0.001193 | 0.00001181141 | 0.00000337469 | 0.00000057130 | 0.00000016323 | 0.00000050538 | 0.00000014439 |
| Car | WBLD | SB1 | DEC | 2 | 5 | 4 |  |  | 31.7 | 0.020 | 0.038301 | 0.003871 | 0.003425 | 0.00000104875 | 0.00000083900 | 0.00000010601 | 0.00000008481 | 0.00000009378 | 0.00000007502 |
| Car | WBLD | SB1 | QUE | 0 | 5 | 4 | 10.3 | 19 | 31.7 | 0.020 | 0.098636 | 0.016165 | 0.014300 | 0.00000039195 | 0.00000057842 | 0.00000006424 | 0.00000009480 | 0.00000005683 | 0.00000008386 |
| Car | WBLD | SB1 | ACC | 4 | 0 | 10 |  |  | 30.5 | 0.019 | 0.032582 | 0.002064 | 0.001825 | 0.00000000000 | 0.00000171413 | 0.00000000000 | 0.00000010856 | 0.00000000000 | 0.00000009604 |
| Car | WBLD | SB1 | FFD | 7 | 0 | 10 |  |  | 184.6 | 0.115 | 0.027878 | 0.001348 | 0.001193 | 0.00000000000 | 0.00000888406 | 0.00000000000 | 0.00000042971 | 0.00000000000 | 0.00000038012 |
| Car | WBLD | SB2 | FFA | 7 | 0 | 9 |  |  | 135.0 | 0.084 | 0.027878 | 0.001348 | 0.001193 | 0.00000000000 | 0.00000584429 | 0.00000000000 | 0.00000028268 | 0.00000000000 | 0.00000025006 |
| Car | WBLD | SB2 | DEC | 2 | 0 | 8 |  |  | 54.5 | 0.034 | 0.038301 | 0.003871 | 0.003425 | 0.00000000000 | 0.00000288476 | 0.00000000000 | 0.00000029159 | 0.00000000000 | 0.00000025795 |
| Car | WBLD | SB2 | QUE | 0 | 0 | 8 | 49.4 | 57.1 | 54.5 | 0.034 | 0.098636 | 0.016165 | 0.014300 | 0.00000000000 | 0.00000347660 | 0.00000000000 | 0.00000056978 | 0.00000000000 | 0.00000050404 |
| Car | WBLD | SB2 | ACC | 4 | 1 | 9 |  |  | 30.5 | 0.019 | 0.032582 | 0.002064 | 0.001825 | 0.00000017167 | 0.00000154503 | 0.000000001087 | 0.00000009785 | 0.00000000962 | 0.00000008656 |
| Car | WBLD | SB2 | FFD | 7 | 1 | 9 |  |  | 273.8 | 0.170 | 0.027878 | 0.001348 | 0.001193 | 0.00000131758 | 0.00001185820 | 0.00000006373 | 0.00000057356 | 0.00000005638 | 0.00000050738 |
| Car | WBLD | SBL2 | DEC | 2 | 0 | 1 |  |  | 39.7 | 0.025 | 0.038301 | 0.003871 | 0.003425 | 0.00000000000 | 0.00000026273 | 0.00000000000 | 0.00000002656 | 0.00000000000 | 0.00000002349 |
| Car | WBLD | SBL2 | QUE | 0 | 0 | 1 | 49.4 | 57.1 | 39.7 | 0.025 | 0.098636 | 0.016165 | 0.014300 | 0.00000000000 | 0.00000043457 | 0.00000000000 | 0.00000007122 | 0.00000000000 | 0.00000006301 |
| Truck | 45ST | EB1 | ACC | 4 | 2 | 5 |  |  | 31.9 | 0.020 | 9.939110 | 0.186020 | 0.171138 | 0.00010960704 | 0.00027401761 | 0.00000205140 | 0.00000512850 | 0.00000188729 | 0.00000471822 |
| Truck | 45ST | EB2 | DEC | 2 | 2 | 5 |  |  | 22.0 | 0.014 | 21.315400 | 0.326079 | 0.299992 | 0.00016151458 | 0.00040378645 | 0.00000247082 | 0.00000617705 | 0.00000227315 | 0.00000568287 |
| Truck | 45ST | EB2 | QUE | 0 | 2 | 5 | 29.7 | 24.4 | 22.0 | 0.014 | 52.932200 | 1.014298 | 0.933151 | 0.00024260592 | 0.00049828151 | 0.00000464887 | 0.00000954818 | 0.00000427694 | 0.00000878429 |
| Truck | 45ST | EB2 | ACC | 4 | 2 | 5 |  |  | 27.6 | 0.017 | 9.939110 | 0.186020 | 0.171138 | 0.00009458332 | 0.00023645829 | 0.00000177022 | 0.00000442554 | 0.00000162860 | 0.00000407150 |
| Truck | 45ST | EB2 | FFD | 7 | 2 | 5 |  |  | 132.9 | 0.083 | 6.352800 | 0.145501 | 0.133860 | 0.00029151027 | 0.00072877569 | 0.00000667658 | 0.00001669144 | 0.00000614241 | 0.00001535603 |
| Truck | 45ST | WB1 | FFA | 7 | 5 | 4 |  |  | 118.1 | 0.073 | 6.352800 | 0.145501 | 0.133860 | 0.00064776141 | 0.00051820913 | 0.00001483594 | 0.00001186875 | 0.00001364898 | 0.00001091918 |
| Truck | 45ST | WB1 | DEC | 2 | 5 | 4 |  |  | 16.1 | 0.010 | 21.315400 | 0.326079 | 0.299992 | 0.00029663248 | 0.00023730598 | 0.00000453783 | 0.00000363026 | 0.00000417479 | 0.00000333983 |
| Truck | 45ST | WB1 | QUE | 0 | 5 | 4 | 25.9 | 25.3 | 16.1 | 0.010 | 52.932200 | 1.014298 | 0.933151 | 0.00052891357 | 0.00041332860 | 0.00001013515 | 0.00000792029 | 0.00000932431 | 0.00000728664 |
| Truck | 45ST | WB1 | ACC | 4 | 5 | 4 |  |  | 31.6 | 0.020 | 9.939110 | 0.186020 | 0.171138 | 0.00027084022 | 0.00021667218 | 0.00000506904 | 0.00000405523 | 0.00000466351 | 0.00000373081 |
| Truck | 45ST | WB2 | DEC | 2 | 5 | 4 |  |  | 17.0 | 0.011 | 21.315400 | 0.326079 | 0.299992 | 0.00031316106 | 0.00025052885 | 0.00000479068 | 0.00000383254 | 0.00000440741 | 0.00000352593 |
| Truck | 45ST | WB2 | QUE | 0 | 5 | 4 | 25.2 | 33.3 | 17.0 | 0.011 | 52.932200 | 1.014298 | 0.933151 | 0.00051461861 | 0.00054402539 | 0.00000986123 | 0.00001042473 | 0.00000907230 | 0.00000959072 |
| Truck | 47ST | EB1 | FFA | 7 | 2 | 3 |  |  | 246.2 | 0.153 | 6.352800 | 0.145501 | 0.133860 | 0.00053998596 | 0.00080997894 | 0.00001236751 | 0.00001855127 | 0.00001137804 | 0.00001706706 |
| Truck | 47ST | EB1 | DEC | 2 | 2 | 3 |  |  | 41.9 | 0.026 | 21.315400 | 0.326079 | 0.299992 | 0.00030796971 | 0.00046195457 | 0.00000471126 | 0.00000706689 | 0.00000433435 | 0.00000650152 |
| Truck | 47ST | EB1 | QUE | 0 | 2 | 3 | 39.9 | 42.7 | 41.9 | 0.026 | 52.932200 | 1.014298 | 0.933151 | 0.00032592512 | 0.00052319559 | 0.00000624545 | 0.00001002558 | 0.00000574579 | 0.00000922351 |
| Truck | 47ST | EB2 | DEC | 2 | 4 | 5 |  |  | 52.4 | 0.033 | 21.315400 | 0.326079 | 0.299992 | 0.00077161990 | 0.00096452488 | 0.00001180409 | 0.00001475511 | 0.00001085973 | 0.00001357466 |
| Truck | 47ST | EB2 | QUE | 0 | 4 | 5 | 27.7 | 20.9 | 52.4 | 0.033 | 52.932200 | 1.014298 | 0.933151 | 0.00045253764 | 0.00042680671 | 0.00000867162 | 0.00000817856 | 0.00000797787 | 0.00000752425 |
| Truck | 47ST | EB2 | ACC | 4 | 4 | 5 |  |  | 30.6 | 0.019 | 9.939110 | 0.186020 | 0.171138 | 0.00021004695 | 0.00026255869 | 0.00000393123 | 0.00000491404 | 0.00000361673 | 0.00000452091 |
| Truck | 47ST | EB2 | FFD | 7 | 4 | 5 |  |  | 102.1 | 0.063 | 6.352800 | 0.145501 | 0.133860 | 0.00044775685 | 0.00055969607 | 0.00001025515 | 0.00001281894 | 0.00000943468 | 0.00001179335 |
| Truck | 47ST | EB3 | FFA | 6 | 4 | 5 | 0 | 0 | 35.6 | 0.022 | 6.992000 | 0.152765 | 0.140544 | 0.00017202729 | 0.00021503412 | 0.00000375855 | 0.00000469818 | 0.00000345786 | 0.00000432233 |
| Truck | 47ST | EB3 | FFD | 6 | 2 | 2 | 0 | 0 | 170.8 | 0.106 | 6.992000 | 0.152765 | 0.140544 | 0.00041236547 | 0.00041236547 | 0.00000900958 | 0.00000900958 | 0.00000828882 | 0.00000828882 |
| Truck | 47ST | WB1 | FFA | 6 | 1 | 2 | 0 | 0 | 171.1 | 0.106 | 6.992000 | 0.152765 | 0.140544 | 0.00020654026 | 0.00041308052 | 0.00000451260 | 0.00000902521 | 0.00000415160 | 0.00000830319 |
| Truck | 47ST | WB1 | FFD | 6 | 5 | 4 | 0 | 0 | 35.5 | 0.022 | 6.992000 | 0.152765 | 0.140544 | 0.00021430299 | 0.00017144239 | 0.00000468221 | 0.00000374577 | 0.00000430763 | 0.00000344610 |
| Truck | 47ST | WB2 | FFA | 7 | 5 | 4 |  |  | 46.8 | 0.029 | 6.352800 | 0.145501 | 0.133860 | 0.00025661817 | 0.00020529454 | 0.00000587743 | 0.00000470194 | 0.00000540720 | 0.00000432576 |
| Truck | 47ST | WB2 | DEC | 2 | 5 | 4 |  |  | 59.1 | 0.037 | 21.315400 | 0.326079 | 0.299992 | 0.00108689878 | 0.00086951902 | 0.00001662716 | 0.00001330173 | 0.00001529695 | 0.00001223756 |
| Truck | 47ST | WB2 | QUE | 0 | 5 | 4 | 35.8 | 43.9 | 59.1 | 0.037 | 52.932200 | 1.014298 | 0.933151 | 0.00073108517 | 0.00071719864 | 0.00001400921 | 0.00001374311 | 0.00001288843 | 0.00001264362 |
| Truck | 47ST | WB3 | DEC | 2 | 4 | 4 |  |  | 48.9 | 0.030 | 21.315400 | 0.326079 | 0.299992 | 0.00071993034 | 0.00071993034 | 0.00001101335 | 0.00001101335 | 0.00001013225 | 0.00001013225 |
| Truck | 47ST | WB3 | QUE | 0 | 4 | 4 | 8.4 | 35.6 | 48.9 | 0.030 | 52.932200 | 1.014298 | 0.933151 | 0.00013723163 | 0.00058160072 | 0.00000262966 | 0.00001114476 | 0.00000241928 | 0.00001025314 |
| Truck | 47ST | WB3 | ACC | 4 | 3 | 3 |  |  | 30.5 | 0.019 | 9.939110 | 0.186020 | 0.171138 | 0.00015693334 | 0.00015693334 | 0.00000293716 | 0.00000293716 | 0.00000270218 | 0.00000270218 |
| Truck | 47ST | WB3 | FFD | 7 | 3 | 3 |  |  | 288.2 | 0.179 | 6.352800 | 0.145501 | 0.133860 | 0.00094790487 | 0.00094790487 | 0.00002171024 | 0.00002171024 | 0.00001997330 | 0.00001997330 |
| Truck | 47ST | WBL3 | DEC | 2 | 1 | 0 |  |  | 48.8 | 0.030 | 21.315400 | 0.326079 | 0.299992 | 0.00017961545 | 0.00000000000 | 0.00000274772 | 0.00000000000 | 0.00000252790 | 0.00000000000 |
| Truck | 47ST | WBL3 | QUE | 0 | 1 | 0 | 8.4 | 35.6 | 48.8 | 0.030 | 52.932200 | 1.014298 | 0.933151 | 0.00003430791 | 0.00000000000 | 0.00000065742 | 0.00000000000 | 0.00000060482 | 0.00000000000 |
| Truck | OAKA | NB | ACC | 4 | 5 | 7 |  |  | 41.7 | 0.026 | 9.939110 | 0.186020 | 0.171138 | 0.00035730938 | 0.00050023314 | 0.00000668739 | 0.00000936234 | 0.00000615239 | 0.00000861335 |

Table 5.1: MOVES Links Worksheet

|  | ProjectName: 53:3398 Wheatland Tube |  |  |  | Traffic Volumes |  | Approach Delay (s) |  | Link Length |  | MOVES Emissions Factors |  |  | Emissions (g/s) NO2 |  | Emissions (g/s) PM10 |  | Emissions (g/s) PM2.5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vtype | StreetName | Dir. | Type | SBIN | AM | PM | AM | PM | Length (m) | Length (mi) | NO2 | PM10 | PM2.5 | AM | PM | AM | PM | AM | PM |
| Truck | OAKA | SB | DEC | 2 | 7 | 6 |  |  | 27.5 | 0.017 | 21.315400 | 0.326079 | 0.299992 | 0.00070950258 | 0.00060814507 | 0.00001085383 | 0.00000930328 | 0.00000998549 | 0.00000855900 |
| Truck | OAKA | SB | QUE | 0 | 7 | 6 | 26.9 | 36.4 | 27.5 | 0.017 | 52.932200 | 1.014298 | 0.933151 | 0.00076906892 | 0.00089200559 | 0.00001473706 | 0.00001709280 | 0.00001355805 | 0.00001572532 |
| Truck | WAVE | NB1 | FFA | 7 | 1 | 2 |  |  | 166.5 | 0.103 | 6.352800 | 0.145501 | 0.133860 | 0.00018261489 | 0.00036522978 | 0.00000418250 | 0.00000836500 | 0.00000384788 | 0.00000769575 |
| Truck | WAVE | NB1 | DEC | 2 | 1 | 2 |  |  | 116.0 | 0.072 | 21.315400 | 0.326079 | 0.299992 | 0.00042680147 | 0.00085360294 | 0.00000652913 | 0.00001305825 | 0.00000600678 | 0.00001201355 |
| Truck | WAVE | NB1 | QUE | 0 | 1 | 2 | 70.5 | 27.9 | 116.0 | 0.072 | 52.932200 | 1.014298 | 0.933151 | 0.00028794137 | 0.00022790253 | 0.00000551759 | 0.00000436712 | 0.00000507617 | 0.00000401773 |
| Truck | WAVE | NB1 | ACC | 4 | 1 | 2 |  |  | 31.0 | 0.019 | 9.939110 | 0.186020 | 0.171138 | 0.00005315317 | 0.00010630633 | 0.00000099481 | 0.00000198963 | 0.00000091523 | 0.00000183045 |
| Truck | WAVE | NB1 | FFD | 7 | 1 | 2 |  |  | 184.5 | 0.115 | 6.352800 | 0.145501 | 0.133860 | 0.00020230256 | 0.00040460513 | 0.00000463342 | 0.00000926683 | 0.00000426272 | 0.00000852543 |
| Truck | WAVE | NB2 | FFA | 7 | 1 | 2 |  |  | 176.2 | 0.109 | 6.352800 | 0.145501 | 0.133860 | 0.00019316103 | 0.00038632206 | 0.00000442404 | 0.00000884809 | 0.00000407009 | 0.00000814019 |
| Truck | WAVE | NB2 | DEC | 2 | 1 | 2 |  |  | 16.0 | 0.010 | 21.315400 | 0.326079 | 0.299992 | 0.00005884430 | 0.00011768859 | 0.00000090019 | 0.00000180038 | 0.00000082817 | 0.00000165634 |
| Truck | WAVE | NB2 | QUE | 0 | 1 | 2 | 4.6 | 3.3 | 16.0 | 0.010 | 52.932200 | 1.014298 | 0.933151 | 0.00001878766 | 0.00002695621 | 0.00000036001 | 0.00000051654 | 0.00000033121 | 0.00000047522 |
| Truck | WAVE | NB2 | ACC | 4 | 5 | 4 |  |  | 30.7 | 0.019 | 9.939110 | 0.186020 | 0.171138 | 0.00026347708 | 0.00021078166 | 0.00000493123 | 0.00000394498 | 0.00000453673 | 0.00000362938 |
| Truck | wave | NB2 | FFD | 7 | 5 | 4 |  |  | 370.5 | 0.230 | 6.352800 | 0.145501 | 0.133860 | 0.00203114012 | 0.00162491209 | 0.00004652001 | 0.00003721601 | 0.00004279814 | 0.00003423851 |
| Truck | wave | SB1 | FFA | 7 | 3 | 5 |  |  | 298.1 | 0.185 | 6.352800 | 0.145501 | 0.133860 | 0.00098051455 | 0.00163419092 | 0.00002245711 | 0.00003742852 | 0.00002066041 | 0.00003443402 |
| Truck | wave | SB1 | DEC | 2 | 3 | 5 |  |  | 82.4 | 0.051 | 21.315400 | 0.326079 | 0.299992 | 0.00090950117 | 0.00151583528 | 0.00001391337 | 0.00002318895 | 0.00001280026 | 0.00002133377 |
| Truck | WAVE | SB1 | QUE | 0 | 3 | 5 | 14.4 | 17.4 | 82.4 | 0.051 | 52.932200 | 1.014298 | 0.933151 | 0.00017644067 | 0.00035533190 | 0.00000338099 | 0.00000680894 | 0.00000311050 | 0.00000626421 |
| Truck | WAVE | SB1 | ACC | 4 | 2 | 2 |  |  | 30.1 | 0.019 | 9.939110 | 0.186020 | 0.171138 | 0.00010323321 | 0.00010323321 | 0.00000193211 | 0.00000193211 | 0.00000177754 | 0.00000177754 |
| Truck | WAVE | SB1 | FFD | 7 | 2 | 2 |  |  | 182.9 | 0.114 | 6.352800 | 0.145501 | 0.133860 | 0.00040103400 | 0.00040103400 | 0.00000918504 | 0.00000918504 | 0.00000845018 | 0.00000845018 |
| Truck | WAVE | SB2 | FFA | 7 | 2 | 2 |  |  | 51.3 | 0.032 | 6.352800 | 0.145501 | 0.133860 | 0.00011244097 | 0.00011244097 | 0.00000257528 | 0.00000257528 | 0.00000236924 | 0.00000236924 |
| Truck | WAVE | SB2 | DEC | 2 | 1 | 1 |  |  | 138.5 | 0.086 | 21.315400 | 0.326079 | 0.299992 | 0.00050961034 | 0.00050961034 | 0.00000779592 | 0.00000779592 | 0.00000717222 | 0.00000717222 |
| Truck | WAVE | SB2 | QUE | 0 | 1 | 1 | 40.3 | 42.5 | 138.5 | 0.086 | 52.932200 | 1.014298 | 0.933151 | 0.00016459627 | 0.00017358167 | 0.00000315403 | 0.00000332621 | 0.00000290170 | 0.00000306010 |
| Truck | WAVE | SB2 | ACC | 4 | 2 | 1 |  |  | 30.3 | 0.019 | 9.939110 | 0.186020 | 0.171138 | 0.00010395097 | 0.00005197548 | 0.00000194554 | 0.00000097277 | 0.00000178990 | 0.00000089495 |
| Truck | WAVE | SB2 | FFD | 7 | 2 | 1 |  |  | 278.2 | 0.173 | 6.352800 | 0.145501 | 0.133860 | 0.00061005079 | 0.00030502540 | 0.00001397224 | 0.00000698612 | 0.00001285438 | 0.00000642719 |
| Truck | WAVE | SBL2 | DEC | 2 | 1 | 1 |  |  | 31.8 | 0.020 | 21.315400 | 0.326079 | 0.299992 | 0.00011689844 | 0.00011689844 | 0.00000178829 | 0.00000178829 | 0.00000164522 | 0.00000164522 |
| Truck | WAVE | SBL2 | QUE | 0 | 1 | 1 | 40.3 | 42.5 | 31.8 | 0.020 | 52.932200 | 1.014298 | 0.933151 | 0.00016459627 | 0.00017358167 | 0.00000315403 | 0.00000332621 | 0.00000290170 | 0.00000306010 |



## Appendix V: AERMOD Results Summary (Inputs and Outputs provided electronically)

## Results Summary

C:\Lakes\AERMOD View\PM25_2016-2020\PM25_2016-2020.isc

## PM2.5 - Concentration - Source Group: ALL

| Averaging <br> Period | Rank | Peak | Units | $\mathbf{X}$ <br> $(\mathbf{m})$ | $\mathbf{Y}$ <br> $\mathbf{( m )}$ | ZELEV <br> $(\mathbf{m})$ | ZFLAG <br> $(\mathbf{m})$ | ZHILL <br> $(\mathbf{m})$ | Peak Date, <br> Start Hour |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 24-HR | 1ST | 0.70358 | $\mathrm{ug} / \mathrm{m}^{\wedge} 3$ | 354250.63 | 571609.48 | 181.31 | 0.00 | 181.31 | $11 / 6 / 2016,24$ |
| ANNUAL |  | 0.12736 | $\mathrm{ug} / \mathrm{m}^{\wedge} 3$ | 354160.00 | 571315.00 | 181.35 | 0.00 | 181.35 |  |
| ANNUAL Y1 |  | 0.13634 |  | 354160.00 | 571465.00 | 181.57 | 0.00 | 181.57 |  |
| ANNUAL Y2 |  | 0.12172 |  | 354160.00 | 571315.00 | 181.35 | 0.00 | 181.35 |  |
| ANNUAL Y3 |  | 0.13474 |  | 354110.00 | 571265.00 | 181.43 | 0.00 | 181.43 |  |
| ANNUAL Y4 |  | 0.12367 |  | 354160.00 | 571315.00 | 181.35 | 0.00 | 181.35 |  |
| ANNUAL Y5 |  | 0.12924 |  | 354160.00 | 571465.00 | 181.57 | 0.00 | 181.57 |  |

## Results Summary

C:ILakes\AERMOD ViewIPM10_2016-2020IPM10_2016-2020.isc
PM10 - Concentration - Source Group: ALL

| Averaging <br> Period | Rank | Peak | Units | $\mathbf{X}$ <br> $(\mathbf{m})$ | Y <br> $\mathbf{( m )}$ | ZELEV <br> $(\mathbf{m})$ | ZFLAG <br> $(\mathbf{m})$ | ZHILL <br> $(\mathbf{m})$ | Peak Date, <br> Start Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $24-H R$ | 2ND | 0.65495 | $\mathrm{ug} / \mathrm{m}^{\wedge} 3$ | 354210.00 | 571615.00 | 181.39 | 0.00 | 181.39 | $11 / 7 / 2016,24$ |

## Results Summary

C:ILakes\AERMOD View 1 NO2_2016-2020\NO2_2016-2020.isc
NO2 - Concentration - Source Group: ALL

| Averaging <br> Period | Rank | Peak | Units | $\mathbf{X}$ <br> $(\mathbf{m})$ | $\mathbf{Y}$ <br> $(\mathbf{m})$ | ZELEV <br> $(\mathbf{m})$ | ZFLAG <br> $(\mathbf{m})$ | ZHILL <br> $(\mathbf{m})$ | Peak Date, <br> Start Hour |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-HR | 8TH | 32.78342 | $\mathrm{ug} / \mathrm{m}^{\wedge} 3$ | 354110.00 | 571165.00 | 181.53 | 0.00 | 181.53 |  |
| ANNUAL |  | 4.48616 | $\mathrm{ug} / \mathrm{m}^{\wedge} 3$ | 354160.00 | 571265.00 | 181.41 | 0.00 | 181.41 |  |
| ANNUAL Y1 |  | 4.53627 | $\mathrm{ug} / \mathrm{m}^{\wedge} 3$ | 354160.00 | 571265.00 | 181.41 | 0.00 | 181.41 |  |
| ANNUAL Y2 |  | 4.29452 | $\mathrm{ug} / \mathrm{m}^{\wedge} 3$ | 354160.00 | 571265.00 | 181.41 | 0.00 | 181.41 |  |
| ANNUAL Y3 |  | 4.57723 | $\mathrm{ug} / \mathrm{m}^{\wedge} 3$ | 354110.00 | 571215.00 | 181.43 | 0.00 | 181.43 |  |
| ANNUAL Y4 |  | 4.51710 | $\mathrm{ug} / \mathrm{m}^{\wedge} 3$ | 354160.00 | 571265.00 | 181.41 | 0.00 | 181.41 |  |
| ANNUAL Y5 |  | 4.55589 | $\mathrm{ug} / \mathrm{m}^{\wedge} 3$ | 354160.00 | 571265.00 | 181.41 | 0.00 | 181.41 |  |

